

# Performance of a Planar Leaky-Wave Slit Antenna for Different Values of Substrate Thickness

Niamat Hussain · Kam Eucharist Kedze · Ikmo Park\*

## Abstract

This paper presents the performance of a planar, low-profile, and wide-gain-bandwidth leaky-wave slit antenna in different thickness values of high-permittivity gallium arsenide substrates at terahertz frequencies. The proposed antenna designs consisted of a periodic array of  $5 \times 5$  metallic square patches and a planar feeding structure. The patch array was printed on the top side of the substrate, and the feeding structure, which is an open-ended leaky-wave slot line, was etched on the bottom side of the substrate. The antenna performed as a Fabry-Perot cavity antenna at high thickness levels ( $H=160 \mu\text{m}$  and  $H=80 \mu\text{m}$ ), thus exhibiting high gain but a narrow gain bandwidth. At low thickness levels ( $H=40 \mu\text{m}$  and  $H=20 \mu\text{m}$ ), it performed as a metasurface antenna and showed wide-gain-bandwidth characteristics with a low gain value. Aside from the advantage of achieving useful characteristics for different antennas by just changing the substrate thickness, the proposed antenna design exhibited a low profile, easy integration into circuit boards, and excellent low-cost mass production suitability.

**Key Words:** Leaky-Wave, Metasurface Antenna, Planar Antenna, Terahertz Antenna, Wide-Gain Bandwidth.

## I. INTRODUCTION

The terahertz (THz) regime, which spans the frequencies of 0.1–10 THz, is the least explored region of the electromagnetic spectrum. This regime is located between the microwave and the optical frequencies and has potential in emerging applications in sensing, imaging, and astronomy, among others. Its unique application in the screening of explosives, biohazards, and weapons and in envisioning concealed objects has also increased the worth of this band for researchers [1, 2]. Besides these applications, radiofrequency engineers suggest that the THz band can also be used to meet the demand of high data rates in wireless communication systems. This band offers many advantages, including extremely high data rate, wide bandwidths, better resolution,

and improved spatial directivity with system compactness [3].

Lens-coupled antennas are widely used in the THz regime because of their advantages of high gain, wide bandwidth, mechanical rigidity, and thermal stability. However, these antennas have their intrinsic drawbacks of bulky size and low radiation efficiency due to the excitation of surface modes that occurs, especially when the substrate thickness is comparable with the excitation signal wavelength [4–6].

Fabry-Perot cavity antennas have also been proposed for THz radiation because of their promising properties of high gain, low complexity, and stability of fabrication, but these antennas undergo design challenges involving a low 3-dB gain bandwidth, particularly antennas with high-permittivity substrates [7–10]. The electrically thick substrates in the THz frequency cause serious problems, such as substrate reso-

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nance, which can be eliminated by decreasing the substrate thickness up to  $\lambda_0/20$ , where  $\lambda_0$  is a free space wavelength [11]. In recent years, researchers have demonstrated many extraordinary properties of metasurface antennas [12–17] because of their potential to provide the novel characteristics of an ultra-low profile and enhanced performance in gain, radiation pattern, and bandwidth [18]. Metasurface antennas have their own intrinsic advantages of easy fabrication, low cost, light weight, and extreme flatness.

In this work, we studied the performance of a planar leaky-wave slit antenna in different substrate thickness values to obtain the advantages of both Fabry-Perot cavity antenna and metasurface antenna characteristics just by changing the substrate thickness. The antenna consists of an array of square patches and a planar leaky-wave slit feeding structure etched on both sides of a high-permittivity gallium arsenide (GaAs) substrate. The patches printed on the top side of the substrate are a bidirectional periodic array of square patches, and the center-fed planar feeding structure is printed on the bottom side of the substrate. The antenna is optimized at each value of the substrate thickness for an optimum wide-band gain bandwidth. This paper is organized as follows: the geometry and the modeling of the antenna are described in Section II. The characteristics of the antenna with respect to substrate thickness are discussed in Section III. The conclusions are presented in Section IV.

## II. ANTENNA GEOMETRY AND MODELING

The detailed geometry of the proposed antenna is shown in Fig. 1. The antenna was patterned on both sides of the GaAs substrate (dielectric constant of  $\epsilon_r = 12.9$ ). As the GaAs material has a high breakdown field and a short carrier lifetime along with reasonably good mobility, it is considered one of the most suitable materials for the fabrication of photoconductive antennas. The patch array, consisting of symmetric bidirectional  $5 \times 5$  metallic square patches, was patterned on the top side of the substrate. The width and the periodicity of the square patch array were defined as  $D$  and  $P$ , respectively. The feeding structure, an opened leaky-wave slit of width  $W_L$ , was etched on the bottom side of the substrate. The metallic layer used in the ground plane and the patch array had a thickness of  $0.35 \mu\text{m}$  and conductivity of  $1.6 \times 10^7 \text{ S/m}$ . The antenna had an overall dimension of  $A \times A \times H \mu\text{m}^3$ , where  $A$  is the lateral size and  $H$  is the thickness of the substrate. The slit was fed by a short dipole at its center, which has a gap and a width of  $g$  and  $W_d$ , respectively. The substrate thickness  $H$  values varied from  $20 \mu\text{m}$  to  $160 \mu\text{m}$ . The antenna was optimized for each value of  $H$  ( $H = 20,$

$40, 80, 160 \mu\text{m}$ ) by changing the periodicity and patch size while maintaining all the other design parameters. The optimized design parameters of the antenna to attain the optimum broadside gain and 3-dB gain bandwidth are summarized in Tables 1 and 2, respectively.

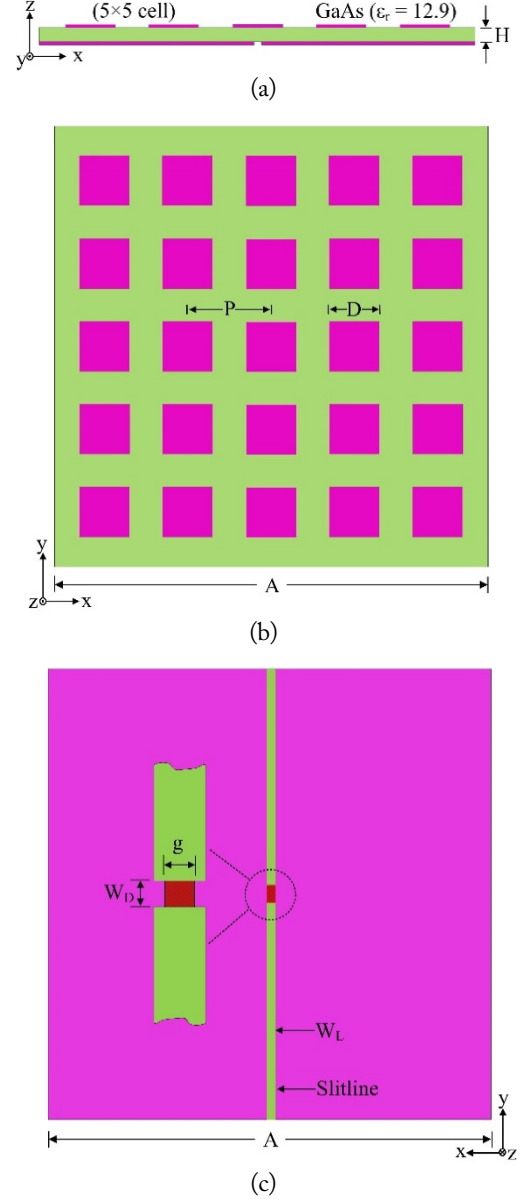


Fig. 1. Antenna geometry: (a) side view, (b) front view, and (c) bottom view.

Table 1. Common antenna design parameters

Parameter	Dimension ( $\mu\text{m}$ )
$A$	$5 \times P + D/2$
$W_L$	15
$W_D$	10
$g$	10

Table 2. Design parameters for different values of substrate thickness  $H$

Substrate thickness $H$ ( $\mu\text{m}$ )	$P$ ( $\mu\text{m}$ )	$D$ ( $\mu\text{m}$ )
160	330	190
80	330	195
40	340	200
20	360	210

### III. ANTENNA CHARACTERISTICS

We modeled the antenna structure and investigated the characteristics of the antenna using the commercial electromagnetic wave simulator CST Microwave Studio (CTS Computer Simulation Technology GmbH, Darmstadt, Germany) based on the finite integration time domain technique. The antenna was excited by the default Gaussian-shaped signal in the desired frequency range by placing a discrete port in the dipole gap at the center of the slit line.

Fig. 2 shows the gain characteristics of antennas at different substrate thickness values. As the thickness,  $H$ , of the substrate decreased from  $H = 160 \mu\text{m}$  to  $H = 20 \mu\text{m}$ , the gain response shifted to higher frequencies. In fact, the change in the substrate thickness changed the effective permittivity. Thus, the gain response shifted to lower or higher frequency as the substrate thickness increased or decreased, respectively.

The antenna performed as a Fabry-Perot cavity antenna at a high thickness range, exhibiting high gain with narrow gain-bandwidths. Conversely, the antenna performed as a metasurface antenna at a low thickness substrate range and showed wide-gain-bandwidth characteristics, but the gain decreased with decreasing thickness. At thickness levels of  $H = 160 \mu\text{m}$  and  $H = 80 \mu\text{m}$ , the antenna presented similar gain values of 13 dBi and 12.5 dBi, respectively. The 3-dB gain bandwidth was narrow at 2% and 4.8% with respect to their central frequencies of 0.316 THz and 0.332 THz at  $H = 160 \mu\text{m}$  and  $H = 80 \mu\text{m}$ , respectively. The antenna with a substrate thickness of  $H = 40 \mu\text{m}$  exhibited wideband and stable gain characteristics, with a value of 9.8 dBi, and the 3-dB gain bandwidth was greater than 16% (0.34–0.4 THz). The antenna gain was around 7 dBi, and the 3-dB gain bandwidth was approximately 8% (0.365–0.395 THz) for the antenna with  $H = 20 \mu\text{m}$ . These results indicate that antennas with thick substrates produce high gain values and are thus suitable for applications requiring high gain. Antennas with thin substrates, especially those where  $H = 40 \mu\text{m}$ , are good candidates for applications that demand a wide bandwidth with moderate gain.

The radiation efficiencies of the antennas are shown in Fig. 3.

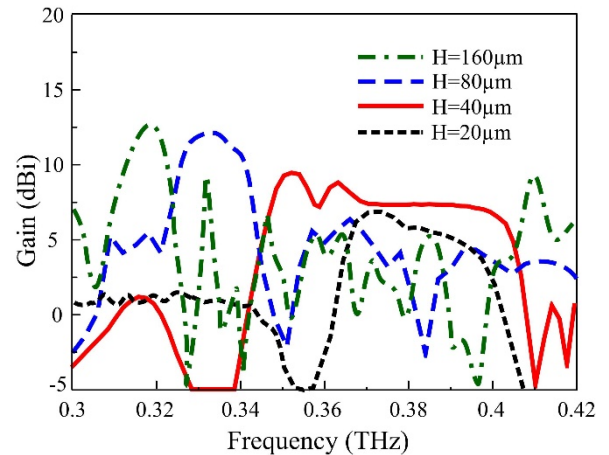


Fig. 2. Antenna gain as a function of the frequency for antennas for different values of  $H$ .

The antennas with thick substrates achieved high radiation efficiencies, which decreased for antennas with thin substrates. The maximum radiation efficiencies verified within the 3-dB gain bandwidth was approximately 75% for antennas with  $H = 160 \mu\text{m}$  and  $H = 80 \mu\text{m}$  thickness levels. This value decreased to approximately 69% and 60% at  $H = 40 \mu\text{m}$  and  $H = 20 \mu\text{m}$ , respectively. Note that although the radiation efficiency was high for thick substrates, the antenna gain dropped to zero at some specific frequencies (e.g., around 0.35 and 0.38 THz). In fact, the antenna radiated well but not in the boresight direction, in which the antenna gain was calculated. Thus, the measured gain dropped to zero, even though the radiation efficiency was high.

Fig. 4 presents the radiation patterns of the antennas at their central frequencies. In general, all the antennas showed clean profile patterns with low side-lobe levels and back radiation in both the  $xz$ - and  $yz$ -planes, and the gain increased with the increase in substrate thickness. Antennas with thick substrates produced similar directive radiation patterns, with

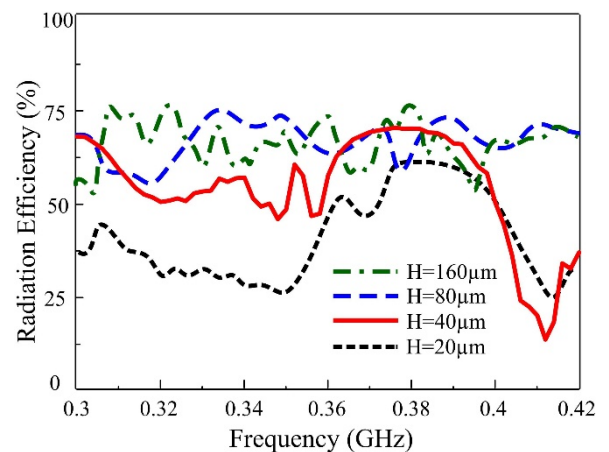


Fig. 3. Radiation efficiency as a function of the frequency for antennas for different values of  $H$ .

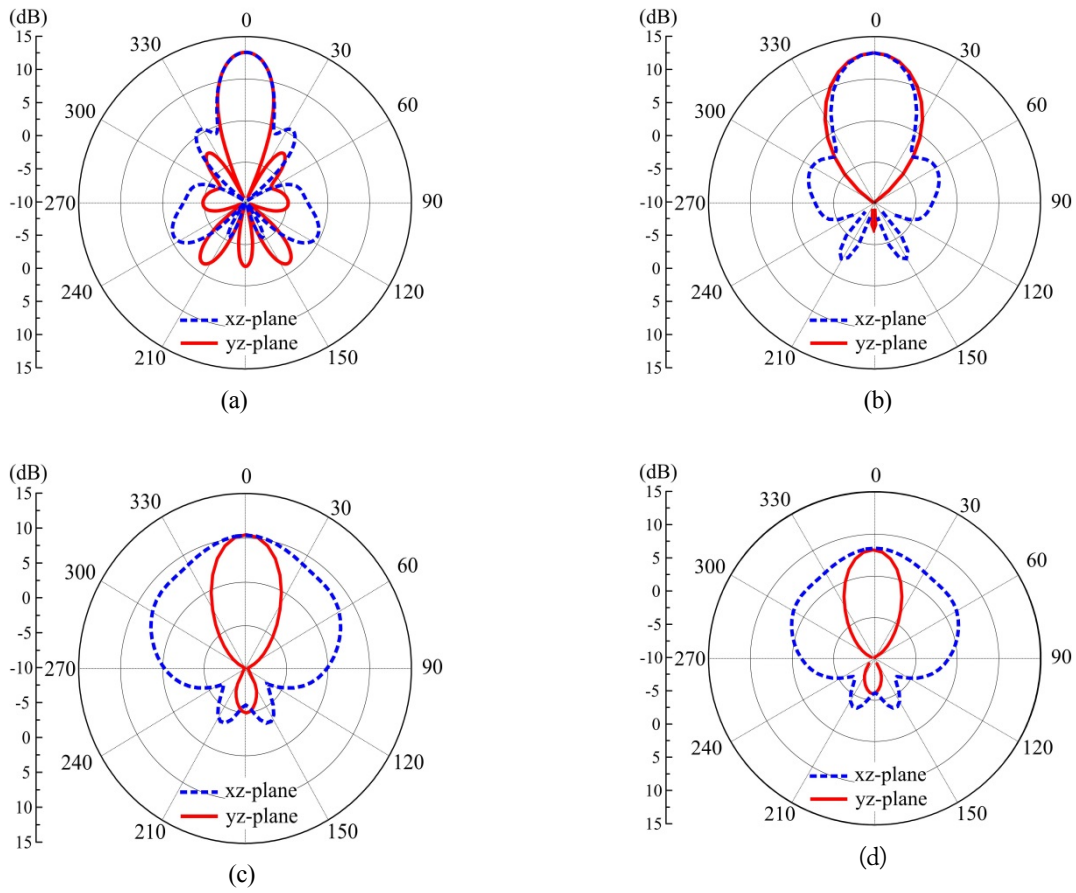


Fig. 4. Radiation patterns of the antennas: (a)  $H=160 \mu\text{m}$  at 0.316 THz, (b)  $H=80 \mu\text{m}$  at 0.332 THz, (c)  $H=40 \mu\text{m}$  at 0.37 THz, and (d)  $H=20 \mu\text{m}$  at 0.38 THz.

a narrow, half-power beamwidth (HPBW). The HPBWs were approximately  $12^\circ$  and  $15^\circ$  for antennas with substrates at  $H=160 \mu\text{m}$  and  $H=80 \mu\text{m}$ , respectively. An interesting phenomenon was observed for the antennas with thin substrates. The HPBW in the  $xz$ -plane increased while having a narrow HPBW in the  $yz$ -plane. The HPBWs in the  $xz$ -plane were  $140.5^\circ$  and  $130^\circ$  for  $H=40 \mu\text{m}$  and  $H=20$ , respectively. These values were around  $30^\circ$  in the  $yz$ -plane.

The surface current density in the patches was calculated to explain the radiation mechanism (Fig. 5). For thick values of the substrate, almost all of the patches were excited in all directions, producing symmetrical and directive radiation patterns with high gain values in both principal planes. In the case of the thin substrates, only the patches along the slit line were activated, and they had a strong current across the direction of the slit line ( $y$ -direction) that produced a strong field in the perpendicular direction. This outcome resulted in a wide beamwidth in the  $xz$ -plane, and the gain was limited because of the excitation of a few patches. Note that all the antennas showed low back radiation. Conventionally, the radiation pattern of the conventional slot in a thin substrate is bidirectional, and a back reflector is used to prevent this

situation. However, a back reflector is not necessary in the proposed antenna design that employs a metasurface because of the effective coupling of the electromagnetic wave to the patch array from the leaky-wave slit feed. This coupling resulted in low back radiations.

#### IV. CONCLUSIONS

The characteristics of planar compact antennas with different substrate thicknesses were studied across the THz frequency range. Each antenna consisted of a square patch array of  $5 \times 5$  and a planar feeding structure, both of which were patterned on a high-permittivity GaAs substrate. The antenna with a narrow 3-dB gain bandwidth at thick ( $H=160 \mu\text{m}$  and  $H=80 \mu\text{m}$ ) values of substrate exhibited high gain. The antenna with thin substrates ( $H=40 \mu\text{m}$  and  $H=20 \mu\text{m}$ ) produced low gain values but wide 3-dB gain-bandwidths. Therefore, the design enables the antenna to be adjusted for specific applications of high gain or wide-gain-bandwidth with moderate gain by simply changing the substrate thickness. Moreover, the antenna design provides a compact size, mechanical robustness, easy integration into circuit boards,

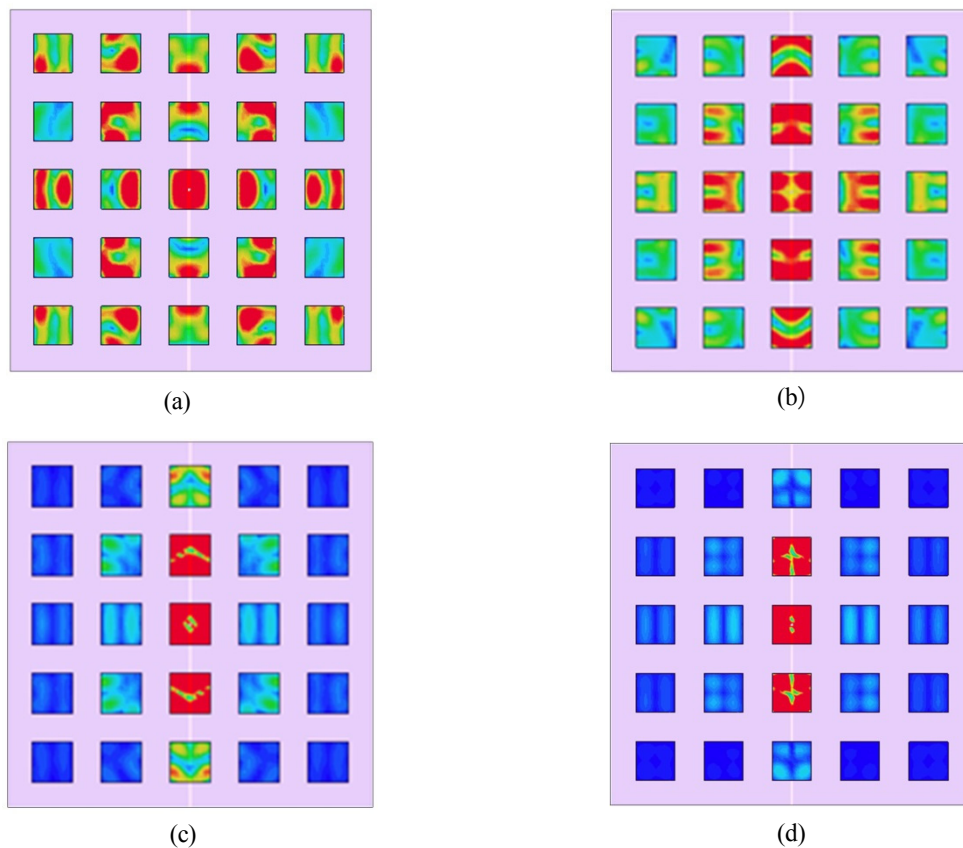


Fig. 5. Surface current density on the patch array of the antenna at (a)  $H=160 \mu\text{m}$ , (b)  $H=80 \mu\text{m}$ , (c)  $H=40 \mu\text{m}$ , and (d)  $H=20 \mu\text{m}$ .

and low-cost mass production suitability, which make the antenna a good candidate for applications in the THz frequency.

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