# A Study on the Goal Setting Method for Increasing the Holed Probability in Slope Putting Stroke on an Artificial Putting Surface 

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Objective: The purpose of this study was to develop a goal setting method for increasing the probability of a holed in a side inclined putting stroke.

Method: Three-dimensional video data was recorded at a frequency of 120 hz per second after synchronizing 19 infrared motion capture systems (Qualisys, Gothenburg, Sweden). Putting green used a polycarbonate plate $(1.2 \times 2.4 \times 0.01$ meter $)$ with coefficient of friction $(\mu=0.062)$ and a real curve of the actual hole.

Results: The velocity ratio between the club and the ball was 1:1.6 under various ball speed conditions in this study. The overall position of the break is 1 m to 1.4 m from the point where the ball leaves. If there is a slope, the ball follows the target line by the straightening force, and when it reaches 1 m position, the straightening force decreases by $30 \sim 50 \%$ and reaches to the deviation (break) point which is severely influenced by the slope. From here, the ball is aimed in a direction other than the target, and the size is affected by the slope.

Conclusion: If there is a side slope, the ball moves away from the straight line, and the larger the slope, the closer the break point is to the starting point of the ball. Therefore, it is necessary to calculate the degree of departure according to the slope carefully, and it is preferable that the slower the speed is, the more the influence of the slope becomes. It is preferable to use the center of the hole as a reference when calculating the departure.

Keywords: Putting stroke, Holed, Slope, Goal setting, Golf

## INTRODUCTION

Golf is a game that involves using various clubs to stroke the ball continuously and finally to the hole. Such golf stroke techniques can be divided into driving strokes and putting strokes from a kinematic point of view. The difference between the two strokes is that the driving stroke is long, while the ball travels from the ground and travels in the air, whereas the putting stroke is long when the ball moves in contact with the ground. Therefore, the driving stroke requires much research on the influence of air or fluid in the process of ball movement, but the phenomenon that occurs in contact with the ground is extremely weak. On the other hand, the putting stroke is more influenced by the condition or slope of the green than by the influence of the fluid. Therefore, the direction of interest is also the state of the ground on which the ball is moving, i.e., the length of the grass, the trace of the ground, and the existence of slope (Pelz \& Frank, 2000). For this reason, Cochran \& Stobbs (1968), who studied various aspects of golf, explains that analyzing balls across the green is a very difficult task.

Putting strokes account for about 40\% to 45\% of all strokes (Palmer \& Dobereiner, 1986; Heuler, 1995; Park, 2000; Pelz \& Frank, 2000). According to Alexander \& Kern (2005), the analysis of the contents of the professional golf association (PGA) in the United States revealed that the putting stroke ability is the first factor to get the most prize money. The technical part of the putting stroke which has a great influence on the golf performance is rather simply explained (Park, 2002). In Sim \& Kim (2010), the most ideal putting stroke is to stroke into the hole by giving the required speed in the intended direction to the ball. They looked at the important kinematics in putting in direction and velocity. And if it does not, it will stroke at a speed close to the hole and end the hole with the next pitch (Sayers, Stuelcken \& Gorman, 2017). In other words, the two things required in the putting technique are the accuracy of the direction and the appropriateness of the speed. Regarding the proper speed, Holmes (1991) reported in computer modeling studies that the ball holdable speed is less than $1.6 \mathrm{~m} / \mathrm{s}$ at the edge of hole. If this speed is exceeded, the rim of the hole will bounce off the ball rather than drop it down. This is the case when the
ball is pointing toward the center of the hole, and if it goes into the hole cup by moving the center, the velocity of the ball must be smaller before it can be held.
According to Pelz \& Frank (2000), the success rate of 1.8 -meter putting is about $43 \sim 57 \%$ even if it is a professional golfer who is world-class. However, if they are aware of the terrain, the success rate at the same distance can rise to $90 \%$. In addition, according to an Internet golf putting material (Golfdatalab, 2017), we analyzed the putting score by distance in the PGA tour. For example, if you are at 0.9 m , it is 1.0008 strokes, and if you are at 1.8 m , it is 1.363 strokes. In other words, it can be concluded that as the distance increases, the shape of the ground influences the putting. Karlsen, Smith \& Nilsson (2008) suggested that the factors affecting the direction of the ball were green reading, goal setting, stroke, and green irregularity. Of these four elements, three except for the stroke are related to the shape or slope of the green surface. These factors also affect the direction of the ball regardless of the stroke performance of the athlete. Before putting, the players will observe the ground and draw a line of putt where the ball will go. In this case, consideration is given to the length of the grass (friction) and the slope of the ground. The length of the grass and the speed of the green are measured using stimpmeter provided by Stimpson (1974) before the game. However, the slope of the green varies depending on the position of the hole, and the shape of the green is not the same as all the holes from the time of designing the golf course. Therefore, it is not easy to grasp the ground conditions around the hole, and research on how the balls move according to the degree of inclination is very insufficient.
Pelz \& Frank (2000) are pioneers in the scientific study of how the ball changes when there is a slope on the green. They describe the change in the position of the ball in the side slope in terms of "break". The break that a researcher is talking about is the distance, which means the deviation between the end point of the target line and the center of the hole, or the width (distance) from the imaginary parabolic tangent line to the target line. However, the contents of this study are not described in academic books but in the form of figures or tables in their own books. Park (2014) presented the theoretical conditions for the holed when the starting and ending points made the putting stroke on the same side slope. For example, if the ball at $1 \mathrm{~m} / \mathrm{s}$ goes 1 meter from the side slope, the size of the break at the end point is 8.6 cm , and if the ball at $2 \mathrm{~m} / \mathrm{s}$ travels 2 meters from the 2 degree side slope, the size of the break at the end point is 17.1 cm , respectively. Theoretically, the center of the hole is preferably shifted to the left or to the right according to a sloping direction of 8.6 cm for a 1 meter putt and 17.1 cm for a 2 meter putt. However, this study also shows that the theoretical result is that there is no friction from the ball to the hole and there is a limit to applying the same angle side slope to realistic greens. Therefore, for a more realistic study, it is necessary to set the green condition similar to the actual green form and to see how the ball's movement changes. If we do, we think that it will be possible to provide the players who perform the actual golf game about the movement of the ball in the putting stroke. Therefore, the purpose of this study relates to a goal setting method for increasing the probability of a holed at a various inclined putting stroke. So the slopes of the ground
were divided into three levels: balance, low side slope, and high side slope. And the ball has four kinds of speed that can be held in the hole. The faster the speed of the ball, the less likely it will be affected by the slope. However, if the speed is slowed down, the slope will affect it more, and the 'flowing' phenomenon of the ball will appear.

## METHODS

## 1. Procedure

All studies were conducted in a biomechanics laboratory at the Korea Institute of Sport Science (KISS). Three-dimensional video data was recorded at a frequency of 120 hz per second after synchronizing 19 infrared motion capture systems (Qualisys, Gothenburg, Sweden). Putting green used a polycarbonate plate ( $1.2 \times 2.4 \times 0.01$ meter $)$ with coefficient of rolling friction ( $\mu=0.062$ ) and a real curve of the actual green (Figure $1 \& 2$ ). The rolling friction coefficient was calculated using the difference between the initial velocity $(50 \mathrm{~cm})$ and the final velocity $(100 \mathrm{~cm})$ and the time taken. The putter was a Ping putter and attached a reflection marker at 4 cm horizontal from the sweet spot to the toe in order to know the movement of the head. The ball was attached to the entire surface with a reflective tape with a Titleist Pro v1. To transfer the momentum to the ball, a pendulum putting machine (PPM) was used (Park, 2006). The machine weighs about 100 N and is 75 cm high. The distance (radius) to the point at which the impact occurs at the fixed part where the putter can be caught is 76 cm . The PPM was fixed on the ground with additional weight so that the putter did not move in the collision with the ball. The putter was manually operated and allowed to hit the ball at the lowest point of free fall. In order to make the slopes of the artificial green with the polycarbonate plate, 2.5 cm diameter iron ball for a low slope (LS) green and 4.3 cm diameter golf ball for a high slope (HS) green were, respectively, placed underneath the polycarbonate plate at the position of -18 cm posteriorly and 150 cm laterally from the origin. The T-shaped wooden pillar ( 1 m tall) is installed in the backswing area of the pendulum putter to prevent the club head from moving beyond the predetermined section. Bosch's GLM500 (Figure 3) is a device that measures the slope of the ground (10 positions), and the angle of the slope to the first decimal place is known (Figure 4). The coordinates of the experiment site are the $y$-axis in the direction of travel of the ball, the $x$-axis in the side-slope direction, and the z -axis in the vertical direction. The origin of the ball movement was set at 18 cm in the $x$-axis and 20 cm in the $y$-axis at the end of the plate. Each marker was attached to every 11 cm of x axis and every 50 cm of y axis, so that a virtual grid plate $(88 \times 200 \mathrm{~cm})$ could be made to grasp the position of the ball (Figure 4). The slope degree of the 10 points determined by the researcher was measured and recorded by the GLM500 (Table 1). Before experiment, the pendulum putter was controlled several times after confirming whether the ball moved to the target (hypothetical hole) set by the researcher. In the first experiment, the poly plate was made flat and the wooden pillar was moved 20 cm horizontally behind the impact point. The researcher moves the club back and then releases it to let the club fall freely. After 5 repetition experiments at the same point, the wooden pillar was moved 25 cm


Figure 1. Experimental conditions with a pendulum putting machine and a wooden plate


Figure 2. Slope change with golf ball
position and same process of experiment was repeated. After that, the wooden pillar was moved 30 cm and 35 cm and same experiment was repeated. The second experiment was a low slope, placing the iron ball at the bottom of coordinate $(-18 \mathrm{~cm}, 150 \mathrm{~cm})$ from the origin. Then, the slope was measured and recorded. Table 1 shows that odd numbers are anteroposterior directions and even numbers are lateral directions. And then the experiment was repeated in the same manner as the first experiment. The third experiment was carried out in the same way except that the golf ball was placed instead of iron ball for a high slope. In the case of low slope, the direction of the ball was 0.7 degree up, and the side was 3.1 degree slope. On the other hand, in the case of


Figure 3. Slope checking machine (GLM 500)
high slope, the direction of the ball was 1.6 degree up and the side was 4.7 degree slope.


Figure 4. Measurement point and ten angle check positions

Table 1. Angle of each measurement point of poly plate

| MP | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F | 0.1 | 0.1 | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 |
| LS | 0.3 | 0.1 | 0.5 | 3.1 | 0.1 | 0.0 | 0.1 | 0.1 | 0.7 | 1.4 |
| HS | 0.8 | 0.5 | 0.2 | 4.7 | 0.1 | 0.1 | 0.0 | 0.7 | 1.6 | 2.6 |

MP: measurement point, F: flat, LS: low slope, HS: high slope

## 2. Data processing

Performed trials were imported into Qualisys motion capture system (Gothenburg, Sweden) for further processing and analyzing the data. The raw coordinates of ball and club head were filtered using Butterworth low-pass filter with 6 hz cut-off frequencies (Winter, 1990). The club's data were collected from the beginning of the move to 20 frames after impact. The data of the ball was collected from the stationary position to the target direction 2 meters. The data of ball compared the displacements and velocities on the $y$ and $x$ axes, which appear in flat, low slope and high slope. The comparison point is $7 \sim 14 \mathrm{~cm}$ (where the maximum velocity appears in the y-axis direction), 50 cm and 100 cm . After passing 100 cm , it was analyzed up to 180 cm in 10 cm increments. Time interval between frames is 0.00833 s and the time interval of finite difference method (Robertson, Caldwell, Hamil, Karmen \& Wittlesey, 2004) is 0.0167 s .

## 3. Statistical analysis

The internal consistency reliability for repeated experiments (flat, low
slope, high slope) is presented in Cronbach's $\alpha$ (Appendix 1). The $y$-axis velocity and the $x$-axis velocity at the maximum velocity of 6 to 14 cm and $50 \mathrm{~cm}, 100 \mathrm{~cm}, 110 \mathrm{~cm}, 120 \mathrm{~cm}, 130 \mathrm{~cm}, 140 \mathrm{~cm}, 150 \mathrm{~cm}, 160 \mathrm{~cm}$, 170 cm and 180 cm were calculated by finite difference method (Robertson, Caldwell, Hamill, Kamen \& Whittlesey, 2004). The statistical significant position (break point) of the ball was confirmed by one-way ANOVA (Appendix 2). When there was an average difference between the groups, Scheffe's post-hoc test was performed. All statistical significance was .05 .

## RESULTS

The club's maximum velocity is $0.72( \pm 0.002) \mathrm{m} / \mathrm{s}$ when the club is allowed to fall freely 20 cm backwards and the maximum velocity of the ball is $1.16( \pm 0.05) \mathrm{m} / \mathrm{s}$. The maximum velocity of the club when it is allowed to fall back 25 cm backward is $0.96( \pm 0.001) \mathrm{m} / \mathrm{s}$ and the maximum velocity of the ball is $1.46( \pm 0.05) \mathrm{m} / \mathrm{s}$. When the club is freely dropped 30 cm backwards, the club's maximum velocity is $1.08( \pm 0.002$ ) $\mathrm{m} / \mathrm{s}$ and the ball's maximum velocity is $1.77( \pm 0.03) \mathrm{m} / \mathrm{s}$. The club's maximum velocity is $1.32( \pm 0.002) \mathrm{m} / \mathrm{s}$ when the club is free to fall back 35 cm
backwards and the maximum velocity of the ball is $2.17( \pm 0.01) \mathrm{m} / \mathrm{s}$.

## 1. Velocity ratio of club to ball

Table 2 shows the magnitude and ratio of velocity of the club and ball at the impact point according to the free-fall distance of the club.
2. Velocity of the ball with the free fall distance of the putter

Table 3 shows the ratio of the $y$-axis velocity to the $y$-axis maximum velocity at each point along the free-fall distance of the club and the $x$-axis velocity.

Table 2. Characteristics of the ratio of impact velocity of the pendulum putting machine to the departure velocity of the ball

| Club head distance | Club head velocity | Ball maximum velocity | Club vs ball ratio |
| :---: | :---: | :---: | :---: |
| 20 D | $0.72 \mathrm{~m} / \mathrm{s}$ | $1.16 \mathrm{~m} / \mathrm{s}$ | $1: 1.6$ |
| 25 D | $0.96 \mathrm{~m} / \mathrm{s}$ | $1.46 \mathrm{~m} / \mathrm{s}$ | $1: 1.5$ |
| 30 D | $1.08 \mathrm{~m} / \mathrm{s}$ | $1.77 \mathrm{~m} / \mathrm{s}$ | $1: 1.6$ |
| 35 D | $1.32 \mathrm{~m} / \mathrm{s}$ | $2.17 \mathrm{~m} / \mathrm{s}$ | $1: 1.6$ |

20D: club head moved 20 cm and freely dropped, 25D: club head moved 25 cm and freely dropped, 30D: club head moved 30 cm and freely dropped, 35D: club head moved 35 cm and freely dropped

Table 3. The velocity of the ball ( $y$ and $x$ axes) with the free fall distance of the putter

| Distance | Slope | Length velocity | $\begin{gathered} 7 \sim 14 \\ \mathrm{~cm} \end{gathered}$ | $\begin{aligned} & 50 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 100 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 110 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 120 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 130 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 140 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 150 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 160 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 170 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 180 \\ & \mathrm{~cm} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20D | F | $y(\mathrm{~m} / \mathrm{s})$ | 1.16 | 0.78 | 0.67 | 0.62 | 0.60 | 0.58 | 0.55 | 0.53 | 0.49 | 0.46 | 0.41 |
|  |  |  | 100 | 67\% | 58\% | 53\% | 52\% | 50\% | 47\% | 46\% | 42\% | 40\% | 35\% |
|  |  | $x(\mathrm{~m} / \mathrm{s})$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
|  | L | $y(\mathrm{~m} / \mathrm{s})$ | 1.16 | 0.77 | 0.62 | 0.56 | 0.53 | 0.49 | 0.44 | 0.41 | 0.38 | 0.32 | 0.32 |
|  |  |  | 100 | 66\% | 53\% | 48\% | 46\% | 42\% | 40\% | 35\% | 33\% | 28\% | 28\% |
|  |  | $x(m / s)$ | 0.00 | 0.01 | 0.07 | ${ }^{*} 0.12$ | 0.16 | 0.20 | 0.26 | 0.25 | 0.29 | 0.29 | 0.29 |
|  | H | $y(m / s)$ | 1.16 | 0.73 | 0.52 | 0.47 | 0.36 | 0.34 | 0.25 | 0.24 | 0.20 | 0.14 | - |
|  |  |  | 100 | 63\% | 45\% | 41\% | 31\% | 29\% | 22\% | 21\% | 17\% | 12\% | - |
|  |  | $x(\mathrm{~m} / \mathrm{s})$ | 0.00 | 0.01 | *0.12 | 0.23 | 0.28 | 0.34 | 0.35 | 0.38 | 0.28 | 0.23 | - |
| 25D | F | $y(m / s)$ | 1.46 | 1.01 | 0.91 | 0.90 | 0.90 | 0.88 | 0.86 | 0.85 | 0.84 | 0.80 | 0.79 |
|  |  |  | 100 | 69\% | 62\% | 62\% | 62\% | 60\% | 59\% | 58\% | 58\% | 55\% | 54\% |
|  |  | $x(\mathrm{~m} / \mathrm{s})$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
|  | L | $y(m / s)$ | 1.46 | 1.02 | 0.91 | 0.85 | 0.82 | 0.78 | 0.76 | 0.73 | 0.71 | 0.67 | 0.68 |
|  |  |  | 100 | 70\% | 62\% | 58\% | 56\% | 53\% | 52\% | 50\% | 49\% | 46\% | 47\% |
|  |  | $x(m / s)$ | 0.00 | 0.01 | 0.01 | 0.05 | 0.05 | ${ }^{* *} 0.13$ | 0.17 | 0.24 | 0.28 | 0.29 | 0.30 |
|  | H | $y(m / s)$ | 1.46 | 1.00 | 0.84 | 0.80 | 0.76 | 0.72 | 0.68 | 0.66 | 0.62 | 0.61 | 0.59 |
|  |  |  | 100 | 68\% | 58\% | 55\% | 52\% | 49\% | 47\% | 45\% | 42\% | 42\% | 40\% |
|  |  | $x(\mathrm{~m} / \mathrm{s})$ | 0.00 | 0.01 | *0.08 | 0.16 | 0.20 | 0.28 | 0.30 | 0.36 | 0.42 | 0.43 | 0.42 |
| 30D | F | $y(m / s)$ | $1.77$ | 1.28 | $1.16$ | $1.17$ | $1.16$ | $1.14$ | $1.13$ | $1.13$ | $1.10$ | $1.08$ | 1.08 |
|  |  |  | 100 | 72\% | $66 \%$ | $66 \%$ | $66 \%$ | $64 \%$ | $64 \%$ | 64\% | 62\% | 61\% | 61\% |
|  |  | $x(\mathrm{~m} / \mathrm{s})$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
|  | L | $y(m / s)$ | 1.77 | 1.27 | 1.16 | 1.12 | 1.10 | 1.06 | 1.07 | 1.04 | 1.02 | 1.01 | 1.00 |
|  |  |  | 100 | 72\% | 66\% | 63\% | 62\% | 60\% | 61\% | 59\% | 58\% | 57\% | 56\% |
|  |  | $x(\mathrm{~m} / \mathrm{s})$ | 0.00 | 0.01 | 0.01 | 0.03 | 0.05 | 0.10 | ${ }^{* *} 0.14$ | 0.18 | 0.23 | 0.24 | 0.31 |
|  | H | $y(m / s)$ | 1.77 | 1.28 | 1.12 | 1.08 | 1.01 | 0.97 | 0.97 | 0.95 | 0.94 | 0.90 | 0.89 |
|  |  |  | 100 | 72\% | 63\% | 61\% | 57\% | 55\% | 55\% | 54\% | 53\% | 51\% | 50\% |
|  |  | $x(\mathrm{~m} / \mathrm{s})$ | 0.00 | 0.01 | 0.01 | 0.08 | *0.10 | 0.11 | 0.24 | 0.30 | 0.30 | 0.38 | 0.41 |

Table 3. The velocity of the ball ( y and x axes) with the free fall distance of the putter (Continued)

| Distance | Slope | Length velocity | $\begin{gathered} 7 \sim 14 \\ \mathrm{~cm} \end{gathered}$ | $\begin{aligned} & 50 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 100 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 110 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 120 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 130 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 140 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 150 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 160 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 170 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 180 \\ & \mathrm{~cm} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 35D | F | $y(m / s)$ | 2.17 | 1.76 | 1.45 | 1.42 | 1.42 | 1.39 | 1.38 | 1.38 | 1.36 | 1.33 | 1.34 |
|  |  |  | 100 | 81\% | 67\% | 65\% | 65\% | 64\% | 64\% | 64\% | 63\% | 61\% | 62\% |
|  |  | x (m/s) | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.10 | 0.10 | 0.16 | 0.17 | 0.20 |
|  | L | $y(m / s)$ | 2.17 | 1.74 | 1.39 | 1.38 | 1.37 | 1.37 | 1.34 | 1.32 | 1.30 | 1.28 | 1.27 |
|  |  |  | 100 | 80\% | 64\% | 64\% | 63\% | 63\% | 62\% | 61\% | 60\% | 59\% | 59\% |
|  |  | $x(m / s)$ | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | ${ }^{* *} 0.10$ | 0.10 | 0.16 | 0.17 | 0.20 |
|  | H | $y(m / s)$ | 2.17 | 1.76 | 1.39 | 1.34 | 1.32 | 1.31 | 1.26 | 1.26 | 1.22 | 1.22 | 1.22 |
|  |  |  | 100 | 81\% | 64\% | 62\% | 61\% | 60\% | 58\% | 58\% | 56\% | 56\% | 56\% |
|  |  | $x(\mathrm{~m} / \mathrm{s})$ | 0.00 | 0.01 | 0.01 | ${ }^{* *} 0.10$ | 0.14 | 0.14 | 0.18 | 0.24 | 0.26 | 0.31 | 0.31 |

20D: club head moved 20 cm and freely dropped, 25D: club head moved 25 cm and freely dropped, 30D: club head moved 30 cm and freely dropped, 35D: club head moved 35 cm and freely dropped, F: flat green, L: green with Low slope, H: green with High slope, * <. 05 , ** <. 01

Table 4. The displacement deviating from the $x$-axis direction at each point and $y$-axis direction velocity

| Distance | y | Length | $\begin{gathered} 7 \sim 14 \\ \mathrm{~cm} \end{gathered}$ | $\begin{aligned} & 50 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 100 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 110 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 120 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 130 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 140 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 150 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 160 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 170 \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 180 \\ & \mathrm{~cm} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20D | L | $\begin{aligned} & x(\mathrm{~cm}) \\ & y(\mathrm{~m} / \mathrm{s}) \end{aligned}$ | $\begin{gathered} 0.01 \\ (1.16) \end{gathered}$ | $\begin{gathered} 0.1 \\ (0.77) \end{gathered}$ | $\begin{gathered} 1.6 \\ (0.62) \end{gathered}$ | $\begin{gathered} 2.3 \\ (0.56) \end{gathered}$ | $\begin{gathered} 4.1 \\ (0.53) \end{gathered}$ | $\begin{gathered} 6.3 \\ (0.49) \end{gathered}$ | $\begin{gathered} 9.4 \\ (0.44) \end{gathered}$ | $\begin{gathered} 13.1 \\ (0.41) \end{gathered}$ | $\begin{gathered} 17.8 \\ (0.38) \end{gathered}$ | $\begin{gathered} 23.0 \\ (0.32) \end{gathered}$ | $\begin{gathered} 28.6 \\ (0.32) \end{gathered}$ |
|  | H | $\begin{aligned} & x(\mathrm{~cm}) \\ & y(\mathrm{~m} / \mathrm{s}) \end{aligned}$ | $\begin{gathered} 0.01 \\ (1.16) \end{gathered}$ | $\begin{gathered} 0.4 \\ (0.73) \end{gathered}$ | $\begin{gathered} 3.0 \\ (0.52) \end{gathered}$ | $\begin{gathered} 6.0 \\ (0.47) \end{gathered}$ | $\begin{gathered} 11.1 \\ (0.36) \end{gathered}$ | $\begin{gathered} 19.0 \\ (0.34) \end{gathered}$ | $\begin{gathered} 30.7 \\ (0.25) \end{gathered}$ | $\begin{gathered} 44.2 \\ (0.24) \end{gathered}$ | $\begin{gathered} 58.6 \\ (0.20) \end{gathered}$ | $\begin{gathered} 73.8 \\ (0.14) \end{gathered}$ | $\begin{aligned} & - \\ & - \end{aligned}$ |
| 25D | L | $\begin{gathered} x(\mathrm{~cm}) \\ y(\mathrm{~m} / \mathrm{s}) \end{gathered}$ | $\begin{gathered} 0.01 \\ (1.46) \end{gathered}$ | $\begin{gathered} 0.01 \\ (1.02) \end{gathered}$ | $\begin{gathered} 1.2 \\ (0.91) \end{gathered}$ | $\begin{gathered} 2.1 \\ (0.85) \end{gathered}$ | $\begin{gathered} 3.2 \\ (0.82) \end{gathered}$ | $\begin{gathered} 4.8 \\ (0.78) \end{gathered}$ | $\begin{gathered} 6.9 \\ (0.76) \end{gathered}$ | $\begin{gathered} 9.6 \\ (0.73) \end{gathered}$ | $\begin{gathered} 12.9 \\ (0.71) \end{gathered}$ | $\begin{gathered} 16.9 \\ (0.67) \end{gathered}$ | $\begin{gathered} 21.3 \\ (0.68) \end{gathered}$ |
|  | H | $\begin{gathered} x(\mathrm{~cm}) \\ y(\mathrm{~m} / \mathrm{s}) \end{gathered}$ | $\begin{gathered} 0.01 \\ (1.46) \end{gathered}$ | $\begin{gathered} 0.2 \\ (1.00) \end{gathered}$ | $\begin{gathered} 3.6 \\ (0.84) \end{gathered}$ | $\begin{gathered} 5.4 \\ (0.80) \end{gathered}$ | $\begin{gathered} 7.8 \\ (0.76) \end{gathered}$ | $\begin{gathered} 10.9 \\ (0.72) \end{gathered}$ | $\begin{gathered} 15.3 \\ (0.68) \end{gathered}$ | $\begin{gathered} 20.5 \\ (0.66) \end{gathered}$ | $\begin{gathered} 26.5 \\ (0.62) \end{gathered}$ | $\begin{gathered} 33.5 \\ (0.61) \end{gathered}$ | $\begin{gathered} 40.7 \\ (0.59) \end{gathered}$ |
| 30D | L | $\begin{aligned} & x(\mathrm{~cm}) \\ & y(\mathrm{~m} / \mathrm{s}) \end{aligned}$ | $\begin{gathered} 0.01 \\ (1.77) \end{gathered}$ | $\begin{gathered} 0.4 \\ (1.27) \end{gathered}$ | $\begin{gathered} 1.8 \\ (1.16) \end{gathered}$ | $\begin{gathered} 2.4 \\ (1.12) \end{gathered}$ | $\begin{gathered} 3.3 \\ (1.10) \end{gathered}$ | $\begin{gathered} 4.4 \\ (1.06) \end{gathered}$ | $\begin{gathered} 5.8 \\ (1.07) \end{gathered}$ | $\begin{gathered} 7.4 \\ (1.04) \end{gathered}$ | $\begin{gathered} 9.5 \\ (1.02) \end{gathered}$ | $\begin{gathered} 12.0 \\ (1.01) \end{gathered}$ | $\begin{gathered} 14.7 \\ (1.00) \end{gathered}$ |
|  | H | $\begin{aligned} & x(\mathrm{~cm}) \\ & y(\mathrm{~m} / \mathrm{s}) \end{aligned}$ | $\begin{gathered} 0.01 \\ (1.77) \end{gathered}$ | $\begin{gathered} 0.2 \\ (1.28) \end{gathered}$ | $\begin{gathered} 1.8 \\ (1.12) \end{gathered}$ | $\begin{gathered} 2.8 \\ (1.08) \end{gathered}$ | $\begin{gathered} 4.3 \\ (1.01) \end{gathered}$ | $\begin{gathered} 5.9 \\ (0.97) \end{gathered}$ | $\begin{gathered} 8.1 \\ (0.97) \end{gathered}$ | $\begin{gathered} 11.0 \\ (0.95) \end{gathered}$ | $\begin{gathered} 14.5 \\ (0.94 \end{gathered}$ | $\begin{gathered} 18.4 \\ (0.90) \end{gathered}$ | $\begin{gathered} 22.8 \\ (0.89) \end{gathered}$ |
| 35D | L | $\begin{aligned} & x(\mathrm{~cm}) \\ & y(\mathrm{~m} / \mathrm{s}) \end{aligned}$ | $\begin{gathered} 0.01 \\ (2.17) \end{gathered}$ | $\begin{gathered} 0.1 \\ (1.74) \\ \hline \end{gathered}$ | $\begin{gathered} 0.2 \\ (1.39) \end{gathered}$ | $\begin{gathered} 0.5 \\ (1.38) \end{gathered}$ | $\begin{gathered} 1.0 \\ (1.37) \end{gathered}$ | $\begin{gathered} 1.5 \\ (1.37) \end{gathered}$ | $\begin{gathered} 2.4 \\ (1.34) \end{gathered}$ | $\begin{gathered} 3.4 \\ (1.32) \end{gathered}$ | $\begin{gathered} 4.7 \\ (1.30) \\ \hline \end{gathered}$ | $\begin{gathered} 6.2 \\ (1.28) \end{gathered}$ | $\begin{gathered} 7.9 \\ (1.27) \\ \hline \end{gathered}$ |
|  | H | $\begin{gathered} x(\mathrm{~cm}) \\ y(\mathrm{~m} / \mathrm{s}) \end{gathered}$ | $\begin{gathered} 0.01 \\ (2.17) \end{gathered}$ | $\begin{gathered} 0.2 \\ (1.76) \end{gathered}$ | $\begin{gathered} 0.5 \\ (1.39) \end{gathered}$ | $\begin{gathered} 1.2 \\ (1.34) \end{gathered}$ | $\begin{gathered} 2.1 \\ (1.32) \end{gathered}$ | $\begin{gathered} 3.1 \\ (1.31) \end{gathered}$ | $\begin{gathered} 4.6 \\ (1.26) \end{gathered}$ | $\begin{gathered} 6.5 \\ (1.26) \end{gathered}$ | $\begin{gathered} 8.8 \\ (1.22) \end{gathered}$ | $\begin{gathered} 11.2 \\ (1.22) \end{gathered}$ | $\begin{gathered} 14.2 \\ (1.22) \end{gathered}$ |

3. Displacement displaced in the $x$-axis direction and the $y$-axis direction velocity

The displacement along the $x$-axis direction along the free-fall distance of the club and the $y$-axis velocity at that time are shown in Table 4.

## DISCUSSION

One of the most important factors in the putting game is the speed of the green. To measure this, Stimpson (1974) proposed a tool to measure the ball's rolling speed constantly. It was named as 'Stimpmeter'. Holmes (1991) measured the velocity of the ball when leaving the tool
at $1.83 \mathrm{~m} / \mathrm{s}$. The speed of the golf green is so varied that the ball rolls up to 3.66 meters for fast greens and 1.22 meters for slow greens. Penner (2002) reported that the coefficient of friction of the ball in this situation was 0.196 to 0.065 . It is recommended to use 0.131 , which is the average coefficient of friction, under normal circumstances. In this study, the coefficient of friction was measured to be 0.062 using four kinds of speeds in the flat area. Therefore, the coefficient of friction of the poly plate in this study is the same as that of the experiment with very fast putting green. One of the important issues in the study of equipment games (golf, baseball, table tennis, etc.) is whether balls and tools impact on sweet spots. In this study, it was controlled that the pendulum putting machine and the ball were contacted in the state of being fitted to the sweet spot, so that repeated impacts occurred
there. The blow from the putting stroke to the sweet spot has a very important meaning. In a typical experiment, the putting machine was set to hit putts which traveled about 6 meters when hit in the center of the putter face (sweet spot). When the ball moved 2.54 cm towards the toe or heel, the putts stopped $1.2 \sim 1.8$ meters short of the centralhit distance, and about 18 cm to one side - left if heeled, right if toed (Cochran \& Stobbs, 1968). As shown in (Table 2), when the impact was at the sweet spot, the velocity ratio between the club and the ball was 1:1.6 under various conditions. This ratio is often known as the golden ratio, and has been the focus of many researchers since the study of the Greek mathematician Euclid (Wikipedia, 2017). The maximum velocity of an impacted ball was at 7 to 14 cm , which corresponds to one half or one turn of the ball after impact. Also, depending on the club's speed, the point at which the ball's maximum velocity appears is affected, and the time it takes to reach the maximum velocity will also vary. As Cochran \& Stobbs (1968) pointed out, the initial movement area of the ball is affected unnecessarily from the ground by the large movement of the ball when viewed from the whole of the ball movement. Also, as the ball continues to progress, the initial effect will cause the ball to change direction. Therefore, it is desirable to roll immediately after impact (Naver, 2014) in order to reduce the unnecessary external influence of the ball. For this purpose, external force must be large and impact point is high. The ball is also believed to be slowing down in its initial movements. As shown in Table 3, when the ball moves at a speed of 50 cm at various ball speeds, the velocity of the ball at 1.16 $\mathrm{m} / \mathrm{s}$ is reduced by about $33 \%$, the ball at $1.46 \mathrm{~m} / \mathrm{s}$ is reduced by about $31 \%$, the ball at $1.77 \mathrm{~m} / \mathrm{s}$ is reduced by about $28 \%$ and $19 \%$ of $2.17 \mathrm{~m} / \mathrm{s}$, respectively. The results of this study are the same as those pointed out by Hubbard \& Alaways (1999) in their study. The slower the ball, the greater the retarding force. That is, as the ball progresses, the influence of the frictional force becomes larger, so that the speed is further reduced. This phenomenon is considered to be greater when the starting velocity is slow.
The position of the changing point (break point) of the ball due to the slope is more closer to the higher slope than lower slope. The changing position of the ball is about 1 to 1.4 m from the point where the ball leaves. Pelz and Frank (2000) analyzed the 'break' and reported that when your target line passes 2.5 cm outside the cup, then putt breaks are 7.9 cm into the center of the hole. In this case, the 'break' is a radius of hole and off distance at the target line. It is a usual term in golf. But in this study, 'break' is a point which changes the direction from the expected ball line. That is, if there is a slope, the ball follows the target line by the straightening force, and when it reaches 1 m position, the straightening force decreases by $30 \sim 50 \%$ and reaches to the deviation point which is severely influenced by the slope. From here, the ball is aimed in a direction other than the target, and the slope affects its size. 20D (club head moved 20 cm and freely dropped) of Table 3 shows that a ball with a speed of $1.16 \mathrm{~m} / \mathrm{s}$ cannot proceed to the target direction when it meets a high slope and continues to 'slip' in the slope direction. In other words, a ball with a speed that cannot overcome a slope cannot reach the target point, so a putting stroke that provides a sufficient speed can be considered necessary.
Table 4 shows the velocity of the ball and the size of the center of
the ball that deviates from the center when entering the hole. Since the radius is 5.4 cm at the center of the hole, if the deviation in the $x$-axis is less than the radius, it can enter the hole once. However, as claimed by Holmes (1991), the position should be 10.8 cm in diameter at the center of the hole. In conclusion, there is no ball held in the hole at the target 1.8 meters if there is some slope, except when the ground is flat. So the goal must be reset and its size is highly relevant to the slope.

## CONCLUSIONS AND SUGGESTION

According to the results of this experiment, the ratio between club and ball was 1:1.6 when the ball was impacted with sweet spot. And the maximum velocity of ball showed at the position of $7 \sim 14 \mathrm{~cm}$ from the starting point and about $0.08 \sim 0.09 \mathrm{~s}$ of time was taken. If there is a side slope when a ball is moving on the putting green, the ball moves away from the straight line. It was also concluded that the bigger the slope, the position of the break is nearer to the starting point. In this experiment, the position of the break was about 1~1.4 m after the ball departed from the original position. If the ball was at 1.8 meters from the target (diameter 10.8 cm ) and the ball was stroke to the center of the hole cup, it cannot get into the hole cup at the starting speeds of 1.16 to $2.17 \mathrm{~m} / \mathrm{s}$. Because the ball is affected by uphill and sidehill slope, the ball slows down and drifts away from the target. Therefore, the player should increase the speed of the ball or change the target from 7.9 to 28.6 cm toward the higher side. According to the results of this study, it is most necessary to make a strong stroke when putting within 1 meter. If the target is 1 to 1.4 meters, hole cup also contains break positions. Therefore, it is necessary to look around the putting green area and set the target, but do not leave the center of the hole cup. For a 1.8 meter putt, the ball may deviate and be affected by the slope. Therefore, it is necessary to calculate the degree of deviation according to the slope. The slower the speed, the more affected by the slope, so it is desirable to hit relatively strong. It is also preferable to use the center of a hole cup as a reference when calculating the departure.

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Appendix 1. Internal consistency reliability for repeated experiments

|  |  | Number | Cronbach's a |
| :---: | :---: | :---: | :---: |
| Flat $y$-axis | 20 cm | 20 | . 997 |
|  | 25 cm |  |  |
|  | 30 cm |  |  |
|  | 35 cm |  |  |
| $\begin{gathered} \text { Flat } \\ \text { x-axis } \end{gathered}$ | 20 cm | 20 | . 997 |
|  | 25 cm |  |  |
|  | 30 cm |  |  |
|  | 35 cm |  |  |
| Flat <br> z-axis | 20 cm | 20 | . 997 |
|  | 25 cm |  |  |
|  | 30 cm |  |  |
|  | 35 cm |  |  |
| Low slope $y$-axis | 20 cm | 20 | . 997 |
|  | 25 cm |  |  |
|  | 30 cm |  |  |
|  | 35 cm |  |  |
| Low slope $x$-axis | 20 cm | 20 | . 993 |
|  | 25 cm |  |  |
|  | 30 cm |  |  |
|  | 35 cm |  |  |
| Low slope z-axis | 20 cm | 20 | . 977 |
|  | 25 cm |  |  |
|  | 30 cm |  |  |
|  | 35 cm |  |  |
| High slope $y$-axis | 20 cm | 20 | . 978 |
|  | 25 cm |  |  |
|  | 30 cm |  |  |
|  | 35 cm |  |  |
| High slope $y$-axis | 20 cm | 20 | . 994 |
|  | 25 cm |  |  |
|  | 30 cm |  |  |
|  | 35 cm |  |  |
| High slope $y$-axis | 20 cm | 20 | . 985 |
|  | 25 cm |  |  |
|  | 30 cm |  |  |
|  | 35 cm |  |  |

Appendix 2. Analysis of variance of $x$ axis variable according to slope

| Variables (x) |  | F |  | L |  | H |  | F | $p$ | Post-hoc |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{M} \pm$ SD |  | $\mathrm{M} \pm$ SD |  | $\mathrm{M} \pm$ SD |  |  |  |  |
| 20D | P20D 50 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 1.00 |  |
|  | P20D 100 | 0.04 | 0.03 | 0.07 | 0.03 | 0.12 | 0.06 | 4.90 | . 027 | $\mathrm{F}<\mathrm{H}$ |
|  | P20D 110 | 0.05 | 0.03 | 0.12 | 0.00 | 0.23 | 0.05 | 38.0 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |
|  | P20D 120 | 0.01 | 0.03 | 0.16 | 0.03 | 0.28 | 0.03 | 91.0 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |
|  | P20D 130 | 0.02 | 0.03 | 0.20 | 0.05 | 0.34 | 0.03 | 73.0 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |
|  | P20D 140 | 0.05 | 0.03 | 0.25 | 0.03 | 0.35 | 0.07 | 45.4 | . 001 | $\mathrm{F}<\mathrm{L}, \mathrm{H}$ |
|  | P20D 150 | 0.02 | 0.03 | 0.25 | 0.03 | 0.38 | 0.05 | 106 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |
|  | P20D 160 | 0.06 | 0.04 | 0.29 | 0.03 | 0.28 | 0.03 | 68.6 | . 001 | $\mathrm{F}<\mathrm{L}, \mathrm{H}$ |
|  | P20D 170 | 0.06 | 0.04 | 0.29 | 0.05 | 0.23 | 0.03 | 41.6 | . 001 | F<L, H |
|  | P20D 180 | - | - | - | - | - | - | - | - | - |
| 25D | P25D 50 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 1.00 |  |
|  | P25D 100 | 0.01 | 0.01 | 0.01 | 0.01 | 0.07 | 0.07 | 6.0 | . 016 | $\mathrm{F}<\mathrm{H}, \mathrm{L}<\mathrm{H}$ |
|  | P25D 110 | 0.01 | 0.01 | 0.058 | 0.07 | 0.16 | 0.03 | 17.7 | . 001 | $\mathrm{F}<\mathrm{H}, \mathrm{L}<\mathrm{H}$ |
|  | P25D 120 | 0.01 | 0.01 | 0.05 | 0.07 | 0.20 | 0.03 | 31.6 | . 001 | $\mathrm{F}<\mathrm{H}, \mathrm{L}<\mathrm{H}$ |
|  | P25D 130 | 0.01 | 0.01 | 0.13 | 0.03 | 0.28 | 0.03 | 158 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |
|  | P25D 140 | 0.01 | 0.01 | 0.17 | 0.05 | 0.30 | 0.01 | 134 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |
|  | P25D 150 | 0.01 | 0.01 | 0.24 | 0.01 | 0.36 | 0.01 | 196 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |
|  | P25D 160 | 0.01 | 0.01 | 0.28 | 0.03 | 0.42 | 0.01 | 632 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |
|  | P25D 170 | 0.02 | 0.05 | 0.29 | 0.03 | 0.43 | 0.03 | 148 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |
|  | P25D 180 | 0.02 | 0.05 | 0.30 | 0.04 | 0.42 | 0.01 | 132 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |
| 30D | P30D 50 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 1.00 |  |
|  | P30D 100 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 1.00 |  |
|  | P30D 110 | 0.02 | 0.05 | 0.02 | 0.05 | 0.07 | 0.07 | 1.1 | . 351 |  |
|  | P30D 120 | 0.01 | 0.01 | 0.05 | 0.07 | 0.1 | 0.05 | 4.8 | . 029 | $\mathrm{F}<\mathrm{H}$ |
|  | P30D 130 | 0.02 | 0.05 | 0.1 | 0.05 | 0.17 | 0.05 | 9.4 | . 004 | $\mathrm{F}<\mathrm{H}$ |
|  | P30D 140 | 0.02 | 0.05 | 0.14 | 0.03 | 0.24 | 0.04 | 30.5 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |
|  | P30D 150 | 0.02 | 0.05 | 0.18 | 0.04 | 0.3 | 0.04 | 44.3 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |
|  | P30D 160 | 0.02 | 0.05 | 0.23 | 0.03 | 0.3 | 0.04 | 56.9 | . 001 | $\mathrm{F}<\mathrm{L}, \mathrm{H}$ |
|  | P30D 170 | 0.02 | 0.05 | 0.24 | 0.04 | 0.38 | 0.03 | 85.5 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |
|  | P30D 180 | 0.02 | 0.05 | 0.31 | 0.03 | 0.41 | 0.03 | 139 | . 001 |  |
| 35D | P35D 50 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 1.00 |  |
|  | P35D 100 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 1.00 |  |
|  | P35D 110 | 0.01 | 0.01 | 0.01 | 0.01 | 0.1 | 0.05 | 16 | . 001 | F, L<H |
|  | P35D 120 | 0.01 | 0.01 | 0.01 | 0.01 | 0.14 | 0.03 | 95.9 | . 001 | F, L<H |
|  | P35D 130 | 0.01 | 0.01 | 0.02 | 0.05 | 0.14 | 0.03 | 22.5 | . 001 | F, L<H |
|  | P35D 140 | 0.01 | 0.01 | 0.1 | 0.05 | 0.18 | 0.01 | 42.3 | . 001 | $F<L<H$ |
|  | P35D 150 | 0.01 | 0.01 | 0.1 | 0.09 | 0.24 | 0.04 | 21.7 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |
|  | P35D 160 | 0.01 | 0.01 | 0.16 | 0.03 | 0.26 | 0.03 | 122 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |
|  | P35D 170 | 0.01 | 0.01 | 0.17 | 0.03 | 0.31 | 0.05 | 112 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |
|  | P35D 180 | 0.01 | 0.01 | 0.2 | 0.03 | 0.31 | 0.05 | 104 | . 001 | $\mathrm{F}<\mathrm{L}<\mathrm{H}$ |

${ }^{*} p<.05,{ }^{* *} p<.01,{ }^{* * *} p<.001$, Flat: F, Low slope: L, High slope: H, Polycarbonate: P, Club head moved 20 cm and freely dropped: 20D Club head moved 25 cm and freely dropped: 25D Club head moved 30 cm and freely dropped: 30D Club head moved 35 cm and freely dropped: 35D

