

# Triple-Mode Characteristics of Cylindrical Cavity Loading a Cylindrical Dielectric Resonator

Seung-Mo Lee\*, Cha-Man Kim\*, Jong-Chul Park\*, In-Ryeol Kim\*\*, Soon-Soo Oh\*\*\*

**Abstract** In this paper, a novel triple-mode cavity structure, designed for compactness and operating at 850 MHz, is analyzed. A cylindrical dielectric resonator is loaded into a metallic cylindrical cavity. Previous study has been focused on the analysis of the cylindrical dielectric resonator, but in this paper, the effect of the cylindrical metallic cavity has been analyzed. Enclosing the dielectric resonator inside the metallic cavity increases the resonant frequency of the dielectric resonator; however, this increases the quality factor and introduces the possibility of installing coupling screws. The principle of generation of triple-mode was investigated by parametric analysis. The generated triple-mode is TE<sub>011</sub> mode and two orthogonally generated HEM<sub>121</sub> modes. By adjusting the radius of the dielectric resonator, the height of the dielectric resonator, or the radius of the cylindrical metallic cavity, three modes could be coincided. However, the height of the metallic cavity keeps three modes separated. The mode characteristics of the proposed cavity are analyzed using a full-wave electromagnetic (EM) simulation. The proposed triple-mode cavity could be developed to triple-mode filter using a coupling screw, and the commercial application for the miniaturized filter below 1 GHz could be expected.

**Key Words** : Dielectric resonator, waveguide filter, cavity resonator, triple mode, metallic cavity

## 1. Introduction

The 800MHz band is interesting in the area of cellular communications; however, there are several problems with miniaturization of microwave devices at this frequency because of the relatively large wavelength [1]. Specifically, metallic waveguide filters operating at 800MHz are heavy and bulky, and integration with base-station antennae is difficult.

Several techniques have been used to decrease filter size, such as the development of dielectric-filled waveguides [2], high-permittivity dielectric resonators [3], or multiple modes [4]. Among these, generation of triple modes in one resonator shows great promise and introduces

the possibility of efficient space utilization, as well as integration with other techniques, for example, a dielectric resonator [5] or microstrip filter [6-7] with triple modes.

This paper proposes a novel triple-mode cavity structure operating at 850MHz, analyzes the field distribution of the proposed cavity is using rigorous electromagnetic software, and describes the operating principles

## 2. Configuration

Fig. 1 shows the configuration of the proposed cavity. A cylindrical dielectric resonator is positioned in the center of a metallic cylindrical cavity. The

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radius and height of the dielectric cylinder are  $R_D = 26\text{mm}$  and  $H_D = 48\text{mm}$ , respectively. The cavity encloses the dielectric resonator, which increases the resonant frequency of the dielectric resonator; however, the quality factor may be increased, and coupling screws may be installed. The radius and height of the metallic cylinder are  $R_C = 45\text{mm}$  and  $H_C = 80\text{mm}$ , respectively.

### 3. Field Analysis

#### 3.1 Parametric Study

In order to investigate the parametric effect, the commercial software ANSYS HFSS based on a finite element method was used, and the resonant mode was measured directly using the eigenvalue mode analysis embedded function, without applying a feeding structure [8]. The parameters  $R_D$ ,  $H_D$ ,  $R_C$ , and  $H_C$  were set to initial values of 26, 48, 45, and 80mm, respectively.

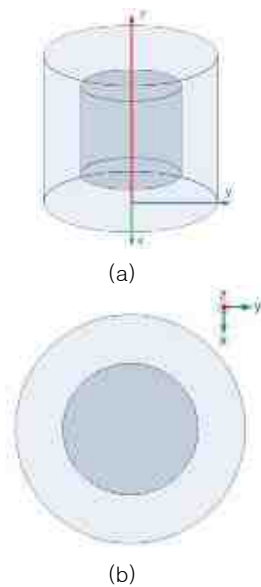


Fig. 1 Configuration of the proposed triple-mode cavity. (a) Perspective view, (b) top view

First, the dielectric resonator was examined. As shown in Fig. 2(a), the radius of the

dielectric resonator  $R_D$  was swept from 16 to 36mm. The resultant resonant frequency drops from about 1.2 GHz to 700MHz over this range. This study indicated that the radius  $R_D$  was the most critical parameter determining the resonant frequency of the cavity. Note that for  $R_D < 25\text{mm}$ , the lowest mode is the  $TE_{011}$  mode, while for  $R_D > 25\text{mm}$  the lowest mode becomes the  $HEM_{121}$  mode. A similar phenomenon was found for the ranges of  $H_D$  and  $R_C$  investigated. Therefore, it is possible to excite three modes with identical frequencies in the same space; this, however, requires consideration when designing coupling or feeding structures.

As shown in Fig. 2(b), the height of the dielectric cylinder was swept from 38 to 58mm. The resonant frequency dropped over this range from about 880 to 830MHz for the  $TE_{011}$  mode, and from 930 to 820MHz for the  $HEM_{121}$  mode.

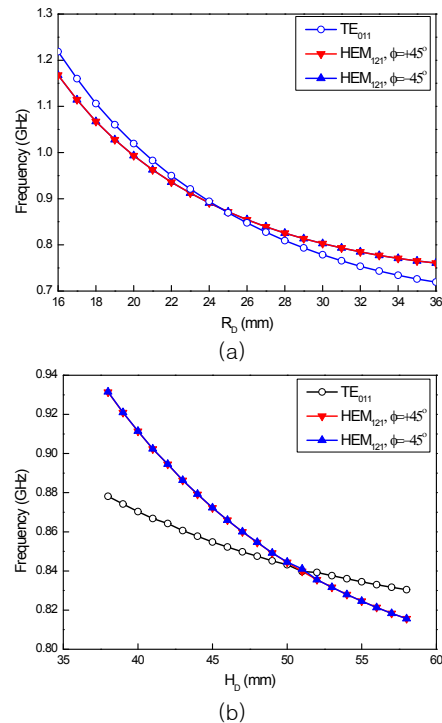


Fig. 2 Resonant frequency versus dielectric resonator parameters. (a) radius  $R_D$ , (b) height,  $H_D$ .

Second, the metallic cylindrical cavity was examined. The radius of the cylindrical cavity RC was swept from 35 to 55mm, as shown in Fig. 3(a). The resonant frequency in this range dropped from about 915 to 825MHz for the TE<sub>011</sub> mode, and from 895 to 840MHz for the HEM<sub>121</sub> mode. Interestingly, the lowest mode, for RC < 41mm is the HEM<sub>121</sub> mode.

As shown in Fig. 3(b), the height of the metallic cavity was tuned from 70 to 90mm. The resultant resonant frequency dropped from about 855 to 845MHz for the TE<sub>011</sub> mode and from 865 to 845MHz for the HEM<sub>121</sub> mode. Compared with other parameters, the smallest frequency variation was observed when changing the height of the cavity, although the energy can be confined to the cavity. The lowest mode was the TE<sub>011</sub> mode over the full range of heights from 70 to 90mm.

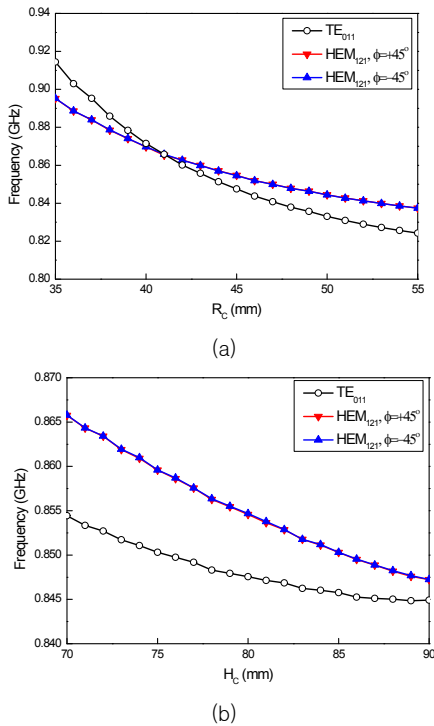


Fig. 3 Resonant frequency versus metallic cavity parameters. (a) radius RC, (b) height, HC.

### 3.2 Electric-Field Distribution

Fig. 4 shows the electric field profile of the TE<sub>011</sub> mode resonating at 848MHz. The left hand side shows the magnitude of the contour, and the right hand side shows the vector flow of the electric field. The variation along the azimuthal direction is zero and the variation along the radial direction shows one peak, as shown in Fig. 4(a). The variation along the radial and height directions has one peak, shown in Fig. 4(b).

Fig. 5 shows that HEM<sub>121</sub> $\phi = +45^\circ$  has a peak at  $\phi = +45^\circ$  and Fig. 6 shows that HEM<sub>121</sub> $\phi = -45^\circ$  has a peak at  $\phi = -45^\circ$ , and the electric field distribution is similar, but rotated through 90 degrees. As they are orthogonally degenerated modes, their resonant frequencies are identical [9]. Since the variation along the cavity height has one peak, the generated mode is denoted the HEM<sub>121</sub> mode rather than the HEM<sub>126</sub> mode. This convention is also applied to the TE<sub>011</sub> mode.

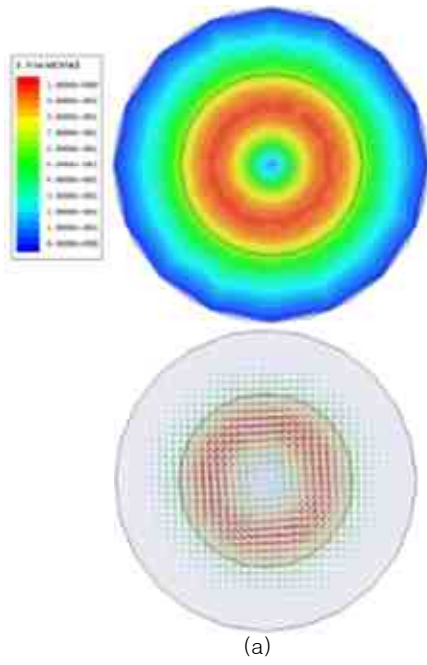


Fig. 4 TE<sub>011</sub> mode of proposed cavity. (a) y-z plane, (b) x-y plane.

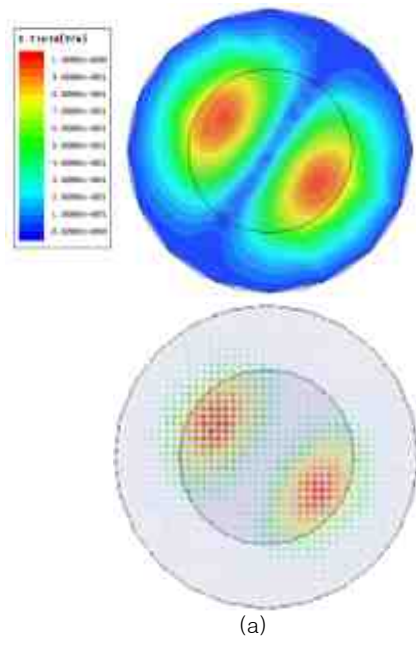


Fig. 5 HEM<sub>121</sub>  $\phi = +45^\circ$  mode of proposed cavity. (a) y-z plane, (b)  $\phi = +45^\circ$  plane.

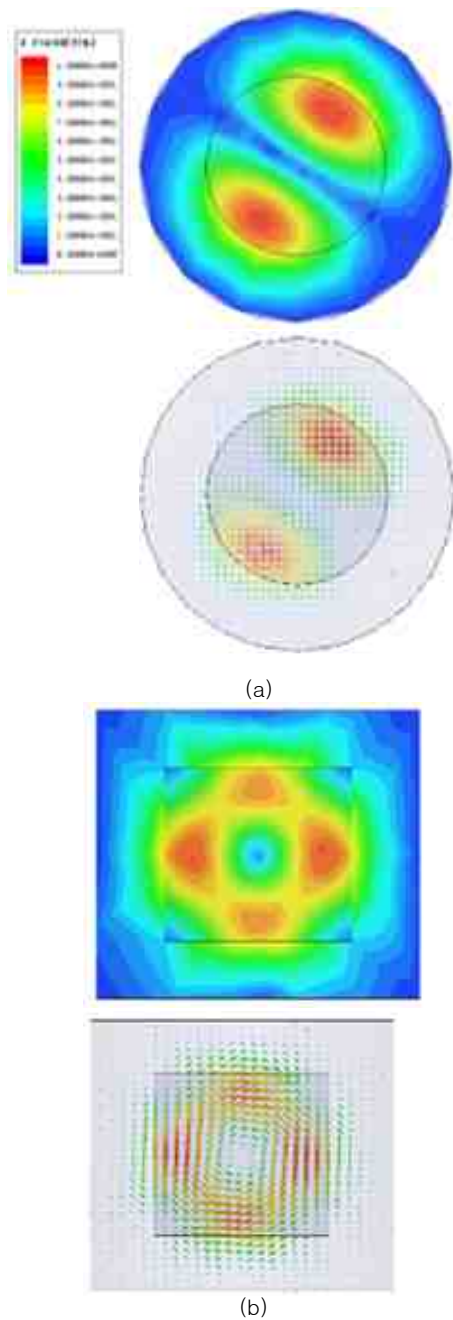


Fig. 6 HEM<sub>121</sub> $\phi = -45^\circ$  mode of proposed cavity. (a)  $y-z$  plane, (b)  $\phi = -45^\circ$  plane.

#### 4. Conclusion

This paper proposed a triple-mode cavity, designed for compactness and operating at 850MHz and a performed parametric study, including a field distribution analysis. A cylindrical dielectric resonator is loaded in order to generate the TE<sub>011</sub> mode and two degenerated HEM<sub>121</sub> modes. The mode characteristics of the proposed cavity were analyzed using full-wave electromagnetic (EM) simulation. By adjusting the radius of the dielectric resonator, the height of the dielectric cylinder, or the radius of the cylindrical cavity, three modes could be coincided. The proposed triple-mode cavity could be developed to triple-mode filter using a coupling screw.

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