

# Charge Controlled Meminductor Emulator

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**Abstract**—Emulations of memristor-family elements are very important, since their physical realizations are very difficult to achieve with recent technologies. Although some previous studies succeeded in designing memristor and memcapacitor emulators, no significant contribution towards meminductor emulator has been presented so far. The implementation of a meminductor emulator is very important, since real meminductors are not expected to appear in near future. We designed the first meminductor emulator whose inductance can be varied by an external current source without employing any memristive system. The principle of our architecture and its feasibility have been verified using SPICE simulation.

**Index Terms**—Pinched hysteresis loop, memristor, memcapacitor, meminductor, emulator

## I. INTRODUCTION

Memristors, memcapacitors, and meminductors are the three major elements of the memristor-family. They are passive circuit elements that store information in the form of resistance, capacitance, and inductance, respectively [1]. Although, these three elements are promising for the implementation of memory smaller than conventional silicon memories, they are not expected to be available in the market in near future. Utilizing emulators might be essential for the

development of application circuits of memristor-family elements. Though there is active research on memristor and memcapacitor emulators [2, 3], there are not many studies on meminductors. The contributions toward meminductors are only confined to build mathematical models, spice macro models, and the transformation of memristive systems to memcapacitive and meminductive systems using mutator [4-8]. However, the mathematical model and spice macro models are only useful for simulation and cannot be used for physical implementable circuits. Similarly, the meminductor built in an indirect way by employing mutator is complicated and leads to difficulty in employing meminductor application circuits.

In this paper, we propose the first simple and dedicated meminductor emulator that does not require any mutator to transform memristor to meminductor. The features of the proposed meminductor has been verified via PSPICE circuit simulations.

## II. PROPOSED MEMINDUCTOR EMULATOR

The relationship between the input current ( $i_{in}$ ) and flux ( $\varphi$ ) in the charge-controlled meminductor is defined as:

$$\varphi(t) = L_M(q)i_{in}(t) \quad (1)$$

where  $L_M(q)$  is the meminductance of a meminductor.

The basic idea to build a meminductor emulator is by composing the input inductance as a function of input current. Figs. 1(a) and (b) show the basic concept and its equivalent circuit respectively to design a meminductor emulator.

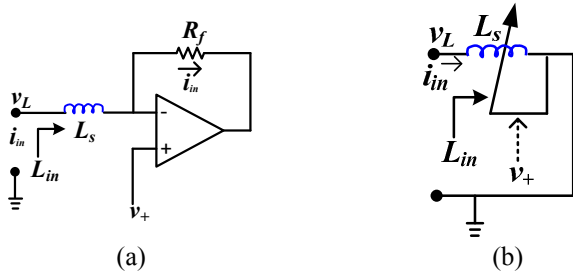
In Fig. 1(a), the relationship between input current  $i_{in}$  and flux  $\varphi$  generated across inductor  $L_s$  is given as:

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**Fig. 1.** Basic concept of proposed meminductor emulator (a) Input inductance as a function of voltage  $v_+$ , (b) Equivalent circuit.

$$\varphi(t) = L_s i_{in}(t) + \int v_+ dt \quad (2)$$

where  $v_+$  is the voltage across the non-inverting terminal of the OPAMP circuit.

If the integration of  $v_+$  in (2) is composed in proportion to the input current  $i_{in}$ , then:

$$\varphi(t) = (L_s + m) i_{in}(t) \quad (3)$$

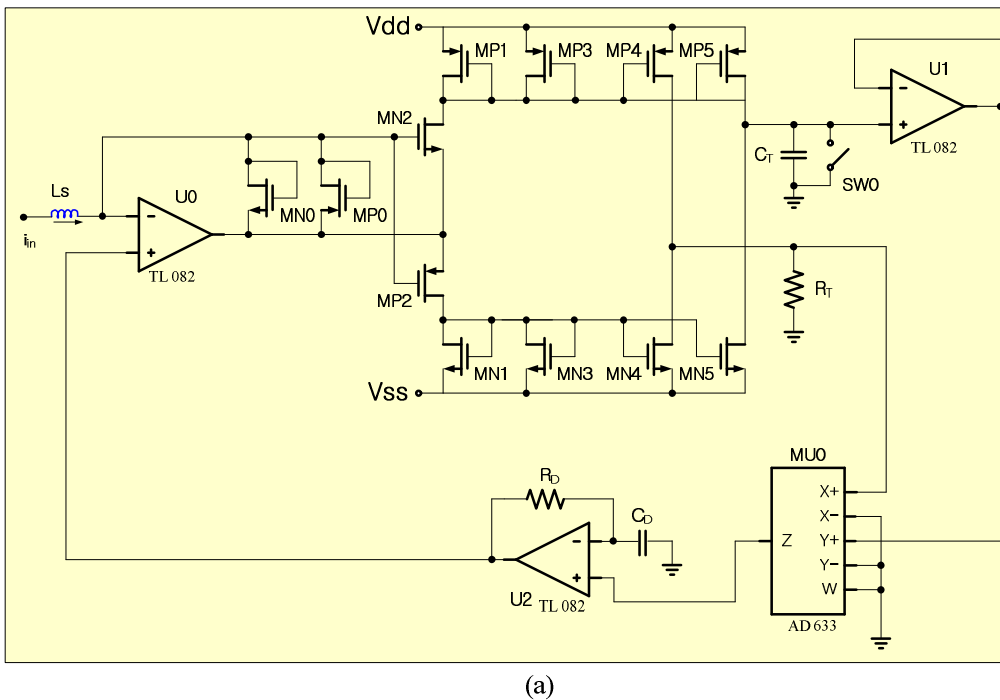
where  $\int v_+ dt = m i_{in}(t)$ . Eq. (3) implies that the meminductance of the charge-dependent meminductor is defined as  $(L_s + m)$ . If  $m$  is controlled by the time integral of  $i_{in}$ , then the circuit of Fig. 1 acts as a meminductor

whose inductance is variable depending upon the integration of the input current. An analog meminductor to emulate  $v_+$  in (3) is constructed using a capacitor, a resistor, an analog multiplier, and a voltage differentiator, as shown in Fig. 2(a).

In Fig. 2(a), an inductor and feedback voltage  $v_+$  are connected across the input terminal and the non-inverting terminal of OPAMP  $U_0$ , respectively. The input current  $i_{in}$  can be expressed in terms of the inductor voltage  $v_L$  and feedback voltage  $v_+$  as:

$$i_{in}(t) = \frac{1}{L_s} \int (v_L(t) - v_+) dt \quad (4)$$

The replicas of positive and negative currents are generated using NMOS and PMOS current mirrors and processed separately at different parts of the circuit [2]. As shown in Fig. 2(a), the positive part of the current, duplicated by a current mirror MN0 and MN2 is fed into a resistor  $R_T$  and a capacitor  $C_T$  by current mirror MP3 and MP4 with couple of MP1 respectively. On the other hand, MP0 and MP2 acts as the negative part of current mirror that flows out from resistor  $R_T$  and capacitor  $C_T$  by current mirror MN3 and MN4 with MN1 couple transistor, respectively. The capacitor  $C_T$  in our emulator



**Fig. 2** Architecture of proposed meminductor (a) Proposed meminductor emulator circuit, (b) Symbol of the meminductor.

stored programmed information in the form of charge. The buffer U1 avoids the discharging during the period when an input signal does not exist.

The voltage across capacitor  $C_T$  is the integration of mirrored current  $i_{in}$ , and the voltage across  $R_T$  is proportional to the mirrored current  $i_{in}$ . Let  $v_C$  and  $v_R$  be the voltage across  $C_T$  and  $R_T$ , respectively. Then,

$$v_C = \frac{1}{C_T} \int i_{in}(t) dt = \frac{q(t)}{C_T} \quad (5)$$

$$v_R = i_{in}(t) R_T \quad (6)$$

where  $q(t) = \int i_{in}(t) dt$  is the charge across capacitor  $C_T$ .

A four-quadrant analog multiplier AD633 performs analog multiplication between voltages  $v_C$  and  $v_R$  respectively [9]. It includes high impedance, differential X and Y inputs, and high impedance summing input (W). The output and input relation of this multiplier is given by,

$$Z = \frac{(X_+ - X_-)(Y_+ - Y_-)}{10} + W \quad (7)$$

From Fig. 2(a), the output voltage  $v_{mul}$  of a voltage multiplier AD633 is given by:

$$v_{mul} = \frac{R_T}{10C_T} q(t) i_{in}(t) \quad (8)$$

The output voltage  $v_{mul}$  is fed to a differentiator composed of  $C_D$ ,  $R_D$ , and OPAMP U3. The output voltage  $v_+$  of the differentiator circuit can be expressed as:

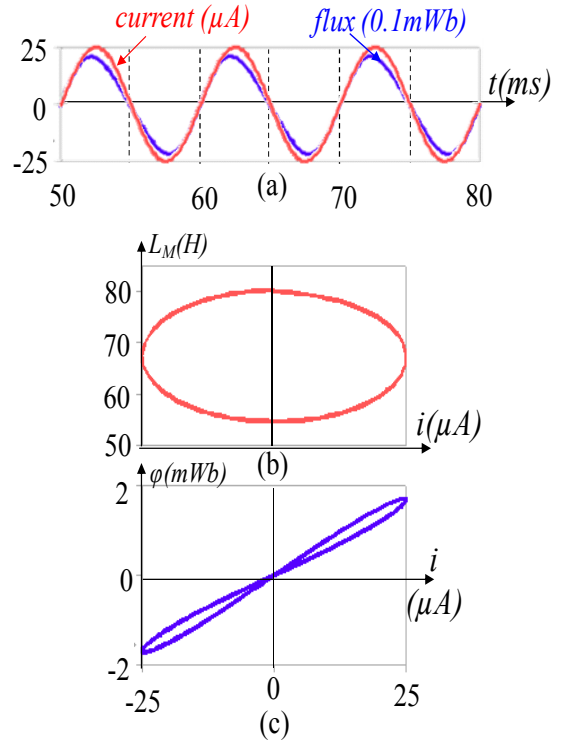
$$v_+ = -\frac{R_T R_D C_D}{10C_T} \frac{d}{dt} [q(t) i_{in}(t)] \quad (9)$$

From (4) and (8), we get:

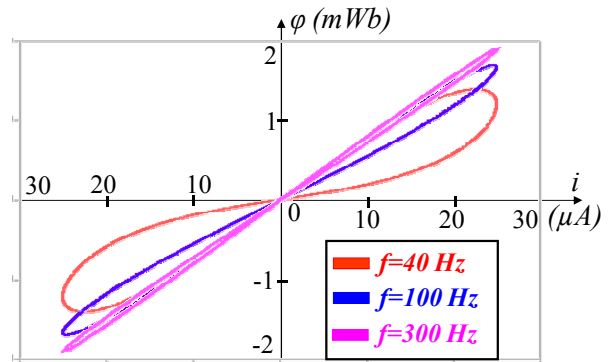
$$\varphi(t) = \left( L_s - \frac{R_T R_D C_D}{10C_T} q(t) \right) i_{in}(t) \quad (10)$$

Eq. (10) describes the operation of the meminductor circuit, in which the meminductance of the meminductor is:

$$L_M(q) = L_s - \alpha q(t) \quad (11)$$



**Fig. 3** Various waveforms measured across our meminductor emulator (a) Input current, flux with respect to time  $t$ , (b) Meminductance ( $L_M$ ) vs. current ( $i$ ), (c) Pinched hysteresis loop on  $\varphi$  vs.  $i$  plane.



**Fig. 4.** Pinched hysteresis loops obtained with the proposed meminductor emulator for various frequencies.

$$\text{where } \alpha = \frac{R_T R_D C_D}{10C_T}.$$

### III. SIMULATION RESULTS

PSPICE simulation was performed to verify the performance of the presented meminductor emulator. The parameters used for the simulations are  $\pm 5$  V power supply,  $C_T=0.1 \mu F$ ,  $R_T=4 K\Omega$ ,  $L_s=80 H$ ,  $C_D=0.8 \mu F$ , and

$R_D = 100\text{ K}\Omega$ .

One of the characteristics of a meminductor is a zero crossing pinched hysteresis loop under the  $\varphi$  versus  $i$  plane for any bipolar periodic signal. This feature was verified in the proposed meminductor emulator for a sinusoidal input current signal with a frequency of 100 Hz and amplitude of 25  $\mu\text{A}$ . The input current signal and the corresponding waveforms of the flux measured across our meminductor emulator are shown in the Fig. 3(a). Figs. 3(b) and (c) are the corresponding variation of meminductance with respect to the applied input current ( $i$ ) and the pinched hysteresis loop on the  $\varphi$  versus  $i$  plane, respectively. Observe that the loci on the  $\varphi$  versus  $i$  plane for the input signal exhibits zero crossing pinched hysteresis loop as expected.

Another characteristic of meminductors is the frequency dependency of the pinched hysteresis loop. The shape of the pinched hysteresis loop decreases as the frequency of the input signal increases. In our emulator circuit, the variation of flux ( $\varphi$ ) and meminductance ( $L_M$ ) depend on the charge ( $q$ ) stored in the capacitor. If the frequency of the input signal is low, then the rate of change of  $q$  across capacitor is wide and vice versa. Therefore, the flux  $\varphi$  defined in (10) will be wider for low frequency and narrow for high frequency signal. In order to verify the pinched hysteresis fingerprint of a meminductor circuit, we carried out the simulation of the proposed circuit at 40 Hz, 100 Hz, and 300 Hz for a sinusoidal current signal with amplitude of 25  $\mu\text{A}$ . Observe that, all of the  $\varphi$  versus  $i$  curves have a zero-crossing, and the shapes of the pinched hysteresis loops are shrunken as the frequency increases. All the pinched hysteresis loops of the proposed meminductor emulator satisfy the required fingerprints of a device to be meminductor.

#### IV. CONCLUSION

We presented a dedicated meminductor emulator without employing any memristive devices. The PSPICE simulations of the proposed architecture confirmed that our emulator satisfies all the criteria for a meminductor circuit. Since solid-state meminductor circuits are not expected to appear in the near future, our proposed meminductor emulator could be an inexpensive and simple solution to develop meminductor application circuits.

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