

불확실 유체 역학 계수를 가진 대형급 무인잠수정의 강인 경로점 추적

Robust Waypoint Tracking of Large Diameter Unmanned Underwater Vehicles with Uncertain Hydrodynamic Coefficients

김도완† · 박정훈* · 박호규* · 김태영*

(Do Wan Kim · Jeong-Hoon Park · Ho-Gyu Park · Tae-Yeong Kim)

Abstract - This paper addresses on an linear matrix inequality (LMI) formulation of the robust waypoint tracking problem of large diameter unmanned underwater vehicles (LDUUVs) in the horizontal plane. The interested design issue can be reformed as the robust asymptotic stabilization of the provided error dynamics with respect to the desired yaw angle, surge speed and attitude. Sufficient conditions for its robust asymptotic stabilizability against the hydrodynamic uncertainties are derived in the format of LMI. An example is provided to testify the validity of the proposed theoretical claims.

Key Words : Large diameter unmanned underwater vehicles (LDUUV), Uncertainty, robust, Lyapunov, Linear matrix inequality (LMI), Waypoint, Asymptotic stability.

1. Introduction

Recently, several techniques involving the control of unmanned underwater vehicles (UUVs) have been proposed in [1]-[7], which are based on their mathematical model. The mathematical model contains hydrodynamic forces and moments expressed in terms of a set of hydrodynamic coefficients [13]. These hydrodynamic coefficients are usually empirically determined, and thereby its exact estimation is virtually impossible. From this reason, the robust control of uncertain UUVs is one of the most important research issues. However, unfortunately, there is still a lack in design methods based on linear matrix inequality (LMI) for uncertain UUVs.

The objective of this study is to present an LMI-based design methodology for the horizontal waypoint tracking control of a class of large diameter UUVs (LDUUVs) with the hydrodynamic uncertainties while keeping its the desired surge speed and attitude. The proposed approach is an extension of [7] to uncertain LDUUVs. The concerned problem can be viewed as the robust asymptotic stabilization of the uncertain error dynamics in terms of the desired yaw angle, surge speed, and attitude. It is shown that two control inputs of uncertain LDUUVs, the rudder angles and the propeller thrust can be separately designed. Finally, sufficient

LMI conditions for the robust asymptotic stabilization of uncertain LDUUVs are provided in the sense of Lyapunov stability criterion.

Notations : The relation $P > Q$ ($P < Q$) means that the matrix $P - Q$ is positive (negative) definite. $\lambda_{\max}(A)$ ($\lambda_{\min}(A)$) is the maximum (minimum) eigenvalue of matrix A . $A_{(i)}$ denotes i th row of the matrix A . $Sym\{S\}$ is defined as $S^T + S$. B_{Δ_n} indicates the ball $\{\eta : \|\eta\| \leq \Delta_n\}$ with $\Delta_n \in \mathbb{R}_{>0}$. \mathcal{J}_m indicates the integer set $\{1, \dots, m\}$. Symbol $*$ denotes a transposed element in a symmetric position.

2. Preliminaries

Consider a class of LDUUVs [8]-[10] with uncertain hydrodynamic coefficients described by the horizontal model

$$\dot{\eta} = J(\psi)\phi \quad (1)$$

$$M\dot{\phi} + (f(\phi) + \Delta f(\phi))\phi = \tau + \Delta\tau \quad (2)$$

where $\eta = [x \ y \ \psi]^T \in \mathbb{R}^3$, $\phi = [u \ v \ r]^T \in \mathbb{R}^3$, (x, y) is the inertial coordinates of the center of mass, ψ is the yaw angle, u and v are the surge and the sway velocities, respectively, and r is the angular velocity in yaw, $J \in \mathbb{R}^{3 \times 3}$ is a frame transformation, $M \in \mathbb{R}^{3 \times 3}$ includes mass and hydrodynamic added mass terms and $f(\phi)\phi \in \mathbb{R}^3$ captures Coriolis-centripetal matrices including the added mass and a damping matrix, τ is the control actuator forces with the propeller thrust ξ , and δ_i , $i \in \mathcal{J}_4$ is the rudder angles, and

† Corresponding Author : Dept. of Electrical Engineering, Hanbat National University, Korea
E-mail: dowankim@hanbat.ac.kr

* Maritime R&D Center, LIG Nex1 Co., Ltd.

Received : January 12, 2017; Accepted : January 25, 2017

Δf and $\Delta \tau$ are uncertainties. In detail, the terms J , M , f , Δf , τ , and $\Delta \tau$ are given by

$$J = \begin{bmatrix} \cos(\psi) - \sin(\psi) & 0 \\ \sin(\psi) & \cos(\psi) & 0 \\ 0 & 0 & 1 \end{bmatrix}, \quad M = \begin{bmatrix} m_1 & 0 & 0 \\ 0 & m_2 & m_3 \\ 0 & m_4 & m_5 \end{bmatrix}$$

$$f = \begin{bmatrix} -X_{uu}u & -X_{vv}v & -mv - mx_g r - X_{rr}r \\ 0 & -Y_v - Y_{v|v}|v| & mu - Y_r - Y_{r|r}|r| \\ 0 & -N_v - N_{v|v}|v| & mx_g u - N_r - N_{r|r}|r| \end{bmatrix}$$

$$\Delta f = \begin{bmatrix} 0 & 0 & 0 \\ 0 - \Delta Y_v - \Delta Y_{v|v}|v| & -\Delta Y_r - \Delta Y_{r|r}|r| \\ 0 - \Delta N_v - \Delta N_{v|v}|v| & -\Delta N_r - \Delta N_{r|r}|r| \end{bmatrix}$$

$$\tau = \begin{bmatrix} \xi + X_{uu\delta\delta} u^2 \sum_{i=1}^4 \delta_i^2 \\ u^2 \sum_{i=1}^4 Y_{uu\delta_i} \delta_i \\ u^2 \sum_{i=1}^4 N_{uu\delta_i} \delta_i \end{bmatrix} \in \mathbb{R}^3, \quad \Delta \tau = \begin{bmatrix} 0 \\ u^2 \sum_{i=1}^4 \Delta Y_{uu\delta_i} \delta_i \\ u^2 \sum_{i=1}^4 \Delta N_{uu\delta_i} \delta_i \end{bmatrix} \in \mathbb{R}^3.$$

where $m_1 = m - X_u$, $m_2 = m - Y_v$, $m_3 = mx_g - Y_r$, $m_4 = mx_g - N_v$, $m_5 = I_{zz} - N_r$, m is the vehicle mass, x_g is the x -position of the center of gravity, I_{zz} is the mass moment of inertia term, X_{uu} , X_{vv} , X_{rr} , Y_v , $Y_{v|v}$, Y_r , $Y_{r|r}$, N_v , $N_{v|v}$, N_r , $N_{r|r}$, $X_{uu\delta\delta}$, $Y_{uu\delta_i}$, and $N_{uu\delta_i}$ are the hydrodynamic coefficients, and ΔY_v , $\Delta Y_{v|v}$, ΔY_r , $\Delta Y_{r|r}$, ΔN_v , $\Delta N_{v|v}$, ΔN_r , $\Delta N_{r|r}$, $\Delta Y_{uu\delta_i}$ and $\Delta N_{uu\delta_i}$ are considered as the time-varying hydrodynamic uncertainties. The related coefficients in (1) and (2) are listed in Appendix 1.

Assumption 1: There exist the known constant D_\star and the unknown time-varying function F_\star satisfying $\|F_\star\| \leq 1$ for $\star \in \{Y_v, Y_{v|v}, Y_r, Y_{r|r}, N_v, N_{v|v}, N_r, N_{r|r}, X_{uu\delta\delta}, Y_{uu\delta_i}, N_{uu\delta_i}\}$ such that

$$\Delta \star = D_\star F_\star \star.$$

For example, $\Delta Y_v = D_{Y_v} F_{Y_v} X_{Y_v}$.

Problem 1: Consider uncertain LDUUV (1) and (2). Suppose that the criteria for updating the waypoint is to shift from (x_{dk}, y_{dk}) to $(x_{d(k+1)}, y_{d(k+1)})$ when $\| [e_{xk} \ e_{yk}]^T \| \leq \rho$, where (x_{dk}, y_{dk}) , $k \in \mathcal{J}_{n_w}$ is the k th given waypoint, $e_{xk} = x - x_{dk}$, and $e_{yk} = y - y_{dk}$. Then, given the desired constant surge velocity $u_d \in \mathbb{R}_{>0}$ and the desired line of sight (LOS) to be the horizontal plane angle defined as

$$\psi_d = \tan^{-1} \frac{e_y}{e_x} \quad (3)$$

design ξ and δ_i , $i \in \mathcal{J}_4$ such that $\|e_u\|$, $\|e_\psi\|$, $\|v\|$, and $\|r\|$ robustly asymptotically converge to zero against the

hydrodynamic uncertainties, where $e_u = u - u_d$ and $e_\psi = \psi - \psi_d$.

3. Main Results

Before proceeding to our main results, the following propositions and the lemmas will be needed throughout the proof:

Proposition 1: Consider (1) and (2). Define $\chi := [e_\psi \ v \ r]^T \in \mathbb{R}^3$, $e_{xy} := [e_x \ e_y]^T \in \mathbb{R}^2$, and $\delta := [\delta_1 \ \delta_2 \ \delta_3 \ \delta_4]^T \in \mathbb{R}^4$. An augmented error system can be represented by

$$\begin{bmatrix} \dot{\chi} \\ \dot{e}_u \end{bmatrix} = \begin{bmatrix} F_1(\chi, e_{xy}) + \Delta F_1(v, r) & F_2(e_\psi, e_{xy}, r, e_u, \delta) + \Delta F_2(e_u, \delta) \\ F_3(v, r) & F_4(e_u, \delta) \end{bmatrix} \begin{bmatrix} \chi \\ e_u \end{bmatrix} + \begin{bmatrix} 0 \\ F_5(\delta) \end{bmatrix} + \begin{bmatrix} G + \Delta G & 0 \\ 0 & \frac{1}{m_1} \end{bmatrix} \begin{bmatrix} \delta \\ \xi \end{bmatrix} \quad (4)$$

where F_1 , ΔF_1 , F_2 , ΔF_2 , F_3 , F_4 , F_5 , G , and ΔG are given in Appendix 2.

Proof: Using $\dot{e}_\psi = \dot{\psi} - \dot{\psi}_d$, (1), (2), and (3), we have

$$\dot{e}_\psi = \frac{u_d \sin e_\psi}{\|e_{xy}\|} + \frac{\cos e_\psi}{\|e_{xy}\|} v + r + \frac{\sin e_\psi}{\|e_{xy}\|} e_u$$

(see [7] for more details). It follows from (2) and $\dot{e}_u = \dot{u}$ that

$$\begin{bmatrix} \dot{v} \\ \dot{r} \end{bmatrix} = \begin{bmatrix} m_2 & m_3 \\ m_4 & m_5 \end{bmatrix}^{-1} \begin{bmatrix} Y_v + Y_{v|v}|v| & -m(e_u + u_d) + Y_r + Y_{r|r}|r| \\ N_v + N_{v|v}|v| & -mx_g(e_u + u_d) + N_r + N_{r|r}|r| \end{bmatrix} \begin{bmatrix} v \\ r \end{bmatrix} + \begin{bmatrix} m_2 & m_3 \\ m_4 & m_5 \end{bmatrix}^{-1} \begin{bmatrix} \Delta Y_v + \Delta Y_{v|v}|v| & \Delta Y_r + \Delta Y_{r|r}|r| \\ \Delta N_v + \Delta N_{v|v}|v| & \Delta N_r + \Delta N_{r|r}|r| \end{bmatrix} \begin{bmatrix} v \\ r \end{bmatrix} + \begin{bmatrix} m_2 & m_3 \\ m_4 & m_5 \end{bmatrix}^{-1} \begin{bmatrix} (e_u^2 + 2u_d e_u + u_d^2) \sum_{i=1}^4 Y_{uu\delta_i} \delta_i \\ (e_u^2 + 2u_d e_u + u_d^2) \sum_{i=1}^4 N_{uu\delta_i} \delta_i \end{bmatrix} + \begin{bmatrix} m_2 & m_3 \\ m_4 & m_5 \end{bmatrix}^{-1} \begin{bmatrix} (e_u^2 + 2u_d e_u + u_d^2) \sum_{i=1}^4 \Delta Y_{uu\delta_i} \delta_i \\ (e_u^2 + 2u_d e_u + u_d^2) \sum_{i=1}^4 \Delta N_{uu\delta_i} \delta_i \end{bmatrix}$$

and

$$\dot{e}_u = \frac{1}{m_1} (X_{uu} e_u^2 + 2X_{uu} e_u u_d + X_{uu} u_d^2 + X_{vv} v^2 + mvr + mx_g r^2 + X_{rr} r^2 + \xi + X_{uu\delta\delta} (e_u^2 + 2u_d e_u + u_d^2) \sum_{i=1}^4 \delta_i^2).$$

Taking the change of variables with $[\chi, e_u]^T$ results in (4). ■

Proposition 2: Consider (4) together with

$$\delta = K\chi \quad (5)$$

$$\xi = -m_1 F_3(v, r)\chi - m_1 F_4(e_u, \delta)e_u - m_1 F_5(\delta) - m_1 \gamma e_u \quad (6)$$

where K is the controller gains to be determined and $\gamma \in \mathfrak{R}_{>0}$. Then the closed-loop system becomes

$$\Sigma_1: \dot{\chi} = (F_1(\chi, e_{xy}) + \Delta F_1(v, r) + (G + \Delta G)K)\chi + (F_2(e_\psi, e_{xy}, r, e_u, \delta) + \Delta F_2(e_u, \delta))e_u \quad (7)$$

$$\Sigma_2: \dot{e}_u = -\gamma e_u. \quad (8)$$

Proof: By substituting (5) and (6) into (4), we have (7) and (8). ■

Proposition 3: It is true that

$$F_1(e_\psi, e_x, e_y, v, r) = \sum_{i_1=1}^2 \sum_{i_2=1}^2 \sum_{i_3=1}^2 \sum_{i_4=1}^2 \theta_{1i_1} \theta_{2i_2} \theta_{3i_3} \theta_{4i_4} A_{i_1 i_2 i_3 i_4}$$

$$\Delta F_1(v, r) = \sum_{i_3=1}^2 \sum_{i_4=1}^2 \theta_{3i_3} \theta_{4i_4} D_{\Delta F_1} F_{\Delta F_1} \tilde{A}_{i_3 i_4}$$

$$\Delta G = D_{\Delta G} F_{\Delta G} \tilde{G}$$

on $B_v \times B_r$, where $\theta_{1i_1}, \theta_{2i_2}, \theta_{3i_3}, \theta_{4i_4}, A_{i_1 i_2 i_3 i_4}, D_{\Delta F_1}, F_{\Delta F_1}, \tilde{A}_{i_3 i_4}, D_{\Delta G}, F_{\Delta G}$ and \tilde{G} are given in Appendix 3.

Proof: The proof directly follows from Assumption 1, [Theorem 2, 7], and the sector nonlinearity methodology [11]. ■

Lemma 1 [12]: Given constant matrices D and X , a time-varying matrix F satisfying $F^T(t)F(t) \leq I$ for all $t \in \mathfrak{R}_{>0}$, and $A = A^T$ of appropriate dimensions, the following equivalence

$$A + \text{sym}\{DFX\} < 0 \Leftrightarrow A + \epsilon DD^T + \epsilon^{-1} X^T X < 0$$

holds for some $\epsilon \in \mathfrak{R}_{>0}$.

Lemma 2: There exists $\zeta \in \mathfrak{R}_{>0}$ such that

$$\|F_2(e_\psi, e_{xy}, r, e_u, \delta) + \Delta F_2(e_u, \delta)\| \leq \zeta$$

on $B_r \times B_{\delta_1} \times B_{\delta_2} \times B_{\delta_3} \times B_{\delta_4}$.

Proof: Under Assumption 1, $F_2 + \Delta F_2$ satisfies

$$\|F_2 + \Delta F_2\| \leq \|E^{-1}\| \left\| \begin{bmatrix} 1/\rho \\ m\Delta_r + |e_u + 2u_d| \sum_{i=1}^4 (1 + |D_{Y_{u\delta_i}}|) |Y_{u\delta_i}| \Delta_{\delta_i} \\ mx_g \Delta_r + |e_u + 2u_d| \sum_{i=1}^4 (1 + |D_{N_{u\delta_i}}|) |N_{u\delta_i}| \Delta_{\delta_i} \end{bmatrix} \right\|$$

on $B_r \times B_{\delta_1} \times B_{\delta_2} \times B_{\delta_3} \times B_{\delta_4}$. ■

Theorem 1: Consider (1) and (2) under (5) and (6). Let $\Omega := \{[\chi e_u]^T \in \mathbb{R}^4: \chi^T P \chi + \alpha e_u^2 < 1\}$ with $P = P^T > 0$ and $\alpha \in \mathfrak{R}_{>0}$. Suppose that there exist $\tilde{P} = \tilde{P}^T > 0, \tilde{K}, \epsilon_1 \in \mathfrak{R}_{>0}$, and $\epsilon_2 \in \mathfrak{R}_{>0}$ such that

$$\begin{bmatrix} \left(\begin{array}{c} \text{Sym}\{A_{i_1 i_2 i_3 i_4} \tilde{P} + \tilde{G} \tilde{K}\} \\ + \epsilon_1 D_{\Delta F_1} D_{\Delta F_1}^T + \epsilon_2 D_{\Delta G} D_{\Delta G}^T \end{array} \right) * & * \\ \tilde{A}_{i_3 i_4} \tilde{P} & -\epsilon_1 I * \\ \tilde{G} \tilde{K} & 0 - \epsilon_2 I \end{bmatrix} < 0 \quad (9)$$

$$E_v \tilde{P} E_v^T < \Delta_v^2 \quad (10)$$

$$E_r \tilde{P} E_r^T < \Delta_r^2 \quad (11)$$

$$\begin{bmatrix} \Delta_{\delta_i}^2 & \tilde{K}_{(i)} \\ \tilde{K}_{(i)}^T & -\tilde{P} \end{bmatrix} < 0 \quad (12)$$

for all $(i_1, i_2, i_3, i_4, i) \in \mathcal{J}_2 \times \mathcal{J}_2 \times \mathcal{J}_2 \times \mathcal{J}_2 \times \mathcal{J}_4$, where $E_v = [010]$ and $E_r = [001]$. Then, for $C\{\chi(t_0), e_u(t_0)\} \in \Omega$, the closed-loop system of (1) and (2) under (5) and (6) is robustly asymptotically stable. In this feasible case, $P = \tilde{P}^{-1}$ and $K = \tilde{K} \tilde{P}^{-1}$.

Proof: Consider a Lyapunov function $V(\chi, e_u) = \chi^T P \chi + \alpha e_u^2$ for the closed-loop system (1), (2), (5), and (6). From Propositions 1, 2, and 3, we can see that

$$\begin{aligned} \dot{V}_{(1),(2),(5),(6)} &= \text{Sym}\{\chi^T P (F_1(\chi, e_{xy}) + \Delta F_1(v, r) + (G + \Delta G)K)\chi\} \\ &\quad + 2\chi^T P (F_2(e_\psi, e_{xy}, r, e_u, \delta) + \Delta F_2(e_u, \delta))e_u - 2\alpha\gamma e_u^2 \\ &= \sum_{i_1=1}^2 \sum_{i_2=1}^2 \sum_{i_3=1}^2 \sum_{i_4=1}^2 \theta_{1i_1} \theta_{2i_2} \theta_{3i_3} \theta_{4i_4} \\ &\quad \times (\text{Sym}\{\chi^T P (A_{i_1 i_2 i_3 i_4} + \tilde{G} \tilde{K})\chi\} \\ &\quad + \text{Sym}\{\chi^T P (D_{\Delta F_1} F_{\Delta F_1} \tilde{A}_{i_3 i_4} + D_{\Delta G} F_{\Delta G} \tilde{G} \tilde{K})\chi\}) \\ &\quad + 2\chi^T P (F_2(e_\psi, e_{xy}) \end{aligned}$$

Note that from Lemma 1,

$$\begin{aligned} &\text{Sym}\{P(A_{i_1 i_2 i_3 i_4} + \tilde{G} \tilde{K}) + P(D_{\Delta F_1} F_{\Delta F_1} \tilde{A}_{i_3 i_4} + D_{\Delta G} F_{\Delta G} \tilde{G} \tilde{K})\} < 0 \\ &\Leftrightarrow \text{Sym}\{P(A_{i_1 i_2 i_3 i_4} + \tilde{G} \tilde{K})\} + \epsilon_1 P D_{\Delta F_1} D_{\Delta F_1}^T P + \epsilon_1^{-1} \tilde{A}_{i_3 i_4}^T \tilde{A}_{i_3 i_4} \\ &\quad + \epsilon_2 P D_{\Delta G} D_{\Delta G}^T P + \epsilon_2^{-1} (\tilde{G} \tilde{K})^T \tilde{G} \tilde{K} < 0 \\ &\Leftrightarrow \text{LMI (9)} \end{aligned}$$

Then, by using from Lemma 2, it can be shown that there exists $Q = Q^T > 0$ such that

$$\begin{aligned} V_{(1),(2),(5),(6)} &< -\lambda_{\min}(Q) \|\chi\|^2 - 2\alpha\gamma e_u^2 + 2\zeta \|P\| \|\chi\| |e_u| \\ &= \begin{bmatrix} \|\chi\| \\ |e_u| \end{bmatrix}^T \begin{bmatrix} -\lambda_{\min}(Q) & \zeta \\ \zeta & -2\alpha\gamma \end{bmatrix} \begin{bmatrix} \|\chi\| \\ |e_u| \end{bmatrix} \end{aligned}$$

on $B_v \times B_r \times B_{\delta_1} \times B_{\delta_2} \times B_{\delta_3} \times B_{\delta_4}$. From the fact that

$$\begin{bmatrix} -\lambda_{\min}(Q)\zeta\|P\| & \\ \zeta\|P\| & -2\alpha\gamma \end{bmatrix} < 0 \Leftrightarrow \begin{cases} \frac{\zeta^2\|P\|^2}{2\alpha\gamma} - \lambda_{\min}(Q) < 0 \\ 2\alpha\gamma > 0 \end{cases}$$

by Schur complement, choosing $\alpha \in \mathfrak{R} > \frac{\zeta^2\|P\|^2}{2\gamma\lambda_{\min}(Q)}$ implies that the closed-loop system (1), (2), (5), and (6) is robustly asymptotically stable. Also, it is not hard to see that by Schur complement, LMI (10), (11), (12) $\Rightarrow \Omega \subset B_v \times B_r \times B_{\delta_1} \times B_{\delta_2} \times B_{\delta_3} \times B_{\delta_4}$. Therefore, if LMIs (9), (10), (11), and (12) hold, then the robust asymptotic stability of the closed-loop system of (1), (2), (5), (6) is guaranteed for $C\{\chi(t_0), e_u(t_0)\} \in \Omega$. ■

Remark 1: If $D_{\Delta F_1} = D_{\Delta G} =: D$ and $F_{\Delta F_1} = F_{\Delta G} =: F$, LMI (9) becomes

$$\begin{bmatrix} \text{Sym}\{A_{i_1, i_2, i_3, i_4} \tilde{P} + G\tilde{K}\} + \epsilon D^T D & * & * \\ \tilde{A}_{i_1, i_2, i_3, i_4} \tilde{P} + \tilde{G}\tilde{K} & -\epsilon I & * \end{bmatrix} < 0$$

for some $\epsilon \in \mathfrak{R}_{>0}$ and $(i_1, i_2, i_3, i_4) \in \mathcal{J}_2 \times \mathcal{J}_2 \times \mathcal{J}_2 \times \mathcal{J}_2$.

4. An Example

For the given $u_d = 3$, $\rho = 2$, and

$$(x_{dk}, y_{dk}) = \left(100 \sin \frac{2\pi(k-1)}{60} + 100, 100 \cos \frac{2\pi(k-1)}{60} + 100 \right)$$

on $k \in \mathcal{I}_{61}$, our goal is to determine K in (5) so that $\|e_u\|$, $\|e_\psi\|$, $\|v\|$, and $\|r\|$ of uncertain LDUUV (1) and (2) under (5) and (6) with $\gamma = 10$ robustly asymptotically converge to zero. Suppose that $\Delta_v = 10$, $\Delta_r = 1$, $\Delta_{\delta_i} = 0.2374$, $i \in \mathcal{J}_4$,

$$D_{\Delta F_1} = D_{\Delta G} = 0.03 \times E^{-1} \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 1 & 1 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 1 & 1 & 1 & 1 \end{bmatrix}$$

and

$$F_{\Delta F_1} = F_{\Delta G} = \text{diag}\{F, F, F, F, F, F, F, F\}$$

in which $\|F(t)\| < 1$. Then, solving LMIs (9), (10), (11), and (12) in Theorem 1 based on Remark 1 results in

$$P = 10^7 \times \begin{bmatrix} 8.7092 & 1.7694 & 3.7088 \\ 1.7694 & 0.3723 & 0.7709 \\ 3.7088 & 0.7709 & 1.6062 \end{bmatrix}$$

$$K = 10^3 \times \begin{bmatrix} -2.1302 & -0.4317 & -0.9118 \\ 1.7068 & 0.3450 & 0.7266 \\ 2.1445 & 0.4353 & 0.9158 \\ -2.1520 & -0.4369 & -0.9202 \end{bmatrix}$$

Figs. 1-5 demonstrates the robust waypoint tracking results when $(x(0), y(0), \psi(0), u(0), v(0), r(0)) = (0, 200, 0, 3, 0, 0)$ and

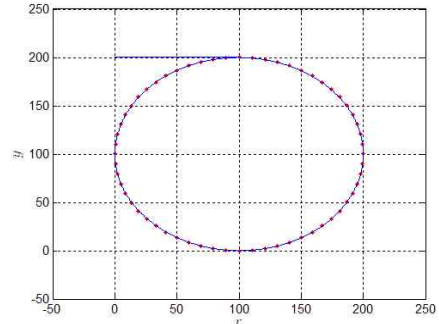


Fig. 1 The trajectories of (x, y) ('·': the desired waypoint).

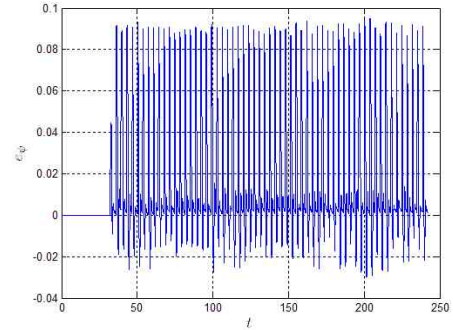


Fig. 2 The time response of e_ψ .

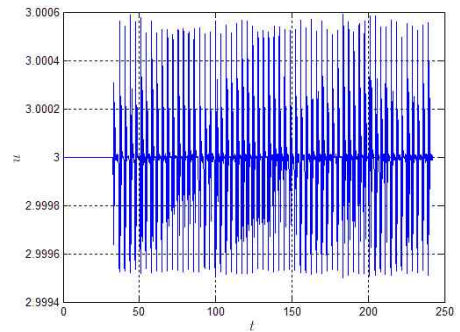


Fig. 3 The time response of u .

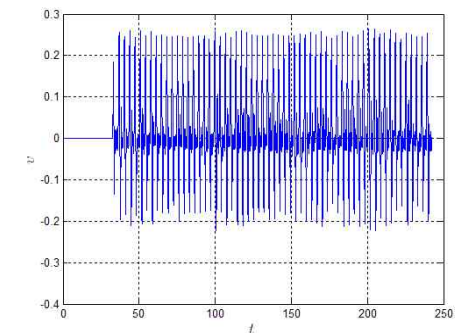


Fig. 4 The time response of v .

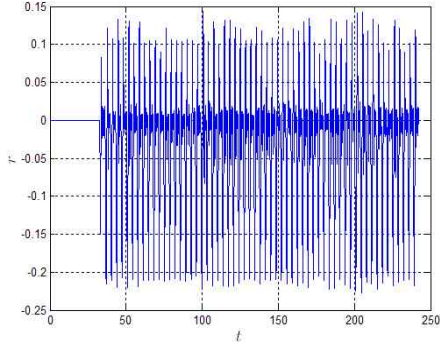


Fig. 5 The time response of r .

$|\delta_i| < 0.2374$. As shown in these figures, the LDUUV (1) and (2) under (5) and (6) successfully tracks all waypoints while keeping the desired surge speed u_d and its attitude.

4. Conclusions

This paper has proposed an LMI formulation of robust waypoint tracking problem for a class of uncertain LDUUVs while keeping its surge speed and attitude. Differently from the prior LMI approach [7], the proposed approach incorporates uncertainties on the hydrodynamic coefficients into design. The theoretical claims has been successfully verified in the given numerical example.

Appendix 1

This paper uses the following hydrodynamic coefficients, obtained by CFD and empirical formulations, of LIG Nex1 LDUUV model:

$$\begin{aligned}
 m &= 7500, I_{zz} = 27081.3, x_g = 0, L = 6.5, u_d = 3, X_u = -157.7122 \\
 X_{uu} &= -62.0022, X_{vv} = 515.6301, X_{rr} = -5.6269 \times 10^3 \\
 X_{uu\delta\delta} &= -228.0492, Y_v = -2.8612 \times 10^3, Y_r = 417.3126 \\
 Y_v &= -2.9887 \times 10^3, Y_{v|v} = -3.1868 \times 10^3, Y_r = 2.7937 \times 10^4 \\
 Y_{r|r} &= -1.3259 \times 10^3, Y_{uu\delta_1} = -591.0686, Y_{uu\delta_2} = 591.0686 \\
 Y_{uu\delta_3} &= 591.0686, Y_{uu\delta_4} = -591.0686, N_v = 417.3126 \\
 N_r &= -9.0809 \times 10^3, N_v = -1.1884 \times 10^4, N_{v|v} = 6.9397 \times 10^3 \\
 N_r &= -2.1449 \times 10^4, N_{r|r} = -1.7355 \times 10^4, N_{uu\delta_1} = 1.4740 \times 10^3 \\
 N_{uu\delta_2} &= -1.4740 \times 10^3, N_{uu\delta_3} = -1.4740 \times 10^3, \\
 N_{uu\delta_4} &= 1.4740 \times 10^3.
 \end{aligned}$$

Appendix 2

$$F_1 = E^{-1} \begin{bmatrix} \frac{u_d \sin e_\psi}{e_\psi \|e_{xy}\|} & \frac{\cos e_\psi}{\|e_{xy}\|} & 1 \\ 0 & Y_v + Y_{v|v}|v| & \begin{pmatrix} -mu_d + Y_r \\ + Y_{r|r}|r| \end{pmatrix} \\ 0 & N_v + N_{v|v}|v| & \begin{pmatrix} -m_x g u_d + N_r \\ + N_{r|r}|r| \end{pmatrix} \end{bmatrix}$$

$$\Delta F_1 = E^{-1} \begin{bmatrix} 0 & 0 & 0 \\ 0 \Delta Y_v + \Delta Y_{v|v}|v| & \Delta Y_r + \Delta Y_{r|r}|r| \\ 0 \Delta N_v + \Delta N_{v|v}|v| & \Delta N_r + \Delta N_{r|r}|r| \end{bmatrix}$$

$$F_2 = E^{-1} \begin{bmatrix} \frac{\sin e_\psi}{\|e_{xy}\|} \\ -mr + (e_u + 2u_d) \sum_{i=1}^4 Y_{uu\delta_i} \delta_i \\ -m_x g r + (e_u + 2u_d) \sum_{i=1}^4 N_{uu\delta_i} \delta_i \end{bmatrix}$$

$$\Delta F_2 = E^{-1} \begin{bmatrix} 0 \\ (e_u + 2u_d) \sum_{i=1}^4 \Delta Y_{uu\delta_i} \delta_i \\ (e_u + 2u_d) \sum_{i=1}^4 \Delta N_{uu\delta_i} \delta_i \end{bmatrix}$$

$$F_3 = \frac{1}{m_1} [0 \quad X_{vv}v \quad mv + m_x g r + X_{rr}r]$$

$$F_4 = \frac{1}{m_1} (X_{uu}e_u + 2X_{uu}u_d + X_{uu\delta\delta}(e_u + 2u_d)\sum_{i=1}^4 \delta_i^2)$$

$$F_5 = \frac{1}{m_1} (X_{uu}u_d^2 + X_{uu\delta\delta}u_d^2\sum_{i=1}^4 \delta_i^2)$$

$$G = E^{-1} \begin{bmatrix} 0 & 0 & 0 & 0 \\ u_d^2 Y_{uu\delta_1} & u_d^2 Y_{uu\delta_2} & u_d^2 Y_{uu\delta_3} & u_d^2 Y_{uu\delta_4} \\ u_d^2 N_{uu\delta_1} & u_d^2 N_{uu\delta_2} & u_d^2 N_{uu\delta_3} & u_d^2 N_{uu\delta_4} \end{bmatrix}$$

$$\Delta G = E^{-1} \begin{bmatrix} 0 & 0 & 0 & 0 \\ u_d^2 \Delta Y_{uu\delta_1} & u_d^2 \Delta Y_{uu\delta_2} & u_d^2 \Delta Y_{uu\delta_3} & u_d^2 \Delta Y_{uu\delta_4} \\ u_d^2 \Delta N_{uu\delta_1} & u_d^2 \Delta N_{uu\delta_2} & u_d^2 \Delta N_{uu\delta_3} & u_d^2 \Delta N_{uu\delta_4} \end{bmatrix}, E = \begin{bmatrix} 1 & 0 & 0 \\ 0 & m_2 & m_3 \\ 0 & m_4 & m_5 \end{bmatrix}.$$

Appendix 3

$$\theta_{11} = \frac{\frac{\sin e_\psi}{e_\psi \|e_{xy}\|} - a_{12}}{a_{11} - a_{12}}, \theta_{21} = \frac{\frac{\cos e_\psi}{\|e_{xy}\|} - a_{22}}{a_{21} - a_{22}}, \theta_{31} = \frac{|v| - a_{32}}{a_{31} - a_{32}}$$

$$\theta_{41} = \frac{|r| - a_{42}}{a_{41} - a_{42}}, \theta_{i2} = 1 - \theta_{i1}, i \in J_4,$$

$$a_{11} = \sup_{e_\psi \in \{|\epsilon_\psi| \leq \pi\}} \frac{\sin e_\psi}{e_\psi \|e_{xy}\|}, a_{12} = \inf_{e_\psi \in \{|\epsilon_\psi| \leq \pi\}} \frac{\sin e_\psi}{e_\psi \|e_{xy}\|}$$

$$a_{21} = \sup_{e_\psi \in \{|\epsilon_\psi| \leq \pi\}} \frac{\cos e_\psi}{\|e_{xy}\|}, a_{22} = \inf_{e_\psi \in \{|\epsilon_\psi| \leq \pi\}} \frac{\cos e_\psi}{\|e_{xy}\|}$$

$$\begin{aligned}
 a_{31} &= \sup_{v \in B_v} |v|, \quad a_{32} = \inf_{v \in B_v} |v| \\
 a_{41} &= \sup_{r \in B_r} |r|, \quad a_{42} = \inf_{r \in B_r} |r| \\
 A_{i_i \neq \bar{a}_i} &= E^{-1} \begin{bmatrix} u_d a_{1i_1} & a_{2i_2} & 1 \\ 0 & Y_v + Y_{v|v|} a_{3i_3} & \begin{pmatrix} -\mu_d + Y_r \\ + Y_{r|r|} a_{4i_4} \end{pmatrix} \\ 0 & N_v + N_{v|v|} a_{3i_3} & \begin{pmatrix} -m x_g u_d + N_r \\ + N_{r|r|} a_{4i_4} \end{pmatrix} \end{bmatrix} \\
 D_{\Delta F_1} &= E^{-1} \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ D_{Y_v} & D_{Y_{v|v|}} & D_{Y_r} & D_{Y_{r|r|}} & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & D_{N_v} & D_{N_{v|v|}} & D_{N_r} & D_{N_{r|r|}} & 0 \end{bmatrix} \\
 F_{\Delta F_1} &= \text{diag}\{F_{Y_v}, F_{Y_{v|v|}}, F_{Y_r}, F_{Y_{r|r|}}, F_{N_v}, F_{N_{v|v|}}, F_{N_r}, F_{N_{r|r|}}\} \\
 D_{\Delta G} &= E^{-1} \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ D_{Y_{u\delta_1}} & D_{Y_{u\delta_2}} & D_{Y_{u\delta_3}} & D_{Y_{u\delta_4}} & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & D_{N_{u\delta_1}} & D_{N_{u\delta_2}} & D_{N_{u\delta_3}} & D_{N_{u\delta_4}} & 0 \end{bmatrix} \\
 F_{\Delta G} &= \text{diag}\{F_{Y_{u\delta_1}}, F_{Y_{u\delta_2}}, F_{Y_{u\delta_3}}, F_{Y_{u\delta_4}}, F_{N_{u\delta_1}}, F_{N_{u\delta_2}}, F_{N_{u\delta_3}}, F_{N_{u\delta_4}}\} \\
 \tilde{A}_{i_i \neq \bar{a}_i} &= \begin{bmatrix} 0 & Y_v & 0 \\ 0 & Y_{v|v|} a_{3i_3} & 0 \\ 0 & 0 & Y_r \\ 0 & 0 & Y_{r|r|} a_{4i_4} \\ 0 & N_v & 0 \\ 0 & N_{v|v|} a_{3i_3} & 0 \\ 0 & 0 & N_r \\ 0 & 0 & N_{r|r|} a_{4i_4} \end{bmatrix}, \quad \tilde{G} = \begin{bmatrix} u_d^2 Y_{u\delta_1} & 0 & 0 & 0 \\ 0 & u_d^2 Y_{u\delta_2} & 0 & 0 \\ 0 & 0 & u_d^2 Y_{u\delta_3} & 0 \\ 0 & 0 & 0 & u_d^2 Y_{u\delta_4} \\ u_d^2 N_{u\delta_1} & 0 & 0 & 0 \\ 0 & u_d^2 N_{u\delta_2} & 0 & 0 \\ 0 & 0 & u_d^2 N_{u\delta_3} & 0 \\ 0 & 0 & 0 & u_d^2 N_{u\delta_4} \end{bmatrix}
 \end{aligned}$$

References

[1] A. J. Healey and D. Lienard, "Multivariable sliding mode control for autonomous diving and steering of unmanned underwater vehicles," *IEEE Journal of Oceanic Engineering*, vol. 18, no. 3, pp. 327-339, 1999.

[2] J. Guo, F. C. Chiu, and C. C. Huang "Design of a sliding mode fuzzy controller for the guidance and control of an autonomous underwater vehicle," *Ocean Engineering*, vol. 30, no. 16, pp. 2137-2155, 2003

[3] W. Naeem, R. Sutton, and S. M. Ahmad, "Pure pursuit guidance and model predictive control of an autonomous underwater vehicle for cable/pipeline tracking," *IMarEST Journal of Marine Science and Environment, PartC*, vol. 1, pp. 15-25, 2004

[4] A. P. Aguiar and M. P. Antonio, "Dynamic positioning and way-point tracking of underactuated AUVs in the presence of ocean currents," *International Journal of Control*, vol. 80, no. 7, pp. 1092-1108, 2007

[5] E. Borhaug, and K. Y. Pettersen, "Adaptive way-point

tracking control for underactuated autonomous vehicles," *in Decision and control, 2005 and 2005 european control conference CDC-ECC '05*, pp. 4028-4034, 2005.

[6] T. I. Fossen, M. Breivik, and R. Skjetne, "Line-of-sight path following of underactuated marine craft," *In Proceedings of the 6th IFAC MCMC*, pp. 244-249, 2003.

[7] D. W. Kim, "Tracking of REMUS autonomous underwater vehicles with actuator saturations," *Automatica*, vol. 58, pp. 15-21, 2015.

[8] T. I. Fossen, *Marine control systems: guidance, navigation and control of ships*, Marine Cybernetics, 2002

[9] T. Presterio, *Verification of the six-degree of freedom simulation model for the REMUS autonomous underwater vehicle (M.S. thesis)*, MA: MIT, 2001

[10] J. E. Refsnes, Nonlinear model-based control of slender body AUVs (Ph.D. thesis), *Trondheim, Norway: Norwegian University of Science and Technology, Department of Marine Technology*, 2007.

[11] K. Tanaka and H. O. Wang, *Fuzzy control systems design and analysis: A linear matrix inequality approach*. NewYork, NY: Wiley, 2001.

[12] L. Xie, "Output feedback H_∞ control of systems with parameter uncertainties," *International Journal of Control*, vol. 63, no. 4, pp. 741-750, 1996.

[13] J. Kim, K. Kim, H. S. Choi, W. Seong, and K. Y. Lee, "Estimation of hydrodynamic coefficients for an AUV using nonlinear observers." *IEEE journal of oceanic engineering*, vol 27, no. 4, pp. 830-840, 2002.

저 자 소 개



김도완 (Do Wan Kim)

He received the B.S., M.S., and Ph.D. degrees from the Department of Electrical and Electronic Engineering, Yonsei University, Seoul, Korea, in 2002, 2004, and 2007, respectively. He was a Visiting Scholar with the Department of Mechanical Engineering, University of California, Berkeley. In 2009, he was a Research Professor with the Department of Electrical and Electronic Engineering, Yonsei University. Since 2010, he has served on the faculty in the Department of Electrical Engineering, Hanbat National University.



박 정 훈 (Jeong-Hoon Park)

He received B.S. and M.S. degree in Yonsei University in 2004 and 2006, respectively. In 2006, he joined the Naval Academy of Republic of Korea as a lecturer and in 2009. From 2009 to present, he has working at LIG Nex1. His research interest includes an artificial intelligence and AUV system.



박 호 규 (Ho-Gyu Park)

He received B.S and M.S. Degree in Myungji University in 1987 and 1989, respectively. From 1992 to present, he has working at LIG Nex1 as principal research engineer. His research interest includes an underwater guidance system and AUV autonomous control system.



김 태 영 (Tae-Yeong Kim)

He received B.S and M.S. Degree in Kyungpook National University in 1985 and 1987, respectively. In 2009, he received Ph. D. degree in mechatronics engineering in Sungkyungkwan University. From 1987 to present, we has working at LIG Nex1. Currently, He is Director of Maritime Dept. His research interest includes underwater guidance weapon system and AUVs.