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### Evaluation of decontamination factor of radioactive methyl iodide on activated carbons at high humid conditions



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Byung-Seon Choi<sup>\*</sup>, Seon-Byeong Kim, Jeikwon Moon, Bum-Kyung Seo

Korea Atomic Energy Research Institute (KAERI), P.O.Box 150, Yuseong, Daejeon, 305-600, Republic of Korea

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### ABSTRACT

Radioactive iodine (<sup>131</sup>I) released from nuclear power plants has been a critical environmental concern for workers. The effective trapping of radioactive iodine isotopes from the off-gas stream generated from nuclear facilities is an important issue in radioactive waste treatment systems evaluation. Numerous studies on retaining methyl iodide (CH<sub>3</sub>I<sup>131</sup>) by impregnated activated carbons under the high content of moisture have been extensively studied so far. But there have been no good results on how to remove methyl iodide at high humid conditions up to now. A new challenge is to introduce other promising impregnating chemical agents that are able to uptake enough radioactive methyl iodide under high humid conditions. In order to develop a good removal efficiency to control radioiodine gas generated from a high humid process, activated carbons (ACs) impregnated with triethylene diamine (TEDA) and qinuclidine (QUID) were prepared. In addition, the removal efficiencies of the activated carbons (ACs) under humid conditions up to 95% RH were evaluated by applying the standard method specified in ASTM-D3808. Quinuclidine impregnated activated carbon showed a much higher decontamination factor above 1,000, which is enough to meet the regulation index for the iodine filters in nuclear power plants (NPPs).

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### 1. Introduction

Radioactive isotopes of iodine are potentially hazardous fission products that could be generated as a uranium fission product during the nuclear power plants' (NPPs) operations, as they can critically impact the workers and the environment. Among the various types of isotopes, iodine-131(<sup>131</sup>I) released as gaseous effluents from the nuclear power plants (NPPs) has been a critical environmental concern. This is due to the combination of its large inventory in irradiated nuclear fuel, a half-life of 8.05 d for the isotope of greatest radiological significance (<sup>131</sup>I), a complex chemistry that may lead to the formation of volatile species, and its hazardous biological effects on the thyroid. Removing these radioactive iodine isotopes from the gaseous effluents of NPPs is an important issue in radioactive waste treatment system evaluation, especially in their adherence to the "as low as reasonably achievable" (ALARA) criteria [1,26].

Under normal power operating conditions, the radioactive iodine release rates from the core and reactor coolant are very low.

In accidental situations, the amounts of iodine released into the containment systems and the environments depend on many factors. The plant's design construction details, and the sequence of the events leading to the accident, are very important. In the case of severe accidents, however, the actual quantities released may represent a significant percentage of the core inventory. Thus, estimates for individual nuclear power plants indicate their potentials [3–6]. Radioactive isotopes of iodine generated from nuclear power plants (NPPs) are partially converted radioactive organic iodide, such as methyl iodide (CH<sub>3</sub>I<sup>131</sup>), which react with organic matter in the process line. Because radioiodine is one of these gaseous wastes that can cause radiological harm on the human body and environment, it is important to remove this gas below the restriction of release, even in the case of normal operating and

### \* Corresponding author.

E-mail address: bschoi@kaeri.re.kr (B.-S. Choi).

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In one study, for example, airborne iodine <sup>131</sup>I was measured in the radioactive wastes treatment system of a German pressurized water reactor (PWR) [1]. Concentrations below 400 Bq/m<sup>3</sup> were detected at the inlets of the exhaust air filters for the reactor containment systems. Typical annual discharge rates for European reactor stations are in the range of  $10^7 - 10^9$  Bq/yr of iodine-131 [1]. An average <sup>131</sup>I discharge of 5.6x10<sup>9</sup> Bq/yr is usual for pressurized water reactors (PWR) in the United States [2].

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accident conditions. Therefore, numerous studies for the removal of radioiodine from the off-gas stream of nuclear facilities have been performed with the formation processes and chemical structure [1–6,26].

The removal of the radioactive isotopes from iodine have generally been performed using activated carbon (AC), silica, alumina, and polymer resin [1-3,5,6,26]. Also, impregnants such as KI, TEDA (triethylene diamine), and QUID (quinuclidine) have been widely used to improve the removal efficiency. The activated carbon is a widely used adsorbent for trapping radioactive iodine gases to protect personnel and environments from various nuclear facilities, including nuclear power plants (NPPs), and it also applicable for military respirators and purification apparatus from various toxic gases vapor and liquid chemicals because it has high porosity and hydrophobicity [7–10]. The impregnated TEDA on activated carbons can convert to quaternary ammonium salts by reacting with organic iodides as follows:

There has been some concern regarding the use of TEDAimpregnated activated carbon (AC) as an adsorbent for radioiodine removal because of pore blocking and the possible release of TEDA from the charcoal in continuously moist air streams. Therefore, the TEDA-impregnated activated carbon showed a rapid drop in the removal efficiency of activated carbon (AC) to trap methyl iodide (CH<sub>3</sub>I) generated from high humid conditions [11–13,26] (see Fig. 1).

Many researchers have tried to enhance the radioactive iodine trapping efficiency by modifying the surface functional groups and porosity of activated carbon or by impregnating with other chemicals [9–16]. Due to its many advantages including a low production cost, easy to control the surface hydrophobicity, and wide applications, activated carbon (AC) has been a widely used adsorbent for removing radioactive iodine isotopes to protect personnel and environments [7]. To enhance the adsorptive removal performance, the surface functional groups and porosity of AC have often been modified or impregnated with other chemicals [8-11,26]. Nowadays, quinuclidine (QUID) has been introduced as a prominent impregnating chemical for removing the radioactive isotopes of iodine. The molecular weight of a QUID (111.19 g/mol) is similar to that of a TEDA (112.18 g/mol), but the basicity of the former (pKa = 11.3) is much higher (TEDA: pKa = 8.7) [7,8]. QUID contains an amine group at one end of the molecule while the opposite end of the molecule permits its ready adsorption and retention on the preferred adsorbent activated carbon, as shown in Fig. 2.

Many previous studies were carried out to evaluate the removal efficiencies of TEDA-AC by changing various test conditions such as bed temperature, bed depth, and amount of impregnant. In the research on the novel impregnants for activated carbons to enhance their chemical activity, we prepared two activated carbons impregnated with TEDA and QUID and experimentally evaluated the decontamination factors of the ACs under high contents of moisture condition up to 95% RH by applying ASTM-D3808 [12,13].

### 2. Experimental and material

### 2.1. Preparation of materials

The two types of activated carbons (ACs) impregnated with TEDA and QUID were prepared to evaluate the decontamination factor (DF) of methyl iodide  $(CH_3I^{131})$  under a highly moisturizing condition up to 95 RH%. The base material used in this experimental evaluation was activated carbon. Activated carbons were prepared by impregnating two different chemical reagents of TEDA and QUID, respectively. Each adsorbent was immersed in the solution for 60 min and dried at 90 °C for 9 h in the oven. The amount of impregnants on ACs were obtained by the extraction of TEDA and QUID with acetonitrile solution and then the analysis of solution



Fig. 1. Reaction mechanism of radioactive methyl iodide with TEDA on activated carbons.



Fig. 2. Reaction mechanism of radioactive methyl iodide with QUID on activated carbons.

concentration using UV-Spectrophotometer. The physical property of two carbons with the aid of the BET-N2 (Micromeritics, ASAP 2400) analysis was obtained, as listed in Table 1. The physical properties of TEDA-AC and QUID-AC were similar to these of the AC, except for a slight decrease in the pore volume and surface area.

# 2.2. Test facility and conditions using radioactive methyl iodide $(CH_3^{131}I)$ tracer

The evaluation test of radioactive methyl iodide at a high moisture condition was conducted by the standard test method, as established in ASTM D3803-91 [14]. This standard covers the test method for establishing the capability of new and used activated carbon in removing gaseous radioactive iodine and iodine compounds from air and gas streams. This test determines the penetration of only <sup>131</sup>I-labeled (CH<sub>3</sub><sup>131</sup>I) through TEDA or QUID impregnated activated carbon under a normal contaminated operating condition (30 °C, 95% relative humidity). A schematic diagram of the test facility for this research is shown in Fig. 3. Based on this schematic diagram, we designed and constructed a test facility that included related components with required functions. The individual components of this facility consist of four systems, such as a gas supply system and humidity control section, test and backup bed assemblies, and radioactive iodine (CH<sub>3</sub><sup>131</sup>I) supply section. Bed canisters were constructed in accordance with ASTM D-3803-91 in all dimensions. The test bed canister was a single unit of the depth specified in the test and assembled from separate 50 mm deep canisters. A backup bed canister was also installed to trap completely radioactive methyl iodide that penetrated through a sample canister. Operating conditions for the test are listed in Table 2. The test adsorbent was packed in a stainless-steel canister assembled with clamps. The total depth of the assembled two canisters was 100 mm, and two canisters were packed with an

Table 1	
Physical characteristics of Adsorbent	s.

Characteristic	TEDA-AC (6.5 wt%)	QUID-AC (6.2 wt%)
Mean Pore Diameter(Å)	13.2	13.4
Micro Pore Volume(cm <sup>3</sup> /g)	0.523	0.515
Surface area(m <sup>2</sup> /g)	1275	1265



Fig. 3. Schematic diagram of test facility for removing radioactive methyl iodide.

# Table 2 Test conditions for removing $CH_3^{131}I$ established in ASM D3803-91.

Parameters	Pre-equilibrium period (First 16 h)	Equilibrium, Challenge and Elution periods (Final 4 h)
Temperature, °C	30 ± 0.5	$30 \pm 0.5$
Relative humidity, %	92-96	93–95
Flow rate, <i>l</i> /min	10-25	10-25
Linear velocity, m/min	12.2	12.2
Absolute pressure, kPa	101 ± 5	101 ± 5
Adsorbate concentration, mg/m <sup>3</sup>		$1.75 \pm 0.25$
Test duration		
Pre-equilibration, hr	$16 \pm 0.1$	
Equilibration, min		$120 \pm 1$
Challenge, min		$60 \pm 1$
Elution, min		60 ± 1

adsorbent of about 56.8 g per canister for each run.

The test facility was equipped with a compressed air supply and humidity control system. All of the flow lines were equipped with check valves to prevent the back flow. The flow rate of air was controlled by a mass flow controller (MFC). The water temperature maintained a constant temperature of 30 °C, and all the gas was supplied into a water bath for humidifying. Radioactive methyl iodide ( $CH_3^{131}I$ ) with 3.7 x  $10^2$  Bq/m<sup>3</sup> was prepared by a synthesis reaction of Na<sup>131</sup>I source with organic compounds. The reaction to synthesize radioactive methyl iodide was proceeded with isotopic substitution as follows:  $CH^{127}I + 2Na^{131}I \cdot CH_3^{131}I + Na^{131}I \Leftrightarrow Na^{127}I$ . The Na<sup>131</sup>I source was purchased from KAERI. A multichannel analyzer (MCA, Canberra GC3018) with a lead-shielded NaI detector was used for the <sup>131</sup>I detection inside a uniform shape sampler.

The decontamination factor (DF) was obtained from the penetration values (P) as follows:

$$DF = 1/[1-P/100] P(\%) = A/(A+B) \times 100$$

A: Amount of gamma activity determined to have passed the backup bed (gamma activity in backup bed, Bq)

B: Amount of gamma activity trapped in the test bed (gamma activity in test bed, Bq).

### 3. Evaluation of decontamination factor (DF) of methyl iodide

### 3.1. Trapping efficiency of methyl iodide by TEDA-AC

In general, the amount of TEDA in activated carbon installed in a

nuclear facility has been applied at ranges from 2 wt% to 5wt. Several studies already conducted the removal efficiencies for radioactive methyl iodide by various commercial TEDA-ACs to determine the optimum amount of TEDA impregnated on ACs [17-20]. González et al. reported that 5.0 wt% impregnated TEDA-AC showed the highest removal efficiencies when it was evaluated by the standard method of ASTM D 3803 [19]. In this study, we measured the decontamination factors (DF) of radioactive methyl iodide on 6.5 wt% TEDA-AC at 95% RH by using the test facility shown in Fig. 3. All of the tests were performed according to ASTM 3803 listed in Table 2. The DFs of radioactive methyl iodide on TEDA-AC were evaluated from 502 to 683 (99.8%-99.82% in removal efficiency), as shown in Fig. 4. From the regulation index for the iodine filters in nuclear power plants (NPPs), the required removal efficiency of the iodine adsorber should be greater than 99.9% (DF  $\geq$  1000). The DFs of 6.5 wt% TEDA-AC measured from this study were not enough to meet the requirement of the TEDA-AC for removing radioactive methyl iodide. Previous studies already found that the removal of methyl iodide from various charcoal filters declined exponentially with an increase in the relative humidity (RH) [10–12,16–19]. Recently Keon Ho et al. reported the effect of moisture on the adsorption amounts of methyl iodide at various moisture contents up to 90% RH on tertiary amine impregnated ACs [20]. They reported that the removal efficiency of methyl iodide on TEDA-AC showed a rapid drop of 3 times compared to the dry condition as the moisture of feed stream increased at a range of 30–90% RH. As the humidity increased, the lots of water molecules inside the pores could block the active sites in pores, retard the reaction rate with methyl iodide, and finally decrease the removal



Fig. 4. Decontamination factors (DF) on TEDA-AC by ASTM D 3803. (30  $^{\circ}$ C, 95 RH, 12. 2 m/min, upstream activity 1279 Bq).

capacity, unlike the case under a dry condition. It has been also generally recognized that TEDA clearly contributed to enhancing the adsorption affinity due to the strong bond strength by chemical reaction between TEDA and water molecules in pores. It implies that the TEDA that reacted with methyl iodide in pores played a large role, and the chemical reaction with methyl iodide is more important than the physical properties (i.e., surface area, pore volume, etc.) of AC as the moisture in the feed stream increased. Removal efficiency on the TEDA-AC depend on the moisture contents of feed stream. DFs were also measured by using radioactive isotopes with high degree of safety. It seemed that data deviation are caused by a small change of moisture contents (95% RH) of feed stream.

### 3.2. Trapping efficiency of methyl iodide by QUID-AC



To evaluate the retention capability of radioactive methyl iodide on QUID-AC, decontamination factors (DF) were tested at a high humid condition of 95% RH. Fig. 5 shows that the DF of radioactive

Fig. 5. Decontamination factors (DF) on QUID-AC by ASTM D 3803. (30 °C, 95 RH, 12. 2 m/min, upstream activity 1564 Bq).

methyl iodide on QUID-AC was evaluated as being more than 1000 (DF > 1000) for the test conditions. In the case of the QUID-AC test results, the removal efficiencies of radioactive methyl iodide were evaluated to be more than 99.9%, which were enough to meet the regulation index for the iodine filters in nuclear power plants (NPPs). Compared with TEDA-AC, the DF of methyl iodide on QUID-AC had higher values than those of TEDA-AC. These results imply that the chemical reaction of OUID with methyl iodide (CH<sub>3</sub>I) might be more enhanced than that of TEDA because QUID formed products with a higher nucleophilicity (Nu = 20.5) than that of TEDA (Nu = 18.8) under a humid condition of up to 95% RH. Recently, the role of tertiary amines, such as TEDA and QUID, on the carbon surface in methyl iodide adsorption was studied by the experiments and DFT (density functional theory) calculations [21,22]. The atomic level removal process of methyl iodide molecules for TEDA-AC surfaces was investigated to identify fundamental mechanisms for the rate determining step as a function of adsorption sites, porosity, and humidity. From the simulation, it was found that the decomposition of methyl iodide into methyl and iodide ions occurs more easily in the presence of both tertiary amines and water. It was presumed that the alkylation of the tertiary amines was the major factor behind the improved CH<sub>3</sub>I removal efficiency of the amine-impregnated AC [23,24].

Among these two different tertiary amines, QUID showed a higher trapping capability of radioactive methyl iodide at a high moisture feed stream condition up to 95% RH. These results indicate that even a small amount of the impregnant contributed strongly to the chemical reaction under humid conditions.  $CH_3I$  molecules in the feed stream were thought to be adsorbed mainly by chemical reactions under humid conditions because of the 4–5-fold reduction of their trapping capacity in the high moisture conditions relative to dry conditions [20].

Under humid conditions, the diffusion of CH<sub>3</sub>I through the pores may be obstructed by pre-adsorbed water molecules. Therefore, it is expected that a certain amount of the impregnants moved into other pore sites when CH<sub>3</sub>I and water molecules were adsorbed. Then the water molecules in pores acted to enhance the chemical reaction between CH<sub>3</sub>I and the tertiary amine. According to DFT calculation [25], the heats generated by the alkylation reaction of CH<sub>3</sub>I with QUID and TEDA were estimated 20.0 kJ/mol and 12.8 kJ/ mol, respectively. Therefore, if CH<sub>3</sub>I reacts with the impregnants in the pore, it cannot diffuse into extremely deep pores where the adsorption potential is high. In case of tertiary amine up to 5 wt% loaded on the surface and pore of AC, more CH<sub>3</sub>I molecules are preferentially chemisorbed on the modified activated carbons. Experimental results showed that the QUID-impregnated AC had a much higher CH<sub>3</sub>I removal efficiency than the TEDA-impregnated AC at the nearly same amount of impregnant. It seems that QUID can be used as a promising chemical agent for removing radioactive methyl iodide.

### 4. Conclusion

The trapping capacity of radioactive methyl iodide with two different tertiary amine loaded ACs were evaluated at a high humidity up to 95% by applying ASTM D 3803. Both TEDA-AC and QUID-AC as adsorbents showed a good performance in removing methyl iodide (>99.9%) at a high humid condition up to 95% RH. Among these two different tertiary amines, QUID showed a higher trapping capability of radioactive methyl iodide at a high moisture feed stream condition up to 95% RH. It was considered that the chemical reaction of QUID with methyl iodide (CH<sub>3</sub>I) might be significantly enhanced due to the higher nucleophilicity than that of TEDA in the presence of a high humid condition. As for QUID-AC, the decontamination factor (DF) for removing radioactive methyl iodide under a high humid condition was more than 1,000, and it satisfied the requirements of the regulation index for the iodine filters in nuclear power plants (NPPs). QUID can be used as a new chemical impregnant for removing the radioactive iodine generated from nuclear power plants (NPPs).

### Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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### References

- D.T. Pence, B.A. Staples, in: In Proc. 13th AEC Air Cleaning Conference, CONF-740807, Atomic Energy Commission, Washington DC, 1974, p. 157.
- [2] International Atomic Energy Agency, Design of Off-Gas and Air Cleaning System at Nuclear Power Plant, IAEA Tech, 1987. No. 274.
- [3] R.T. Jubin, A Literature Survey of Methods to Remove Iodine from Off-Gas Streams Using Solid Sorbents, Citeseer, 1979.
- [4] J.G. Wilhelm, J. Furrer, in: In CEC Seminar on Radioactive Effluents from Nuclear Fuel Reprocessing Plants, Kernforschungszentrum, Karlsruhe, Federal Republic of Germany, 1977, p. 248.
- [5] R.H. Bellamy, Elemental iodine and methyl iodide adsorption on activated charcoal at low concentrations, Nucl. Saf. 15 (1974) 16.
- [6] J.C. Wren, C.J. Moore, M.T. Rasmussen, Methyl iodide trapping efficiency of aged charcoal samples from bruce-A emergency filtered air discharge systems, Nucl. Technol. 125 (1999) 28–39.
- [7] Y.C. Chiang, P.C. Chiang, C.P. Huang, Effects of pore structure and temperature on VOC adsorption on activated carbon, Carbon 39 (2001) 523–534.
- [8] T. Garcia, R. Murillo, D. Cazorla-Amoros, A. Mastral, A. Linares-Solano, Role of the activated carbon surface chemistry in the adsorption of phenanthrene, Carbon 42 (2004) 1683–1689.
- [9] M. Lillo-Ródenas, D. Cazorla-Amorós, A. Linares-Solano, Behaviour of activated carbons with different pore size distributions and surface oxygen groups for benzene and toluene adsorption at low concentrations, Carbon 43 (2005) 1758–1767.
- [10] M. Gonçalves, L. Sánchez-García, E. de Oliveira Jardim, J. Silvestre-Albero, F. Rodríguez-Reinoso, Ammonia removal using activated carbons: effect of the

surface chemistry in dry and moist conditions, Environ. Sci. Technol. 45 (2011) 10605–10610.

- [11] D. Kaplan, I. Nir, L. Shmueli, Effects of high relative humidity on the dynamic adsorption of dimethyl methylphosphonate (DMMP) on activated carbon, Carbon 44 (2006) 3247–3254.
- [12] G.I. Park, B.S. Choi, I.L. Cho, J.H. Kim, S.K. Ryu, Journal of Korea Nuclear Society 32 (5) (2000) 504.
- [13] J.J. Mahle, G.W. Peterson, B.J. Schindler, P.B. Smith, J.A. Rossin, G.W. Wagner, Role of TEDA as an activated carbon impregnant for the removal of cyanogen chloride from air streams: synergistic effect with Cu (II), J. Phys. Chem. C 114 (2010) 20083–20090.
- [14] J.A. Rossin, R.W. Morrison, Spectroscopic analysis and performance of an experimental copper/zinc impregnated, activated carbon, Carbon 29 (1991) 887–892.
- [15] S.W. Park, W.K. Lee, H. Moon, Adsorption and desorption of gaseous methyl iodide in a triethylenediamine-impregnated activated carbon bed, Sep. Technol. 3 (1993) 133–142.
- [16] G.O. Wood, Effects of air temperatures and humidities on efficiencies and lifetimes of air-purifying chemical respirator cartridges tested against methyl iodide, Am. Ind. Hygiene Assoc. J. 46 (1985) 251–256.
- [17] V.R. Deitz, Interaction of radioactive iodine gaseous species with nucleargrade activated carbons, Carbon 25 (1987) 31–38.
- [18] V.R. Deitz, L.A. Jonas, Catalytic trapping of methyl iodide by beds of impregnated charcoal, Nucl. Technol. 37 (1978) 59-64.
- [19] C. González-García, J. González, S. Román, Removal efficiency of radioactive methyl iodide on TEDA-impregnated activated carbons, Fuel Process. Technol. 92 (2011) 247–252.
- [20] K. Ho, S. Moon, H.C. Lee, Y.K. Hwang, C.H. Lee, Adsorptive removal of gaseous methyl iodide by triethylenediamine (TEDA)-Metal impregnated activated carbons under humid conditions, J. Hazard Mater. 368 (2019) 550–559.
- [21] H.C. Brown, N.R. Eldred, Studies in stereochemistry. XIV. Reaction of triethylamine and quinuclidine with alkyl halides; steric effects in displacement reactions, J. Am. Chem. Soc. 71 (1949) 445–450.
- [22] H. Chun, J. Kang, B. Han, First principles computational study on the adsorption mechanism of organic methyl iodide gas on triethylenediamine impregnated activated carbon, PCCP 18 (2016) 32050–32056.
- [23] V.K. Aggarwal, I. Emme, S.Y. Fulford, Correlation between pKa and reactivity ofQuinuclidine-based catalysts in the Baylis– hillman reaction: discovery of quinuclidine as optimum catalyst leading to substantial enhancement of scope, J. Org. Chem. 68 (2003) 692–700.
- [24] J. Kovach, J. Grimm, W. Freeman, TEDA vs quinuclidine: evaluation and comparison of two tertiary amine impregnants for methyl iodide removal from flow air stream, in: 17th DOE Nuclear Air Cleaning Conference: Proceedings, vol. 2, 1983, pp. 652–663.
- [25] K. Ho, H.C. Lee, Y. Lee, S. Lee, H. Jung, B. Han, C.H. Lee, Design of highly efficient adsorbents for removal of gaseous methyl iodide using tertiary amineimpregnated activated carbon: integrated experimental and first-principles approach, Chem. Eng. J. (2019).
- [26] B.S. Choi, B.Y. Min, S.B. Kim, J.K. Moon, Performance test of removal of gaseous radioactive methyl iodide by TEDA-impregnated activated carbon, in: WM Symposia, 2018, p. 18049.