# Characterization of Anodized Al 1050 with Electrochemically Deposited $\mathrm{Cu}, \mathrm{Ni}$ and $\mathrm{Cu} / \mathrm{Ni}$ and Their Behavior in a Model Corrosive Medium 

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#### Abstract

The specific benefits of the modified films formed on preliminary anodized aluminum, including the versatility of their potential applications impose the need for evaluation of the exploitation reliability of these films. In this aspect, the durability of Cu and Ni modified anodized aluminum oxide (AAO) films on the low-doped AA1050 alloy was assessed through extended exposure to a $3.5 \% \mathrm{NaCl}$ model corrosive medium. The electrochemical measurements by means of electrochemical impedance spectroscopy (EIS) and potentiodynamic scanning (PDS) after 24 and 720 hours of exposure have revealed that the obtained films do not change their obvious barrier properties. In addition, supplemental analyses of the coatings were performed, in order to elucidate the impact of the AC -deposition of Cu and Ni inside the pores. The scanning electron microscopy (SEM) images have shown that the surface topology is not affected and resembles the typical surface of an etched metal. The subsequent energy dispersive X-ray spectroscopy (EDX) tests have revealed a predominance of Cu in the combined AAO-Cu/Ni layers, whereas additional X-ray photoelectron (XPS) analyses showed that both metals form oxides with different oxidation states due to alterations in the deposition conditions, promoted by the application of AC -polarization of the samples.


Keywords : AA1050, Anodization, AC-Electrochemical Deposition, Copper, Nickel
Received: 21 July 2020, Accepted: 6 October 2020

## 1. Introduction

Anodization of aluminum and its alloys is a relatively simple approach for formation of highly-textured surfaces [1-10]. It enables ease of control of the respective surface parameters (pore diameters, depth and distribution) [11]. Among the apparent benefits of the anodic aluminum oxide (AAO) films is their highly-textured topology, which consists of a multitude of ordered hexagonal cells with centered cylindrical pores. This well-developed specific surface

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enables the deposition of a large variety of chemical substances, like paints, pigments, metals, oils, etc.

Particularly, the deposition of metals inside the pores of the $\mathrm{Al}_{2} \mathrm{O}_{3}$-matrices is successfully applied for the formation of functional coatings, having a number of practical applications. The AAO layers, modified with Cu [12-20], Ni [21-29] and combined Cu and Ni [30-34], are implemented as decorative and corrosion protective coatings [35-45], as well as solar absorbers [22,24,25].

The beneficial properties of the $\mathrm{Cu} / \mathrm{Ni}$ modified AAO layers can be further extended by addition of other elements, such as Fe and Co [46-49].

Among these remarkable benefits, especially the Cu and Ni modified AAO layers attract special attention, because of their ability to be used as catalysts for hydro-
gen and oxygen evolution [50-54], chemical synthesis [55-61] and contaminant decomposition [62,63].
On the other hand, the reliable service of any anodic aluminum oxide (AAO) film with deposited Cu and/or Ni requires high durability and chemical stability in aggressive and especially corrosive media. In this sense, the most widely used model corrosive media are NaCl solutions [64-66]. Particularly, the $3.5 \% \mathrm{NaCl}$ solutions are the most preferred, since they resemble sea water [67-69].
The coincidence of the application versatility of copper or nickel modified AAOs and the need for evaluation of their durability have imposed the investigation of the performance of the combined AAO$\mathrm{Cu} / \mathrm{Ni}$ films in model corrosive media (MCM).

In this sense, the aim of the present research is to define the impact of the AC -assisted Cu and Ni deposition on the characteristics and performance of preliminary anodized AA1050 alloy after extended periods of exposure to a $3.5 \% \mathrm{NaCl} \mathrm{MCM}$. The investigations comprise the evaluation of their durability in corrosive medium, the acquired morphology and the chemical composition of the obtained $\mathrm{Cu} / \mathrm{Ni}$ modified AAO layers. The performance of the coatings in the model corrosive medium was assessed by means of electrochemical impedance spectroscopy (EIS) and potentiodynamic scanning (PDS). The film topology was characterized by scanning electron microscopy (SEM), whereas the exact chemical composition of the layers was defined by energy dispersion X-ray spectroscopy (EDX) and X-ray photoelectron spectroscopy (XPS).

## 2. Experimental

### 2.1. Electrochemical film formation

The anodic films were formed on eight square $(2 \times 2 \mathrm{~cm})$ specimens, cut from the low-doped AA1050 alloy, in order to perform a systematic comparative study. All, but the referent samples underwent the following three consecutive procedures:

The preliminary surface treatment included etching in a NaOH solution $\left(50 \mathrm{~g} \mathrm{dm}^{-3}\right)$ for 2 minutes at $60^{\circ} \mathrm{C}$ and subsequent activation in diluted nitric acid $\left(\mathrm{HNO}_{3}: \mathrm{H}_{2} \mathrm{O}-1: 1\right)$, again for 2 minutes at room temperature, followed by vigorous washing with both tap and double-distilled water. All samples were anodized in $15 \mathrm{wt} . \% \mathrm{H}_{2} \mathrm{SO}_{4}$ by polarization under galvanostatic conditions (current density $15 \mathrm{~mA} \mathrm{~cm}^{-2}$ ) for

Table 1. Sample description

| Sample type | Sample codes | Electrolyte composition |
| :---: | :---: | :---: |
| references | AAO-Ref(1) | - |
|  | $\mathrm{AAO}-\mathrm{Ref}(2)$ | - |
| with copper | $\mathrm{AAO}-\mathrm{Cu}(1)$ | $0.4 \mathrm{~mol} \mathrm{dm}^{-3} \mathrm{CuSO}_{4}$ |
| deposition | $\mathrm{AAO}-\mathrm{Cu}(2)$ | $30 \mathrm{~g} \mathrm{dm}^{-3}\left(\mathrm{NH}_{4}\right) \mathrm{SOO}_{4}$ |
|  |  | $50 \mathrm{~g} \mathrm{dm}^{-3} \mathrm{H}_{3} \mathrm{BO}_{3}$ |
| with nickel | $\mathrm{AAO}-\mathrm{Ni}(1)$ | $0.4 \mathrm{~mol} \mathrm{dm}^{-3} \mathrm{NiSO}_{4}$ |
| deposition | $\mathrm{AAO}-\mathrm{Ni}(2)$ | $30 \mathrm{~g} \mathrm{dm}^{-3}\left(\mathrm{NH}_{4}\right) \mathrm{SO}_{4}$ |
|  |  | $50 \mathrm{~g} \mathrm{dm}^{-3} \mathrm{H}_{3} \mathrm{BO}_{3}$ |
|  |  | $0.2 \mathrm{~mol} \mathrm{dm}^{-3} \mathrm{CuSO}_{4}$ |
| with combined | $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}(1)$ | $0.2 \mathrm{~mol} \mathrm{dm}^{-3} \mathrm{NiSO}_{4}$ |
| $\mathrm{Cu} / \mathrm{Ni}$ deposition $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}(2)$ | $30 \mathrm{~g} \mathrm{dm}^{-3}\left(\mathrm{NH}_{4}\right) \mathrm{SO}_{4}$ |  |
|  |  | $50 \mathrm{~g} \mathrm{dm}^{-3} \mathrm{H}_{3} \mathrm{BO}_{3}$ |

50 min at $20^{\circ} \mathrm{C}$.
The electrochemical deposition of Ni and/or Cu in the anodized oxide layers was performed by alternating current polarization with at a constant voltage of 20 V and frequency 60 Hz , for 15 min at $20^{\circ} \mathrm{C}$. In order to carry out the planned systematic comparative study on the influence of the AC-deposition, the samples were divided into four sets of two samples, as shown in Table 1.

### 2.2. Electrochemical characterizations

All samples were subjected to comparative electrochemical measurements after 24 and 720 hours of exposure to the model corrosive medium (MCM), composed of $3.5 \% \mathrm{NaCl}$ solution performed with a potentiostat/galvanostat Autolab PGStat 30 of Metrohm (Netherlands), equipped with a frequency response analyzer (FRA2). The experiments were performed in a standard, three-electrode flat cell (ISO 16773-2), equipped with a cylindrical platinum mesh as a counter-electrode and an $\mathrm{Ag} / \mathrm{AgCl} / 3 \mathrm{M} \mathrm{KCl}$ reference electrode. Test areas of $2 \mathrm{~cm}^{2}$ from each specimen served as working electrodes. The measurements included electrochemical impedance spectroscopy (EIS) and potentiodynamic scanning (PDS). The EIS spectra were acquired in the frequency range from 10 kHz to 0.01 Hz , distributed in 50 measurement points. The amplitude of the excitation signal was up to 35 mV regarding the open circuit potential (OCP), in order to acquire readable spectra. The PDS measurements were performed in the range from -150 to +550 mV vs. OCP, at a sweep rate of $10 \mathrm{mV} \mathrm{s}^{-1}$.

### 2.3. Surface morphology and composition characterizations

The morphological observations were performed by means of Scanning Electron Microscopy (SEM), at 5000x magnification, in regime of back scattered electrons applying acceleration voltage of 20 kV . All the SEM images were acquired using a SEM/FIB LYRA I XMU product of TESCAN (UK).

Two independent methods were used for defining the element distribution on the surface of the formed films. The investigated samples were submitted to energy dispersion spectroscopy (EDX) analyses, followed by X-Ray Photoelectron Spectroscopy (XPS). The EDX analyses were executed by Quantax 200 of BRUKER (Germany), immediately after acquisition of the SEM images.

Subsequent XPS studies were performed on a VG Escalab II system, using Al $\mathrm{K} \alpha$ radiation with an energy of 1486.6 eV , whereas the chamber pressure was $10^{-9} \mathrm{~Pa}$. The C 1 s line of adventitious carbon at 285.5 eV was used as internal standard to calibrate the binding energies. The photoelectron spectra were corrected by subtracting a Shirley-type background and were quantified using the peak area and Scofield's photoionization cross-section. The accuracy of the backscattered electrons measured was $\pm 0.2 \mathrm{eV}$.

## 3. Results and Discussion

### 3.1. Electrochemical measurements

In order to obtain reliable data for both the barrier ability and durability of the obtained films, all elec-


Fig. 1. Averaged Nyquist (a) and Bode (b) plots of the EIS spectra, acquired after 24 and 720 hours of exposure.
trochemical measurements were performed twice: after 24 and 720 hours of exposure to the seawaterresembling MCM. The acquired spectra reveal almost perfect overlapping between the samples of each of the respective groups and indistinguishable deviations among the respective $\mathrm{AAO}, \mathrm{AAO}-\mathrm{Cu}, \mathrm{AAO}-\mathrm{Ni}$ and combined AAO-Cu/Ni coatings. Fig. 1 shows the averaged EIS spectra for each sample couple.

In addition, there are no distinguishable changes in the spectra, acquired after 720 hours of exposure, compared to those, obtained after the initial 24 hours. For this reason, all spectra were fitted to the same model equivalent circuit (MEC), in order to point out the variation of the values of the respective impedance elements.
For the present study, a simplified MEC was employed, compared to those in previous works [35,67,70-72]. This simplified circuit was selected following the rule of thumb [69,73-75], which imposes the use of the simplest possible equivalent circuit, that enables a high rate of fitting to the acquired spectra. Besides, following other previous works, it was assumed that some of the interfaces cannot be distinguished, due to the inherent similarities of the corresponding phases. A clear distinguishable electric double layer ( $e d l$ ) appears on the interface between the liquid MCM and the solid AAO (including the Cu and Ni deposits). The edl possesses its own capacitance ( $C_{\text {edl }}$ ). This layer covers the entire AAO surface, including the pore walls and bottoms and the areas among the pores (Fig. 2).

It is possible to expect some fluctuations of $C_{\text {edl }}$ inside the pores and the zones among them, but these cannot be distinguished by the impedance analyzer.

On the other hand, due to their insulation properties, the reference and the modified AAO layers (all assigned just as "oxide layers" or OL) also possess distinguishable capacitances ( $C_{\mathrm{AAO}}, C_{\mathrm{AAO}-\mathrm{Cu}}, C_{\mathrm{AAO}-\mathrm{Ni}}$ and $C_{\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}}$, respectively).

On the contrary, the porous and the dense parts of the respective oxide layers cannot be distinguished, since both are composed of amorphous $\mathrm{Al}_{2} \mathrm{O}_{3}$. Consequently, the capacitance of the entire oxide layer depends on the dense barrier layer which completely covers the metallic substrate, insulating it from the corrosive medium, already penetrated in the pores. In the same manner, the interface between the metallic substrates and the covering oxide layers should be indistinguishable, as well. The reason being is that both Al and $\mathrm{Al}_{2} \mathrm{O}_{3}$ solid phases are composed of aluminum in different oxidation states and that strong covalent bonds between the substrate and the covering oxide exist.

However, according to the classical theories [7679] and some recent extended reviews [80-82] the pore formation and the subsequent electrochemical deposition of Cu and/or Ni require occurrence of defects in the dense oxide sublayer. These defects serve as ion transport pathways, which enable electric charge transfer between the electrolyte and the metallic surface during anodization (in this case 15 $\mathrm{wt} . \% \mathrm{H}_{2} \mathrm{SO}_{4}$ ) and during metal deposition (from the electrolytes described in Table 1). These ion transport pathways remain after the film formation and during the impedance data acquisitions they can be distinguished by the diffusion obstructions accompanying the interaction of the corrosive medium components with the surface of the metallic substrate. The reac-


Fig. 2. Conceptual models of the investigated in the present study reference (a) and modified (b) AAO layers.
tions between the corrosive components of the electrolyte and the Al-surface under the defects in the dense AAO layer provide the whole charge transfer between the MCM and the investigated specimens during EIS data acquisition. These charge transfer reactions comprise both types of cathodic (oxygen reduction and resulting local alkalization) and anodic (aluminum oxidation and dissolution) corrosion reactions. The obstructions, related to the ion transport through the defects underneath the pores are ascribed to retarded diffusion constant phase elements ( $C P E_{\text {diff }}$ ) and charge transfer resistance $\left(R_{\mathrm{ct}}\right)$. Thus, the used MEC for the interpretation of the acquired EIS data (Fig. 3) was composed, following the model described above.


Fig. 3. Model equivalent circuit used for numerical EIS data acquisition: $R_{\mathrm{MCM}}$ - resistance of the model corrosive medium; $C_{(\text {OL+edl })}$ - capacitance of the dense $\mathrm{Al}_{2} \mathrm{O}_{3}$ part of the AAO; $R_{(\mathrm{OL}+\mathrm{ct})}$ - resistance of the MCM penetrated to the metallic substrate and the respective charge transfer; $C P E_{\text {diff }}$ - constant phase element of the diffusion retarding the ion transport across the AAO defects.

The data acquired from the fitting of the EIS spectra from Fig. 1 to the MEC illustrated in Fig. 3 are summarized in Table 2, for the initial 24 hours of exposure, and in Table 3 for the final EIS spectra acquisitions after 720 hours of exposure.

The data acquired after the initial 24 hours of exposure do not reveal remarkable differences among the sample groups. The resistance of the $3.5 \% \mathrm{NaCl}$ solution ( $R_{\mathrm{MCM}}$ ) has shown a deviation between 5 and $10 \Omega$ $\mathrm{cm}^{2}$. These deviations are probably related to the penetration rate of MCM into the respective OL pores. The oxide layer capacitance ( $\left.C_{(\text {oL }+ \text { edl })}\right)$ increases with one order of magnitude after Cu -impregnation, twice more, after Ni-inclusion, and almost with two orders of magnitude after the combined $\mathrm{Cu} / \mathrm{Ni}$ film formation. This $C_{(\mathrm{OL}+\mathrm{edI})}$ increment is related to the respective decrease of the capacitive reactance $Z_{\mathrm{c}}$ of the oxide layers due to the Cu and/or Ni depositions. The unexpected decrease of the capacitive reactance of the AAO layers by the electrochemical metal deposition is related to the widening of the AAO pores and the ion transport pathways beneath them. This claim is reasonable since the alternating current application results in a multitude of subsequent anodic and cathodic polarizations, promoted by the respective positive and negative AC-signal alterations. During the positive (anodic) semi-periods, the relatively high voltage causes oxygen evolution reaction. This reaction results in abundance of dissolved oxygen inside the pores.

Afterwards, during the negative (cathodic) semiperiods, the forced polarization results in accelerated local alkalization (Eq. 1):

$$
\begin{equation*}
2 \mathrm{H}_{2} \mathrm{O}+\mathrm{O}_{2}+4 \mathrm{e}^{-} \rightarrow 4 \mathrm{OH}^{-} \tag{1}
\end{equation*}
$$

Table 2. Results of the data fitting of the EIS spectra, acquired after 24 hours of exposure
$\left.\begin{array}{cccccc}\hline \hline \text { Sample } & \begin{array}{c}R_{\mathrm{McM}} \\ {\left[\Omega \mathrm{cm}^{2}\right]}\end{array} & \begin{array}{c}C_{(\text {OL }+ \text { ed })} \\ {[\mathrm{F} \mathrm{cm}}\end{array}\end{array}\right)$

This alkalization is confined to the pore bottoms just above the dense AAO layer and its defects (Eq. 2).

$$
\begin{equation*}
\mathrm{Al}_{2} \mathrm{O}_{3}+3 \mathrm{H}_{2} \mathrm{O}+2 \mathrm{OH}^{-} \rightarrow 2 \mathrm{Al}(\mathrm{OH})_{4}^{-} \tag{2}
\end{equation*}
$$

Finally, the higher $C_{(\text {oltedl }}$ of the modified oxide layers, compared to the reference AAO reveal that the Cu and/or Ni depositions on the pore walls and bottoms are rather thin and probably porous, otherwise these depositions would interrupt any contact between the MCM inside the pores and the defects beneath them, resulting in a pure capacitive response from the EIS spectra.
Indeed, the insets in Fig. 1 reveal slight ( $-Z^{\prime \prime} / Z^{\prime}$ )slopes, which become more distinct after incorporation of copper and nickel.
The $R_{(\mathrm{OL}+\mathrm{ct})}$ variations, caused by the Cu and/or Ni incorporation reveal other trends. The copper incorporation results in a weak decrease in $R_{(\mathrm{OL}+\mathrm{ct})}$, whereas its values increase by two entire orders of magnitude after Ni deposition. In the cases of combined $\mathrm{Cu} / \mathrm{Ni}$ incorporation, the $R_{(\mathrm{OL}+\mathrm{ct})}$ increment caused by the Ni -incorporation is suppressed rather by the lower concentration of $\mathrm{Ni}^{2+}$ ions (i.e. 0.2 and $0.4 \mathrm{~mol} \mathrm{dm}^{-3} \mathrm{NiSO}_{4}$, Table 1) than by the occurrence of $\mathrm{Cu}^{2+}$ ions. Consequently, adding $0.2 \mathrm{~mol} \mathrm{dm}^{-3} \mathrm{Ni}^{2+}$ ions, results in the increase of $R_{(\mathrm{OL}+\mathrm{ct})}$ by an entire order of magnitude, whereas the Cu -incorporation leads to negligible $R_{(\mathrm{OL}+\mathrm{ct})}$ alterations. The remarkable difference in $R_{(\mathrm{OL}+\mathrm{ct})}$ after Ni or Cu incorporation appears predominantly over the dense AAO layer and its defects. Probably, the $\mathrm{Ni}^{2+}$ ions obstruct the access of corrosive species to the defective dense AAO by forming a denser film of incorporated metal
or by formation of additional complex compounds in the liquid medium above the pore bottoms. This assumption is more probable than any obstruction by Ni-precipitates, because Ni and Cu compounds possess similar solubility and their effects should be indistinguishable. Indeed, the major difference between $\mathrm{Ni}^{2+}$ and $\mathrm{Cu}^{2+}$ ions is the much higher aptitude of the former type of ions to form complexes.

Finally, the diffusion constant phase element (CPEdiff) values uncover other features of the investigated oxide layers. The relatively similar $C P E_{\text {diff }}$ values for all cases of AAO, AAO-Cu, AAO-Ni and combined AAO-Cu/Ni layers reveal that the denser Ni-films and complexes do not obstruct completely the ion transfer pathways beneath the pores. Consequently, these pathways are not capillaries filled by MCM, but rather linear and/or planar defects in the $\mathrm{Al}_{2} \mathrm{O}_{3}$ structure, which enable $\mathrm{Al}^{3+}$ and $\mathrm{O}^{2-}$ ions transition towards both interfaces of the dense AAO layer: with the pore bottoms and the metallic surface. This assumption is confirmed by the almost capacitive character of the $C P E_{\text {diff }}$ elements, revealed by the rather high values of the exponential multiplier ( $n$ ), which tends to unit for all cases. Consequently, the ion exchange between the pore bottoms and the metallic surface proceeds by transport of point defects, like interstitial $\mathrm{Al}^{3+}$ and $\mathrm{O}^{2-}$ ions, as well as vacancies transitions through the solid amorphous $\mathrm{Al}_{2} \mathrm{O}_{3}$.

The data in Table 3, acquired after 720 hours of exposure reveal that the modified films began to resemble the reference AAO layers. On the other hand, the impedance values of the reference AAO layers have not altered their values. These facts show

Table 3. Results of the data fitting of the EIS spectra, acquired after 720 hours of exposure

| Sample type | $R_{\mathrm{MCM}}$ <br> $\left[\Omega \mathrm{cm}^{2}\right]$ | $C_{(\text {OL+edl }}$ <br> $\left[\mathrm{F} \mathrm{cm}^{-2}\right]$ | $R_{(\mathrm{OL}+\mathrm{ct)}}$ <br> $\left[\Omega \mathrm{cm}^{2}\right]$ | $C P E_{\text {diff }}$ <br> $\left[\mathrm{s}^{\mathrm{n}} \Omega^{-1} \mathrm{~cm}^{-2}\right]$ | n |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{AAO}-\operatorname{Ref}(1)$ | $10.27 \pm 2.42$ | $(1.30 \pm 0.28) \times 10^{-7}$ | $(2.69 \pm 0.22) \times 10^{3}$ | $(12.77 \pm 0.40) \times 10^{-7}$ | $0.90 \pm 0.01$ |
| $\mathrm{AAO}-\operatorname{Ref}(2)$ | $36.60 \pm 6.98$ | $(3.55 \pm 0.24) \times 10^{-7}$ | $(0.76 \pm 0.08) \times 10^{3}$ | $(12.22 \pm 0.28) \times 10^{-7}$ | $0.93 \pm 0.01$ |
| $\mathrm{AAO}-\mathrm{Cu}(1)$ | $20.70 \pm 2.31$ | $(7.34 \pm 0.46) \times 10^{-7}$ | $(0.34 \pm 0.03) \times 10^{3}$ | $(5.86 \pm 0.04) \times 10^{-7}$ | $0.91 \pm 0.01$ |
| $\mathrm{AAO}-\mathrm{Cu}(2)$ | $26.12 \pm 2.31$ | $(5.94 \pm 0.36) \times 10^{-7}$ | $(0.31 \pm 0.03) \times 10^{3}$ | $(5.97 \pm 0.06) \times 10^{-7}$ | $0.93 \pm 0.01$ |
| $\mathrm{AAO}-\mathrm{Ni}(1)$ | $11.73 \pm 2.05$ | $(1.66 \pm 0.29) \times 10^{-7}$ | $(0.81 \pm 0.05) \times 10^{3}$ | $(2.77 \pm 0.01) \times 10^{-7}$ | $0.95 \pm 0.01$ |
| $\mathrm{AAO}-\mathrm{Ni}(2)$ | $9.26 \pm 2.05$ | $(4.30 \pm 0.34) \times 10^{-7}$ | $(0.26 \pm 0.04) \times 10^{3}$ | $(6.90 \pm 0.01) \times 10^{-7}$ | $0.91 \pm 0.01$ |
| $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}(1)$ | $9.26 \pm 2.05$ | $(163.31 \pm 32.66) \times 10^{-7}$ | $(4.90 \pm 1.81) \times 10^{3}$ | $(6.63 \pm 0.02) \times 10^{-7}$ | $0.91 \pm 0.01$ |
| $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}(2)$ | $7.27 \pm 2.05$ | $(386.00 \pm 34.14) \times 10^{-7}$ | $(11.24 \pm 6.27) \times 10^{3}$ | $(6.31 \pm 0.01) \times 10^{-7}$ | $0.90 \pm 0.01$ |

that the AAO layers possess remarkable durability, whereas the films of incorporated metal on the pore walls and bottoms have lost their supplemental contribution to the barrier properties of the resulting protective layers.

The unique exclusion from the inference made above belongs to the $C_{(\text {oL+edl })}$ values of the combined $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}$ layers. These values are by an entire order of magnitude higher than all the rest. Obviously, this increment of the oxide layer capacitance is a result of the simultaneous occurrence of Cu and Ni in the combined layers. Consequently, the combined $\mathrm{Cu} / \mathrm{Ni}$ deposits on the pore walls and bottoms deteriorate due to the potential difference between the composing Cu and Ni. Hence, according to the standard potentials [83], Ni is more active than Cu (Eqs. 3-5):

$$
\begin{align*}
& \mathrm{Cu}^{2+} \rightarrow \mathrm{Cu}^{0}+2 \mathrm{e}^{-} \quad\left(+0.34 \mathrm{~V}_{\mathrm{SHE}}\right)  \tag{3}\\
& \mathrm{Ni}^{2+} \rightarrow \mathrm{Ni}^{0}+2 \mathrm{e}^{-} \quad\left(-0.26 \mathrm{~V}_{\mathrm{SHE}}\right) \tag{4}
\end{align*}
$$

Therefore, in the $\mathrm{Cu} / \mathrm{Ni}$ redox couple, the copper will oxidize nickel, resulting in the following overall reaction:

$$
\begin{equation*}
\mathrm{Ni}^{0}+\mathrm{Cu}^{2+} \rightarrow \mathrm{Ni}^{2+}+\mathrm{Cu}^{0} \quad\left(0.08 \mathrm{~V}_{\text {couple }}\right) \tag{5}
\end{equation*}
$$

In the present case, the combined $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}$ layers suffer partial destruction, by dissolution of the Nidomains, promoted by the occurrence of Cu , as an oxidant. This assumption provides the most probable explication for the sharp $C_{(\mathrm{OL}+\mathrm{ed})}$ rise after 720 hours of exposure, corresponding to the decay of the capacitive resistance of the respective combined AAO-Cu/ Ni layer.
The comparison of the EIS data acquired after 24 and 720 hours of exposure (Tables 2 and 3) reveal that $R_{(\mathrm{OL}+\text { edl })}$ of the AAO-Ni layers decays with four entire orders of magnitude. The most probable reason is the much lower adhesion of the incorporated Ni films to the pore walls and bottoms. Probably, the decomposition of the Ni-complex compounds has an additional effect to this decay. The acquired EIS data cannot uphold any alternative explications, since Cu is a stronger oxidant than Ni , in respect to Al . However, the AAO-Cu films show insignificant $C_{\text {(OL+edl) }}$ and $R_{(\text {OL+edl })}$ alterations, compared to those of the AAO-Ni films.


Fig. 4. Averaged anodic PDS curves acquired after 24 (a) and 720 (b) hours of exposure.

Consequently, the Ni deposits form thicker films with lower adhesion to the AAO pore walls and bottoms, compared to those of Cu .
In order to obtain a more complete image regarding the electrochemical performance of the obtained samples, during their exposure to $3.5 \% \mathrm{NaCl}$ solution, additional potentiodynamic scanning curves (PDS) were acquired. The overlapping of the potentiodynamic curves and the almost horizontal anodic branches (Fig. 4a) reveal the complete passivation of the substrate surfaces by the AAO layers. Besides, these curves are positioned well below $10^{-8} \mathrm{~A} \mathrm{~cm}^{-2}$, revealing the remarkable suppression of the interaction between the samples and the MCM (i.e. remarkable corrosion supression). Following the concepts, described in the previous sections, the corrosion process is strongly hindered by the $\mathrm{Al}^{3+}$ and $\mathrm{O}^{2-}$ charge transfer across the ion transport pathways under the

AAO pores. This inference is further confirmed by the PDS curves acquired after 720 hours (Fig. 4b). These curves remain at the same current densities as the initial ones, revealing that the interaction between the MCM and the AAO covered specimens is quasistationary and that corrosion proceeds with an insignificant rate. In addition, the incorporated Cu and/or Ni do not contribute to the formed films of corrosion protective properties of the AAO layers, since the PDS curves of all the investigated specimens are situated at similar corrosion current densities. Finally, comparing positions (a) and (b) of Fig. 4, it could be concluded that at the initial 24 hours of exposure the thin $\mathrm{AAO}-\mathrm{Cu}$ and $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}$ layers possess slightly enhanced barrier ability (i.e. lower current densities), compared to this of the AAO references, due to the thin layers deposited on the pore walls and bottoms. At the beginning of the exposure these layers interrupt the ion transport pathways. However, after 720 hours of exposure, the respective PDS curves overlap with the one of the reference samples, suggesting that the additional Cu and $\mathrm{Cu} / \mathrm{Ni}$ layers have already lost their supplemental effect to the basic AAO layer barrier properties.
For comparison, the PDS curves of the AAO-Ni layers remain above all others (i.e. at higher current densities) for the entire exposure period. The most probable reason is the higher chemical activity of this element, compared to that of copper. This statement is confirmed by the more negative $E_{\text {corr }}$ potentials of the AAO-Ni samples. In contrast, copper possesses cathodic nature, compared to the other elements. It is rather noticeable by the more positive $E_{\text {corr }}$ values, detected after the initial 24 hours of exposure. However, after 720 hours, the PDS curve of the AAO-Cu has approached the others, revealing a shift towards more negative values. Only the AAO-Ni layer has shown a shift in the opposite direction. This exclusion can be explained with the variety of possible oxidation states of the Ni compounds [84]. This variety enables various transitions among the respective oxidation states of this element during the long-term corrosion test. Indeed, the exposure of the already formed Ni containing layers on the AAO pore surfaces to the corrosive medium species (e.g. $\mathrm{Na}^{+}, \mathrm{Cl}^{-}$, $\mathrm{OH}^{-}, \mathrm{H}_{3} \mathrm{O}^{+}$, dissolved $\mathrm{O}_{2}$, etc.) predetermines a multitude of possible chemical interactions between this layer and the corrosive medium.

Besides, all depositions were performed by means

Table 4. Numerical data obtained from the PDS curves acquired after 24 and 720 hours of exposure

| Sample | After 24 hours |  | After 720 hours |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $E_{\text {corr }}[\mathrm{mV}]$ | $R_{p}\left[\mathrm{k} \Omega \mathrm{cm}^{2}\right]$ | $E_{\text {corr }}[\mathrm{mV}]$ | $R_{\mathrm{p}}\left[\mathrm{k} \Omega \mathrm{cm}^{2}\right]$ |
| AAO-Ref(1) | -0.196 | $3.427 \times 10^{3}$ | -0.322 | $10.710 \times 10^{3}$ |
| $\mathrm{AAO}-\mathrm{Ref}(2)$ | -0.101 | $4.276 \times 10^{3}$ | -0.068 | $11.130 \times 10^{3}$ |
| $\mathrm{AAO}-\mathrm{Cu}(1)$ | -0.058 | $18.820 \times 10^{3}$ | -0.290 | $23.240 \times 10^{3}$ |
| $\mathrm{AAO}-\mathrm{Cu}(2)$ | -0.057 | $26.633 \times 10^{3}$ | -0.130 | $30.140 \times 10^{3}$ |
| $\mathrm{AAO}-\mathrm{Ni}(1)$ | -0.117 | $5.618 \times 10^{3}$ | -0.134 | $5.927 \times 10^{3}$ |
| $\mathrm{AAO}-\mathrm{Ni}(2)$ | -0.374 | $17.020 \times 10^{3}$ | -0.323 | $13.730 \times 10^{3}$ |
| $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}(1)$ | -0.075 | $14.320 \times 10^{3}$ | -0.232 | $13.367 \times 10^{3}$ |
| $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}(2)$ | -0.201 | $18.858 \times 10^{3}$ | -0.129 | $15.790 \times 10^{3}$ |

of AC-polarization. The shift in reduction (during the negative semi-periods) and oxidation (during the positive semi-periods) conditions and vice versa result in the simultaneous formation of: $\mathrm{Cu}^{0} \leftrightarrow \mathrm{Cu}^{\mathrm{I}} \leftrightarrow \mathrm{Cu}^{\text {II }}$ and/or $\mathrm{Ni}^{0} \leftrightarrow \mathrm{Ni}^{\mathrm{I}} \leftrightarrow \mathrm{Ni}^{\mathrm{II}} \leftrightarrow \mathrm{Ni}^{\text {iII }} \leftrightarrow \mathrm{Ni}^{\text {IV }}$ deposits. The constant interactions of the formed Cu and/or Ni layers with the components of the corrosive medium, result in continuous $E_{\text {corr }}$ dissipations, but do not affect the protective properties of the AAO layer.

The weak increase of the $R_{\mathrm{p}}$ values after 720 hours of exposure to MCM can be explained, considering obstruction of the pore bottoms of the AAO layers by Keggin-like corrosion products [85].

### 3.2. Morphological observations and compositional characterizations

Supposing the existence of a direct correlation between the electrochemical performance of the investigated samples and their morphology, additional topological observations were performed by means of scanning electron microscopy (SEM).

The SEM images (Fig. 5) have confirmed the inferences from the previous paragraphs, since Cu and Ni deposition did not result in modification of the AAO morphology. At the applied magnification, the AAO pores are indistinguishable. The morphologies of the anodized samples resemble the observed Al-surfaces after the preliminary etching and acidic activation. The low-resolution images reveal laminar morphologies, resulting from the alloy rolling as a final production stage. The high-resolution images show multitude of shallow concavities with various diameters. These craters are a result of the preliminary alkaline and acidic treatment procedures. In addition, randomly spread coarse intermetallic inclusions or


Fig. 5. High- and low-resolution SEM images of the investigated samples: (a) AAO-Ref(1); (b) AAO-Ref(2); (c) $\mathrm{AAO}-\mathrm{Cu}(1)$; (d) $\mathrm{AAO}-\mathrm{Cu}(2)$; (e) $\mathrm{AAO}-\mathrm{Ni}(1)$; (f) AAO$\mathrm{Ni}(2) ;$ (g) AAO-Cu/Ni (1) and (h) AAO-Cu/ $\mathrm{Ni}(2)$.
cavities can also be distinguished. These cavities result from already dissolved intermetallic phases. In some images (Fig. 5b, c, g, h), the intermetallic inclusions or their cavities are beneath the craters, evincing that the intermetallic precipitates are also spread in depth, occupying the entire alloy bulk. The simultaneous occurrence of intermetallic phases and concavities from already dissolved inclusions reveals that the AA1050 alloy contains both types of more active (e.g. $\mathrm{Mg}, \mathrm{Zn}$, etc.) and nobler (e.g. $\mathrm{Cu}, \mathrm{Fe}, \mathrm{Mn}$, $\mathrm{Si}, \mathrm{Ti}, \mathrm{V}$, etc.) phases, so that the preliminary treatments cause dissolution of the formers.

Considering a direct relation between the chemical composition of the film and the resulting performance in the model corrosive medium, all samples were submitted to chemical analysis by means of different X-ray techniques.

The energy dispersion X-ray (EDX) maps analyses have shown that all elements composing the oxide layer are equally distributed on the whole surface of the respective samples, following its topology (Fig. 6).

The subsequent quantitative EDX point analyses have provided much more information on the exact content of the elements, composing the reference and the modified AAO layers. All data, acquired by the EDX point analyses are summarized in Table 5. In order to collect more interesting data, the reference samples were not submitted to quantitative analyses, but both samples of the biggest interest, namely the combined AAO-Cu/Ni coatings, were submitted to these measurements in triplicate.

The analysis of the quantitative data reveal that the

Table 5. Quantitative data acquired by EDX point analyses of the investigated samples

| Group | Sample | Element content [at. \%] |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Al | O | S | Cu | Ni |
| with copper | $\mathrm{AAO}-\mathrm{Cu}(1)$ | $40.20 \pm 1.13$ | $55.46 \pm 2.83$ | $4.29 \pm 0.01$ | $0.05 \pm 0.01$ | - |
| deposition | $\mathrm{AAO}-\mathrm{Cu}(2)$ | $40.64 \pm 1.10$ | $55.01 \pm 2.97$ | $4.29 \pm 0.01$ | $0.06 \pm 0.01$ | - |
|  |  |  |  |  | - | $0.05 \pm 0.01$ |
| with nickel | $\mathrm{AAO}-\mathrm{Ni}(1)$ | $40.04 \pm 1.08$ | $55.58 \pm 2.95$ | $4.33 \pm 0.01$ |  | $0.05 \pm 0.01$ |
| deposition | AAO-Ni(2) | $39.29 \pm 0.16$ | $56.44 \pm 2.94$ | $4.21 \pm 0.01$ | - | $0.03 \pm 0.01$ |
|  |  | $37.46 \pm 0.71$ | $58.85 \pm 2.41$ | $3.49 \pm 0.07$ | $0.17 \pm 0.01$ | $0.02 \pm 0.01$ |
|  |  | $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}(1)$ | $38.10 \pm 0.76$ | $58.01 \pm 2.44$ | $3.72 \pm 0.04$ | $0.15 \pm 0.01$ |
| with combined |  | $36.39 \pm 0.66$ | $60.16 \pm 2.29$ | $3.28 \pm 0.01$ | $0.16 \pm 0.01$ | $0.02 \pm 0.01$ |
| $\mathrm{Cu} / \mathrm{Ni}$ deposition |  | $37.45 \pm 0.71$ | $58.87 \pm 2.41$ | $3.50 \pm 0.01$ | $0.16 \pm 0.01$ | $0.02 \pm 0.01$ |
|  | $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}(2)$ | $37.88 \pm 0.76$ | $58.41 \pm 2.28$ | $3.56 \pm 0.01$ | $0.13 \pm 0.01$ | $0.02 \pm 0.01$ |
|  |  | $37.52 \pm 0.71$ | $58.67 \pm 2.46$ | $3.62 \pm 0.01$ | $0.16 \pm 0.01$ | $0.03 \pm 0.01$ |



Fig. 6. EDX map analyses of the element distribution in the reference and in the modified AAO layers
composition of the AAO layer in all cases is close the stoichiometric $\mathrm{Al}_{2} \mathrm{O}_{3}$, approaching 40 at. $\% \mathrm{Al}$ and 60 at. \% O. This finding suggests that the anodic oxide layers are composed of pure alumina, without any occurrence of boehmite or other $\mathrm{Al}_{2} \mathrm{O}_{3-\mathrm{x}} \mathrm{OH}_{\mathrm{x}}$ compounds. The relatively lower oxygen content is compensated by incorporated sulfur. This means that part of the oxygen in the AAO layers is substituted by sulfur from the anodization electrolyte ( $15 \mathrm{wt} . \%$ $\mathrm{H}_{2} \mathrm{SO}_{4}$ ), following the well-described mechanism, proposed by Shimizu et al. [86], and confirmed by our previous research work [70]. Probably, namely the incorporated sulfur is one of the reasons for the appearance of point defects in the AAO layers, since this element could exist in different oxidation states (being an electron donor or acceptor). These defects provide electron transport across the dense AAO layer, since this element occurs in different oxidation stages. The transitions between these oxidation states enables sulfur to donate or accept electrons, especially when the sample is polarized. Besides, the average sulfur content does not completely compensate the oxygen deficit in the cases of single Cu and Ni deposition. This deficit can be expressed as the difference between the stoichiometric $C_{\mathrm{O}}=60 \mathrm{at} . \%$
and the average value ( $a v$ ) measured for both types of coatings $C_{\text {Oav }}=55.62 \mathrm{at} . \%$. Thus, the oxygen deficit is equal to $\Delta C_{\mathrm{O}}=4.38 \%$, whereas the average value of the involved sulfur is: $C_{\mathrm{Sav}}=4.28 \mathrm{at} . \%$. Consequently, the sulfur incorporation results in the formation of anionic vacancies. Namely these vacancies could supply the $\mathrm{O}^{2-}$ ions transport across the dense part of the AAO layer. The subsequent electrochemical metal deposition has revealed rather low contents of Cu and Ni : around $0.05 \mathrm{at} . \%$, which corresponds to about $0.16 \mathrm{wt} . \%$. This fact reveals that the AC electrochemical metal incorporation results in the equal and low metal deposition rate for both metals.

The most interesting results are these obtained for the combined $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}$ coatings, which imposed the need for triple measurement. This approach enabled the determination of the average values of the incorporated metals: 0.155 at. $\%$ for Cu and 0.023 at. $\%$ for Ni. The comparison of the data in Table 5 shows that the combined electrochemical deposition from $\mathrm{Cu}^{\mathrm{II}}$ and $\mathrm{Ni}^{\text {II }}$ sulfates results in three times higher Cu and twice lower Ni contents, compared to the single metal incorporations. The twice lower Nicontent in the combined coating, compared to the single metal incorporation ( $0.05 \mathrm{at} . \% \mathrm{Ni}$ in the AAO-

Ni , compared to $0.02 \mathrm{at} . \% \mathrm{Ni}$ in the $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}$ ) is a result of the twice lower concentration of the used electrolyte (Table 1, experimental section). However, the Cu content is three times higher in the combined $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}$ coating, regardless in the lower $\mathrm{CuSO}_{4}$ concentration in the electrolyte. This correlation between the Cu and Ni contents in the modified AAO layers reveals that the presence of Ni accelerates the Cu deposition, probably following the mechanism, described by Eqs. 3-5.

Another interesting fact, which can be observed from Table 5 is that the Al concentration in the combined $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}$ layer ( $C_{\text {Alav }}=37.47$ at. $\%$ ) is with about $2.53 \%_{\text {at }}$ lower than the stoichiometric one. The sulfur content is also with about $1 \mathrm{at} . \%$ lower in the combined AAO-Cu/Ni coatings, compared to the single metal doped ones. On the contrary, the average oxygen content ( $C_{\text {Oav }}=58.83 \mathrm{at}$. $\%$ for $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}$ ) of the combined $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}$ layers is by $3.21 \mathrm{at} . \%$ higher than those of the single Cu or Ni metal doped AAO layers (i.e. $C_{\text {Oav }}=55.62$ at. $\%$ for both AAOCu and $\mathrm{AAO}-\mathrm{Ni}$ ).

Thus, the EDX point analyses have uncovered that the combined AAO-Cu/Ni coatings possess some differences, compared to the single metal doped $\mathrm{AAO}-\mathrm{Cu}$ and AAO-Ni coatings. Besides the three times higher Cu and twice lower Ni contents, the combined layers reveal lower contents of Al and S , but higher content of O . The lower Al and S contents of the combined coatings can be explained by their release, caused by dissolution of the S containing $\mathrm{Al}_{2} \mathrm{O}_{3}$ surface. This dissolution is induced from the AC-polarization during metal incorporation (Eqs. 1 and 2). However, in the present case, all samples pre-
sented in Table 5 have undergone metal incorporation.

Consequently, the lower Al and S contents in the combined $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}$ is a result of the relatively thicker $\mathrm{Cu} / \mathrm{Ni}$ layer, due to the enhanced copper deposition. This layer covers the entire AAO pore walls and bottoms and the point defects of incorporated sulfur, resulting in weaker Al and S detection X-ray signals.

Finally, the higher oxygen content, observed for the combined AAO-Cu/Ni layers is a result of the partial oxidation, at the oxidant conditions during the negative AC semi-periods. Indeed, the thicker $\mathrm{Cu} / \mathrm{Ni}$ layers, require higher oxygen amounts from the electrolyte for their oxidation.

The exact chemical composition, including the oxidation states of the involved elements requires a more precise analytical technique, such as X-ray photoelectron spectroscopy (XPS) analysis. The quantitative results of the respective XPS analyses in Table 6 confirm the above commented results from the EDX analyses, revealing that the main components of the AAO layers (i.e. Al and O ) approach the ratio of ( $\mathrm{Al}: \mathrm{O} \approx 2: 3$ ).

The relatively lower Al and O contents are result of the occurrence of $\mathrm{Fe}, \mathrm{Zn}$ and Cr , which are inherent for the AA1050 substrate. The composition of the samples of each pair are identical, revealing that the electrochemical deposition proceeds with obvious repeatability in all investigated cases. The data analyses of the XPS spectra also confirm the low efficiency of the deposition process, since both Cu and Ni contents are rather lower than this of incorporated S . The trends of rather higher Cu and twice lower Ni

Table 6. Element contents of the investigated samples determined by XPS

| Element content <br> [at. \%] | O | Al | S | Fe | Zn | N | Ca | Ni | Cu | Cr | Cl |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{AAO}(1)$ | 55.0 | 31.2 | 4.0 | 0.2 | 1.3 | 2.3 | 1.1 | 0.0 | 0.0 | 0.5 | 1.5 |
| $\mathrm{AAO}(2)$ | 54.1 | 34.4 | 3.2 | 0.5 | 1.5 | 3.9 | 1.7 | 0.0 | 0.0 | 0.8 | 0.0 |
| $\mathrm{Cu}(1)$ | 58.4 | 33.2 | 3.2 | 0.6 | 0.0 | 1.3 | 1.4 | 0.0 | 0.3 | 1.0 | 0.6 |
| $\mathrm{Cu}(2)$ | 60.0 | 30.8 | 3.7 | 0.6 | 0.0 | 2.2 | 1.8 | 0.0 | 0.2 | 0.8 | 0.0 |
| $\mathrm{Ni}(1)$ | 57.8 | 35.1 | 3.3 | 0.5 | 0.8 | 1.4 | 0.7 | 0.2 | 0.0 | 0.0 | 0.0 |
| $\mathrm{Ni}(2)$ | 59.7 | 33.3 | 3.1 | 0.0 | 1.2 | 0.0 | 0.0 | 0.1 | 0.0 | 1.0 | 0.0 |
| $\mathrm{Cu} / \mathrm{Ni}(1)$ | 58.4 | 32.8 | 3.2 | 0.6 | 0.4 | 0.8 | 0.2 | 0.2 | 1.5 | 0.0 | 1.8 |
| $\mathrm{C} / \mathrm{Ni}(2)$ | 58.0 | 32.5 | 4.3 | 1.4 | 0.9 | 0.6 | 0.5 | 0.1 | 0.8 | 0.0 | 0.0 |

contents in the combined AAO-Cu/Ni layers, compared to the single metal containing ones confirm the inferences made from the EDX analyses.

In addition, the acquired O1s spectra in Fig. 7a show that in all cases the oxygen peak is positioned at 531.6 eV . This peak is an indication for the Al-O chemical bonding, composing the AAO layer matrices $[87,88]$. This fact is an undoubted evidence for the complete coverage of the surface with $\mathrm{Al}_{2} \mathrm{O}_{3}$ layers. The wide asymmetrical A12p peak at 74.1 eV , in Figure 7 b also evinces that aluminum is in oxidized form [89-91].

Fig. 8a summarizes the Cu2p spectra of all copper containing samples. It shows that these spectra, acquired at 20 eV , for both Cu and Ni doped AAO layers possess very low intensity, due to the rather low concentrations of the electrochemically deposited metals.
The detailed Cu 2 p spectra of both $\mathrm{AAO}-\mathrm{Cu}$ films are shown in Fig. 8b. It shows that the acquired spec-


Fig. 7. O1s and Al 2 p spectra of the investigated films.
tra have rather low intensity and with remarkable noise, which imposes serious difficulties for the determination of the oxidation state of this element in the AAO-Cu doped films. The spectra, obtained at 20 eV show that the $\mathrm{Cu} 2 \mathrm{p}_{3 / 2}$ peak is situated at 932.8 or 933.4 eV , whereas the $\mathrm{Cu} 2 \mathrm{p}_{1 / 2}$ is at 952.8 or 953.4 eV , revealing spin-orbital splitting of 20.0 eV in both cases. A weak double satellite, indicative for $\mathrm{Cu}^{1+}$ was detected at 944 eV for one of the $\mathrm{AAO}-\mathrm{Cu}$ samples, whereas the other one showed intensive satellites, typical for CuO and $\mathrm{Cu}(\mathrm{OH})_{2}$. Nevertheless, both Cu -doped samples revealed a shoulder at 933.4 eV , which according to Biesinger et al. [92] is inherent for the $\mathrm{Cu}^{2+}$ oxidation state. In general, the spectra of the AAO-Cu doped films showed simultaneous occurrence of $\mathrm{Cu}^{0}, \mathrm{Cu}^{1+}$ and $\mathrm{Cu}^{2+}$, in different proportions for each sample. Further, Figure 8c shows the deconvoluted spectra of the combined AAO-Cu/ Ni layers, acquired at 50 eV . These spectra also reveal the coincident occurrence of $\mathrm{Cu}^{0}, \mathrm{Cu}^{1+}$ and $\mathrm{Cu}^{2+}$ in miscellaneous mixtures with different contents.

The acquired Ni2p spectra also possess low intensity and high signal noise, like the described above Cu 2 p spectra. Consequently, nickel content is as low as the copper one. This fact again imposed to acquire detailed spectra at 50 eV . The deconvolutions of $\mathrm{AAO}-\mathrm{Ni}$ and $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}$ spectra were performed following Grosvenor [93] and Biesinger [94], and are shown in Fig. 9.

The Ni2p spectrum is rather complex, since it is composed of a multitude of peaks and satellites, due to the considerable variety of possible electron transitions. For instance, the assignment of $\mathrm{Ni}^{2} \mathrm{p}_{3 / 2}$ spectra to Ni oxides and other compounds is based on charge


Fig. 8. Basic and deconvoluted Cu2p spectra of the investigated samples.


Fig. 9. Deconvoluted Ni 2 p spectra of the investigated samples.
transfer assignments of the main peak (at 854.6 eV in NiO ) and the broad satellite (centered at $\sim 861 \mathrm{eV}$ in NiO ) to the $\mathrm{cd}^{9} \mathrm{~L}$ and the unscreened $\mathrm{cd}^{8}$ final-state configurations, respectively ( L is a ligand hole) [95,96].
The splitting of the $\mathrm{Ni} 2 \mathrm{p}_{3 / 2}$ spectra of the AAO-Ni samples and the definition of the peak positions and half-widths for the respective oxidized states of Ni were performed following strictly the works of Biesinger et al. [92-94], using Casa XPS software, avoiding the use of offset. The analyzed spectrum contained two distinguishable satellites at 862.4 and 865.9 eV , respectively. These satellites are typical for the $\mathrm{Ni} 2 \mathrm{p}_{3 / 2}$ spectrum of $\beta-\mathrm{NiOOH}$ fitted with $\mathrm{Ni}(\mathrm{II})$ and $\mathrm{Ni}($ III $)$ multiplet envelops [93]. That was the reason to perform specific deconvolution for this compound. As a result, the positions of the characteristic peaks for $\mathrm{Ni} 2 \mathrm{p}_{3 / 2}$ Beta $\mathrm{Ni}^{3+} \mathrm{OOH}$, situated respec-
tively at: $854.6,855.3,855.7$ and 856.5 eV , as well as those for $\mathrm{Ni}^{2} \mathrm{p}_{3 / 2}$ Beta $\mathrm{Ni}^{2+} \mathrm{OOH}$, positioned at: 854.9, $855.7,857.7$ and 860.5 eV , as well as their satellites were defined. The analysis has shown that the ratio between $\mathrm{Ni}(\mathrm{III})$ and $\mathrm{Ni}(\mathrm{II})$ is $34 \%: 44 \%$, approaching 1:1. Consequently, the electrodeposited nickel forms simultaneously various oxides and hydroxides. In addition, peaks typical for metallic $\mathrm{Ni}^{0}$ and $\mathrm{Ni}_{2} \mathrm{~S}_{3}$ [97-99] were also registered at 852.6 eV and at 853.5 eV , respectively. Furthermore, the Ni2p spectra of the combined AAO-Cu/Ni layers contain supplemental peaks, at 853.1 eV and at 856.6 eV , with additional shake-up satellites which are characteristic for $\mathrm{Ni}^{2+}$ and $\mathrm{Ni}_{3} \mathrm{~S}_{2}$ [97]. Both shake-up satellites originated from the deconvolution, were joined in a wider peak at 861.9 eV . The valence states of nickel ions in $\mathrm{Ni}_{3} \mathrm{~S}_{2}$ are mostly $\mathrm{Ni}^{+}$and partially $\mathrm{Ni}^{2+}$. Therefore, the $\mathrm{Ni} 2 \mathrm{p}_{3 / 2}$ line appears at 853.1 eV , indicating the presence of divalent Ni species, as was established by Park et al. [97]. The correlation between the areas of the peaks of $\mathrm{Ni}^{2+}: \mathrm{Ni}_{3} \mathrm{~S}_{2}$ is approximately $1: 2$ (i.e. the area of the $\mathrm{Ni}^{2+}$ peak is 2356, whereas this of the $\mathrm{Ni}_{3} \mathrm{~S}_{2}$-peaks is about 4745).

Finally, from the analysis of the XPS spectra of all the investigated samples, it can be concluded that all the elements, composing the doped AAO layers are in oxidized form. The AC electrochemical metal incorporation has resulted in the formation of oxides and hydroxides in all possible oxidation states of Cu and Ni . The AAO- Cu layers contain basically $\mathrm{Cu}^{0}$, $\mathrm{Cu}^{1+}$ and $\mathrm{Cu}^{2+}$ ions, whereas the combined AAO-Cu/ Ni films have shown predominance of $\mathrm{Cu}^{0}$ and $\mathrm{Cu}^{1+}$, and only traces of $\mathrm{Cu}^{2+}$. This fact confirms again the inferences made, regarding the appearance of a redox couple, which results in the reduction of the copper deposits in presence of Ni , demonstrated by Eqs. 3 5. The AC nickel incorporation has resulted in coincidence of the three $\mathrm{Ni}^{0}, \mathrm{Ni}^{2+}, \mathrm{Ni}^{3+}$ oxidation states, including $\mathrm{Ni}_{3} \mathrm{~S}_{2}$. This sulfide was the predominant compound in the combined $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}$ layers.

## 4. Conclusions

The present systematic study comprises the results of the comparative analyses performed on porous reference and modified AAO layers. The modifications were performed by means of AC -electrochemical Cu and/or Ni incorporation. Considering the wide potential application field of these films, it was important
to establish their durability in corrosive media. For that purpose, electrochemical measurements were performed in duplicate after 24 and 720 hours of exposure to a $3.5 \% \mathrm{NaCl}$ solution, resembling seawater. This approach has enabled to obtain reliable data for both the barrier ability and durability of the obtained films. The acquired EIS spectra reveal almost perfect overlapping of each sample couple from the respective groups and indistinguishable deviations between the respective sample groups. All EIS spectra were further analyzed by fitting them to a suitable simplified model equivalent circuit.
The spectra, acquired after the initial 24 hours of exposure have shown definitely capacitive character of all investigated samples, due to the contribution of the basic AAO matrix. In addition, the analyses of the EIS spectra have shown that the incorporated Cu and/ or Ni deposits on the AAO pore walls and bottoms are rather thin, evinced from the low efficiency of the deposition process. These metal deposits are also porous (or at least rather defective) and do not contribute to the dielectric properties of the basic AAO layer.
After 720 hours of exposure, no distinguishable changes in the spectra were registered, revealing the considerable durability of all the investigated films. The references did not show notable changes in their spectra, revealing that corrosion proceeds as a quasistationary process and does not change the properties of the AAO matrices. In the case of Cu -deposition, the resulting deposits do not have any protective properties, whereas Ni films had lost their protective abilities (detected at the beginning of the exposure), probably due to detaching from the basic oxide surface. Consequently, the Ni deposits form thicker films with lower adhesion to the AAO pore walls and bottoms, compared to the Cu ones. In the case of combined $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}$ layers, their deterioration is obviously caused by electrochemical interactions between the composing elements (i.e. Cu and Ni ).

The PDS curves confirmed the inferences made for the EIS measurements. The PDS results have revealed the exceptional barrier ability and durability of the AAO matrices and the insignificant contribution of the $\mathrm{Cu} / \mathrm{Ni}$ deposits, evinced from the rather low current densities and the almost horizontal anodic branches. Initially, the $E_{\text {corr }}$ values of the respective PDS curves reveal some differences (due to the more active Ni and the nobler Cu ). These dif-
ferences disappear after 720 hours of exposure. Their disappearance is a result of the complete extension of the insignificant contribution of the Cu and/or Ni thin films to the barrier properties of the basic AAO matrices.

The SEM images have confirmed the assumption for the deposition of very thin $\mathrm{Cu} / \mathrm{Ni}$ layers inside the AAO pores, since no change in the surface morphology was observed after the respective electrochemical metal deposition.

The EDX analyses have revealed that all the elements composing the modified AAO layers are completely equally distributed on the entire surface of the samples. Besides, the quantitative EDX point analyses have revealed several basic differences among the coating types: (i) The AAO layers are composed of almost pure $\mathrm{Al}_{2} \mathrm{O}_{3}$, where part of the oxygen is partially substituted with sulfur; (ii) The AC incorporations of single metals ( Cu and Ni ) result in the equal deposition of very low amounts of the respective metal; (iii) In the combined AAO-Cu/Ni coatings, the Cu content is three times higher, whereas the Ni one is twice lower, compared to the layers incorporated with a single metal; (iv) The contents of Al and S look lower in the case of the combined layers, compared to the rest, due to their coverage by thicker $\mathrm{Cu} /$ Ni mixed films on the AAO pores walls and bottoms. Besides, the higher oxygen content of the modified AAO layers reveals that the deposited Cu and Ni are in oxide forms.

The XPS spectra of all the investigated samples, have also shown that all elements, composing the modified AAO layers are in oxidized form (i.e. oxides and hydroxides in all possible oxidation states of Cu and Ni ). The AAO-Cu layers contain basically $\mathrm{Cu}^{0}, \mathrm{Cu}^{1+}$ and $\mathrm{Cu}^{2+}$ ions. In the case of AAO-Ni layers the incorporated metal was in the three $\mathrm{Ni}^{0}, \mathrm{Ni}^{2+}$, $\mathrm{Ni}^{3+}$ oxidation states, including $\mathrm{Ni}_{3} \mathrm{~S}_{2}$. Finally, the combined $\mathrm{AAO}-\mathrm{Cu} / \mathrm{Ni}$ films have shown predominance of $\mathrm{Cu}^{\circ}$ and $\mathrm{Cu}^{1+}$, and only traces of $\mathrm{Cu}^{2+}$, whereas the nickel was basically in form of $\mathrm{Ni}_{3} \mathrm{~S}_{2}$.

## Acknowledgement

The authors would like to express their gratitude to the Bulgarian National Scientific Fund for the financial support under contract No. КП-06-M 38/1 (2019).

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    DOI: https://doi.org/10.33961/jecst.2020.01235

