# Enhanced Crystallization Behaviour and Microwave Dielectric Properties of 0.9CaMgSi<sub>2</sub>O<sub>6</sub>-0.1MgSiO<sub>3</sub> Glass-Ceramics Doped with TiO<sub>2</sub>

# Hyun Jin Jo, Gui Nam Sun, and Eung Soo Kim<sup>†</sup>

Department of Materials Engineering, Kyonggi University, Suwon 16227, Korea (Received February 1, 2016; Revised February 18, 2016; Accepted February 19, 2016)

#### ABSTRACT

The dependence of the microwave dielectric properties of the glass-ceramic composite  $0.9 \text{CaMgSi}_2 \text{O}_6 \cdot 0.1 \text{MgSiO}_3$  on the crystallization behaviour was investigated as functions of the  $\text{TiO}_2$  content and heat-treatment temperature. The crystallization behaviour of the specimens was evaluated via a combination of the Rietveld and reference-intensity ratio methods. For specimens with a  $\text{TiO}_2$  content of up to 1 wt.%, a monoclinic diopside phase was formed, whereas a secondary  $\text{TiO}_2$  phase was formed with further increases in the  $\text{TiO}_2$  content. The quality factor (Qf) of the specimens was strongly dependent on the degree of crystallization. The highest Qf value was obtained with a  $\text{TiO}_2$  content of 0.5 wt.%, which was improved by increasing the heat-treatment temperature. The dielectric constant (K) was affected by the size of the crystallites and the  $\text{TiO}_2$  content. The temperature coefficient of the resonant frequency (TCF) was nearly constant for all of the specimens, regardless of the  $\text{TiO}_2$  content or heat-treatment temperature.

Key words: Glass-ceramics, Diopside, Enstatite, Microwave dielectric properties, Degree of crystallization

## 1. Introduction

**I** n recent years, the applicability of low-temperature cofired ceramics (LTCCs) to technology has been widely investigated to meet the demand for miniaturized and multifunctional electronic devices. The key properties required for LTCC-based substrate materials include a low dielectric constant (K), high quality factor (Qf), near-zero temperature coefficient of the resonant frequency (TCF), and heat-treatment temperature that is much lower than the melting points of commonly used metallic electrodes (Ag, Au, or Cu).

CaMgSi $_2$ O $_6$  and MgSiO $_3$  (diopside and enstatite, respectively) glass-ceramic composites are good candidates for LTCC-based substrate materials because of the low heat-treatment temperature, low K, high Qf, and high mechanical strength of such systems. It has been reported that the dielectric properties of glass-ceramic composites can be affected by the density, porosity, crystalline phases formed, and degree of crystallization. According to our preliminary experiments, the glass-ceramic composite 0.9CaMgSi $_2$ O $_6$ -0.1MgSiO $_3$  exhibits a high Qf value (36,000 GHz) when a high degree of crystallization is achieved. Therefore, improving the degree of crystallization of 0.9CaMgSi $_2$ O $_6$ -0.1MgSiO $_3$  is the most important factor for enhancing the Qf value.

Various methods have been developed to improve the

<sup>†</sup>Corresponding author: Eung Soo Kim

Tel: +82-31-249-9764 Fax: +82-31-244-6300

Corresponding author: Eung Soo Kin E-mail: eskim@kyonggi.ac.kr crystallization behaviour of glass-ceramic composites. One such method is controlling the heat-treatment temperature. <sup>2,4,5)</sup> Generally, glass-ceramic composites that are heat-treated at the optimum temperature exhibit enhanced crystallinity. <sup>5)</sup>

Another method for improving the crystallization of glass-ceramic composites is the addition of nucleation agents. With the addition of a nucleation agent, the crystallization of the glass can occur at both the surface and bulk, which can lead to an increase in the degree of crystallization;  $\text{Cr}_2\text{O}_3$  and  $\text{TiO}_2$  have been widely investigated as nucleation agents for the  $\text{CaMgSi}_2\text{O}_6$  system.  $^{4,6\text{-}11)}$ 

Cr<sub>2</sub>O<sub>3</sub> is commonly used as a nucleation agent for diopside glass. It has been reported that the addition of Cr<sub>2</sub>O<sub>3</sub> leads to the formation of heterogeneous nucleation sites in diopside glass; this process causes crystallization via the formation of  $\mathrm{MgCr_2O_4}$  spinel domains.<sup>7)</sup> However, Cr ions can exist in two valence states:  $Cr^{3+}$  and  $Cr^{6+}$ . It has been reported that Cr3+ is miscible with diopside glass at high temperatures, while  $\operatorname{Cr}^{6+}$  separates from the diopside glass at low temperatures because of the high field strength of the hexavalent state. These phenomena can degrade the degree of crystallization of a diopside glass. 9) Therefore, Cr<sub>2</sub>O<sub>3</sub> should be used alongside other nucleation agents for diopside glass, such as Fe<sub>2</sub>O<sub>3</sub> or TiO<sub>2</sub>. On the other hand, TiO<sub>3</sub> is a well-known nucleation agent for diopside glass. It can enter the glass as either a network modifier in the form of TiO<sub>6</sub> at high temperatures, or as a network former in the form of TiO<sub>4</sub> at low temperatures. Once TiO<sub>2</sub> has been transformed into TiO6, it can decrease the viscosity of the glass, thereby increasing the mobility during crystallization. Therefore, the addition of  ${\rm TiO_2}$  can enhance the crystallization behaviour of diopside glass. <sup>10,11)</sup> Thus, it is expected that the crystallinity of diopside glass can be improved by adding an optimum concentration of  ${\rm TiO_2}$ .

Even though many studies have investigated the effects of TiO<sub>2</sub> on glass-ceramic composites, the two factors controlling the degree of crystallization have not been sufficiently clarified, i.e., the optimum concentration of TiO, for glass-ceramic composites and the relationship between the dielectric properties and the degree of crystallization have not been reported. Moreover, the effects of the TiO<sub>2</sub> content and the heat-treatment temperature on the crystallization behaviour of 0.9CaMgSi<sub>2</sub>O<sub>6</sub>-0.1MgSiO<sub>3</sub> have not yet been investigated. Therefore, in this study, the microwave dielectric properties of 0.9CaMgSi<sub>2</sub>O<sub>6</sub>-0.1MgSiO<sub>3</sub> were investigated as functions of the TiO2 content (0-6 wt.%) and the heat-treatment temperature. The crystallization behaviour of the specimens will be discussed based on how the degree of crystallization varies with the TiO2 content and the heattreatment temperature.

# 2. Experimental Procedures

 $\rm CaCO_3$  (99.9%), MgCO $_3$  (99.9%), SiO $_2$  (99.9%), and TiO $_2$  (99.9%) powders were used as the precursor materials. The powders were mixed to achieve the desired composition of  $\rm 0.9CaMgSi_2O_6-0.1MgSiO_3$ , with the  $\rm TiO_2$  content ranging from 0 to 6 wt.%; samples were ball-milled with  $\rm ZrO_2$  balls for 24 h in ethanol. The mixed powders were then melted in Pt crucibles at 1500°C for 3 h and quenched in distilled water. Cullet of the samples was obtained by pulverizing the quenched products, which were then sieved through size-50 meshes. The glass frits were re-milled for 24 h and isostatically pressed into pellets at a pressure of 147 MPa. The pellets were then heat-treated at 850-950°C for 3 h in air

The densities of the heat-treated specimens were measured via the Archimedes' method. The crystalline phases and crystallization behaviours of the specimens were analysed with X-ray diffraction (XRD, D/Max-2500V/PC, RIGAKU, Japan). Scanning electron microscopy (SEM, JSM-6700F, JEOL, Japan) was used to evaluate the phase and crystallite size of the glass-ceramic specimens.

To evaluate the degree of crystallization of the specimens via a combination of Rietveld and reference-intensity ratio (RIR) methods, a sample of 10 wt.% a-Al $_2$ O $_3$ , which was annealed at 1500°C for 24 h to increase the crystallinity to 100%, was added to all of the samples to act as an internal standard. Rietveld refinements of the XRD patterns were performed with the Full-Prof program. The degree of crystallization of the samples was evaluated against the internal standard with Eq. (1):

$$\alpha = \left(\frac{W_c}{W_{cd}}\right) \left(\frac{W_{std}}{W}\right) \tag{1}$$

where W,  $W_c$ , and  $W_{std}$  are the weights of the specimen, crys-

talline component, and internal standard, respectively. The value of  $W_c/W_{std}$  was calculated from the Rietveld quantitative analysis under the condition of  $W_c+W_{std}=1$ . The value of  $W_{std}/W$  was determined by measuring the weights of the specimen and of the internal standard. The microwave dielectric properties were measured according to the method reported by Hakki and Coleman with the  $TE_{011}$  mode in the range of 11-13 GHz. The TCF values of the specimens were measured according to the cavity method over a temperature range of 25 - 80°C.

## 3. Results and Discussion

#### 3.1. Physical Properties

The relative densities of the  $0.9 {\rm CaMgSi_2O_6}\text{-}0.1 {\rm MgSiO_3}$  specimens with various  ${\rm TiO_2}$  contents (0-6 wt.%) that were heat-treated at 850-950°C for 3 h are shown in Fig. 1. As the  ${\rm TiO_2}$  content increases, the relative densities of all of the specimens decrease, but remain above 90% regardless of the  ${\rm TiO_2}$  content.

Figure 2 provides SEM micrographs of the  $0.9 {\rm CaMgSi}_2 {\rm O}_6$   $0.1 {\rm MgSiO}_3$  specimens with  ${\rm TiO}_2$  contents of 0.5, 2, and 6 wt.% that were heat-treated at  $850^{\circ}{\rm C}$  for 3 h. As the  ${\rm TiO}_2$  content increases, the porosity increases because of the decreasing relative density, as shown in Fig. 1. These results can be attributed to the weak adhesion at the interfaces between the diopside (glass) and  ${\rm TiO}_2$  (ceramic) phases, which arises from the degradation of pore elimination during the densification process and/or the difference between the thermal expansion coefficients of the diopside  $(8.40\times 10^6\,{\rm ^oC^{-1}}$  (crystal),  $6.65\times 10^6\,{\rm ^oC^{-1}}$  (glass) $^{17}$ ) and  ${\rm TiO}_2$  phases  $(8.9210^{-6}{\rm ^oC}^{1}$   $^{18}$ ). Considering the globular shape of the pores shown in Fig. 2, the degradation of pore elimination during the densification process is a major factor in the weak adhesion.

Figure 3 provides XRD patterns of the 0.9CaMgSi<sub>2</sub>O<sub>6</sub>-0.1MgSiO<sub>3</sub> specimens with various TiO<sub>2</sub> contents (0-6 wt.%)

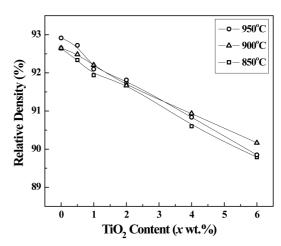


Fig. 1. Relative densities of the  $0.9 {\rm CaMgSi_2O_6}$ - $0.1 {\rm MgSiO_3}$  specimens with various  ${\rm TiO_2}$  contents (0-6 wt.%) that were heat-treated at 850-950°C for 3 h.

Fig. 2. SEM micrographs of the 0.9CaMgSi $_2$ O $_6$ -0.1MgSiO $_3$  specimens with various TiO $_2$  contents (0.5-6 wt.%) that were heat-treated at 850-950 °C for 3 h: (a) 0.5, (b) 2, and (c) 6 wt.%.

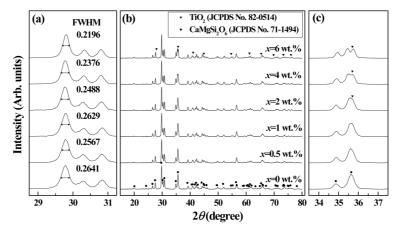


Fig. 3. XRD patterns of the  $0.9 \text{CaMgSi}_2 \text{O}_6$ - $0.1 \text{MgSiO}_3$  specimens with various  $\text{TiO}_2$  contents (0-6 wt.%) that were heat-treated at  $850^{\circ}\text{C}$  for 3 h: (a)  $2q = 29 \cdot 31^{\circ}$ , (b)  $2q = 15 \cdot 80^{\circ}$ , and (c)  $2q = 34 \cdot 37^{\circ}$ .

that were heat-treated at 850°C for 3 h. The XRD patterns show that a single monoclinic diopside phase (CaMgSi<sub>2</sub>O<sub>6</sub>, JCPDS No. 71-1494) is detected for TiO<sub>2</sub> contents of up to 1 wt.% (Fig. 3(b)). However, a secondary TiO<sub>2</sub> phase (JCPDS No. 82-0514) becomes evident with further increases in the TiO<sub>2</sub> content; this is confirmed by the XRD peak at  $2q = 35.5^{\circ}$  splitting into the diopside and TiO<sub>2</sub> phases (Fig. 3(c)).

To determine the crystallite size (L) of the specimens, the full width at half-maximum (FWHM) values of the XRD peaks were calculated with the Scherrer Equation  $(Eq. (2))^{19}$ :

$$L = \frac{0.89\lambda}{B\cos\theta} \tag{2}$$

where L is the crystallite size, l is the wavelength of the X-ray radiation (l=0.154 nm), B is the FWHM of the peak (in radians) after being corrected for instrumental broadening, and q is the Bragg angle. As the FWHM of an XRD peak decreases, the crystallite size increases. Fig. 3(a) shows that the specimens containing less than 1 wt.% of  ${\rm TiO_2}$  have similar FWHM values, while those with  ${\rm TiO_2}$  contents greater than 1 wt.% exhibit reduced FWHM values, which indicates that the crystallite size has increased.

#### 3.2. Microwave Dielectric Properties

Figure 4 shows the relationship between the Qf values of

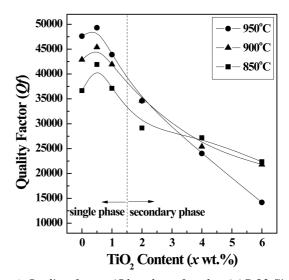


Fig. 4. Quality factor (Qf) values for the 0.9CaMgSi<sub>2</sub>O<sub>6</sub>-0.1MgSiO<sub>3</sub> specimens with various TiO<sub>2</sub> contents (0-6 wt.%) that were heat-treated at 850-950°C for 3 h.

the  $0.9 \text{CaMgSi}_2 \text{O}_6$ - $0.1 \text{MgSiO}_3$  specimens and the  $\text{TiO}_2$  content (0 - 6 wt.%), as well as the effects of the heat-treatment temperature on the Qf values. The maximum Qf value for each temperature is achieved when the  $\text{TiO}_2$  content is 0.5 wt.%, and then the Qf values gradually decrease with fur-

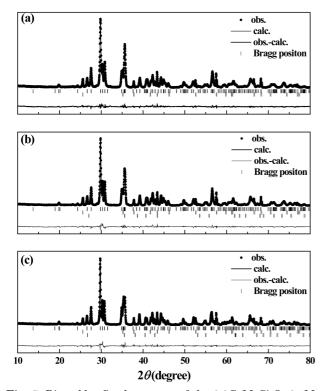


Fig. 5. Rietveld-refined patterns of the  $0.9 \mathrm{CaMgSi_2O_6}$ - $0.1 \mathrm{MgSiO_3}$  specimens with various  $\mathrm{TiO_2}$  contents (0.5-6 wt.%) that were heat-treated at 850-950°C for 3 h: (a) 0.5, (b) 2, and (c) 6 wt.%.

ther increases in the  ${\rm TiO_2}$  content. In addition, the Qf values increase as the heat-treatment temperature increases from 850 to 950°C. Generally, the Qf value of a glass-ceramic composite is strongly dependent on the degree of crystallization, which can be improved by either adding a nucleation agent, such as  ${\rm TiO_2}$ , or increasing the heat-treatment temperature.

To evaluate the crystallinity of the  $0.9{\rm CaMgSi_2O_6}\text{-}0.1{\rm Mg-SiO_3}$  specimens with various  ${\rm TiO_2}$  contents (0-6 wt.%) that were subjected to heat treatments at different temperatures, the Rietveld-RIR method described in section 2 was used. The resulting Rietveld-refined patterns are shown in

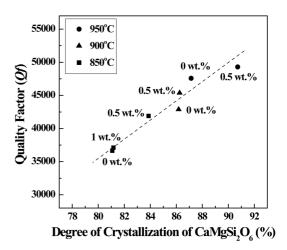


Fig. 6. Dependence of the quality factor (Qf) on the degree of crystallization of the  $0.9\mathrm{CaMgSi}_2\mathrm{O}_6$ - $0.1\mathrm{MgSiO}_3$  specimens with various  $\mathrm{TiO}_2$  contents (0-1 wt.%) that were heat-treated at 850-950°C for 3 h.

Fig. 5. The data points represent the measured intensities, the overlying solid lines are the calculated intensities, and the lower lines show the differences between the observed and calculated intensities. In addition, the short vertical bars indicate the Bragg reflections that correspond to the monoclinic diopside (top row), a-Al<sub>2</sub>O<sub>3</sub> (middle row), and  $\text{TiO}_2$  (bottom row) phases. Table 1 shows that the *R*-factors, i.e. the goodness of fit (*GoF*), profile factor ( $R_p$ ), weighted profile factor ( $R_{vp}$ ), and expected weighted profile factor results are reliable.

Figure 6 shows the dependence of the Qf values on the degree of crystallization of the glass-ceramic composites. For the specimens composed of a single diopside phase ( $\text{TiO}_2$  content = 0-1 wt.%), the highest degree of crystallization is obtained with a  $\text{TiO}_2$  content of 0.5 wt.%; the crystallization then decreases and is nearly constant with further increases in the  $\text{TiO}_2$  content, as shown in Table. 1. In addition, the degree of crystallization of the specimens with  $\text{TiO}_2$  contents of 0.5 wt.% is enhanced as the heat-treatment temperature increases from 850 to 950°C. These tendencies are reflected

 $\begin{tabular}{ll} \textbf{Table 1.} Results of the Rietveld-RIR Quantitative Analysis of the $0.9$CaMgSi$_2O$_6-0.1MgSiO$_3 Specimens with Various TiO$_2 Contents (0-6 wt.%) that were Heat-Treated at $50-950^{\circ}$C for 3 h $0.950^{\circ}$ Contents (0-6 wt.%) at the content of the c$ 

${ m TiO_2}$ (wt.%)	0		0.5		1	2	4	6
Heat-treatment temperature (°C)	850	850	900	950	850			
Degree of crystallization of $\mathrm{CaMgSi_2O_6}$ (%)	81.79	83.87	86.25	87.15	81.17	79.36	81.64	80.20
$TiO_2$ (%)	0	0	0	0	0	0.35(4)	0.65(2)	0.77(7)
Glass (%)	18.21	16.13	13.75	12.85	18.83	20.29	17.71	19.03
Total (%)	100.00	100.00	100.00	100.00	100.00	99.9	99.9	99.9
GoF	1.6	1.5	1.5	1.5	1.5	1.6	1.5	1.5
$R_{ m p}$	8.71	8.26	8.35	8.54	8.6	9.02	9.09	9.52
$R_{ m wp}$	11.1	10.4	10.5	10.7	10.9	11.4	11.2	11.6
$R_{ m exp}$	7.1	7.01	6.99	7.12	7.12	7.09	7.23	7.26

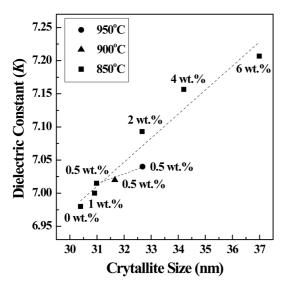


Fig. 7. Dependence of the dielectric constant (K) on the crystallite size of the  $0.9 \mathrm{CaMgSi}_2 \mathrm{O}_6$ - $0.1 \mathrm{MgSiO}_3$  specimens with various  $\mathrm{TiO}_2$  contents (0 - 6 wt.%) that were heat-treated at 850-950°C for 3 h.

in the trends of the Qf values of the specimens, as shown in Fig. 4. This is because single crystals always have smaller dielectric losses than the corresponding glass and, thus, high Qf values of the specimens are obtained when there is a high degree of crystallization.<sup>20)</sup> In addition, the Qf value of the specimen containing 0.5 wt.% of  $TiO_2$  and heat-treated at  $950^{\circ}$ C (Qf = 49,300 GHz) is similar to that of the  $CaMgSi_2O_6$  ceramics sintered at  $1290^{\circ}$ C (Qf = 59,600 GHz<sup>21)</sup>), but the dielectric properties are not highly degraded because of the lower heat-treatment temperature.

Figure 7 shows the dependence of *K* on the crystallite size of the 0.9CaMgSi<sub>2</sub>O<sub>6</sub>-0.1MgSiO<sub>3</sub> specimens with various TiO<sub>2</sub> contents (0-6 wt.%) that were heat-treated at 850-950°C for 3 h. The crystallite sizes of the specimens are similar for TiO<sub>2</sub> contents of up to 1 wt.%; then, the crystallite sizes increase from 30.8 to 37.0 nm with further increases in the TiO<sub>2</sub> content, as shown in Fig. 3(a). The crystallite size increases with increasing TiO, content because of the accelerated grain growth that is caused by heterogeneous nucleation.<sup>22)</sup> For the specimens with TiO<sub>2</sub> contents of 0.5 wt.%, the crystallite size also increases as the heat-treatment temperature increases from 850 to 950°C. It has been reported that K is dependent on the crystallite size of the specimens because of the reduced porosity of the interfaces between the grains.  $^{3,23,24)}$  In addition, the increasing K values of the specimens could be caused by the higher intrinsic K of the secondary  $\text{TiO}_2$  phase  $(K_{\text{TiO}2} = 100^{25})$ , while K = 6.98for the  $0.9CaMgSi_2O_6$ - $0.1MgSiO_3$  phase).

The TCF values of the  $0.9 {\rm CaMgSi_2O_6}$ - $0.1 {\rm MgSiO_3}$  specimens with various  ${\rm TiO_2}$  contents (0-6 wt.%) that were heattreated at 850-950°C for 3 h did not change significantly with the  ${\rm TiO_2}$  content and/or heat-treatment temperature; the TCF values were approximately -20 ppm/°C for all of the compositions tested.

# 4. Conclusions

In this study, the effects of the TiO<sub>2</sub> content (0-6 wt.%) and heat-treatment temperature on the microwave dielectric properties of 0.9CaMgSi<sub>2</sub>O<sub>6</sub>-0.1MgSiO<sub>3</sub> glass-ceramic composites were investigated. The specimens with TiO2 contents of up to 1 wt.% and heat-treated at 850°C for 3 h exhibited a single phase of diopside (CaMgSi,O6), and then a secondary TiO2 phase became evident with further increases in the TiO2 content. For the specimens composed of a single diopside phase, the Qf values of these specimens were dependent on the degree of crystallization, which was affected by both the TiO2 content and the heat-treatment temperature; the highest degree of crystallization was achieved when the TiO<sub>2</sub> content was 0.5 wt.%. Moreover, the degree of crystallization of the specimens with TiO<sub>2</sub> contents of 0.5 wt.% was improved by increasing the heat-treatment temperature. The K values of the specimens were mainly affected by the size of the crystallites, while the TCF values did not change significantly. By adding 0.5 wt.% of  $TiO_2$  to the  $0.9CaMgSi_2O_6$ - $0.1MgSiO_3$  glass-ceramic composite (Qf = 49,300 GHz), the heat-treatment temperature was effectively lowered to 950°C.

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