

Effects of V-Skew on the Torque Characteristic in Permanent Magnet Synchronous Motor

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Abstract – In this paper, we proposed how the V-skew applied on a magnet of the rotor to improve the characteristics of cogging torque in large PMSM. Large PMSM is difficult to apply a pitch of the diagonal magnetic skew because of the motor's structure and making. In addition, the force in the direction of z-axis occurs when the diagonal skew is applied. So we are applying the optimal v-skew to reduce torque ripple and cogging torque because this reduces the noise and vibration on the motor. Through FEM 3D analysis, we studied to find the optimal v-skew angle for reducing torque ripple.

Keywords: V-Skew, PMSM, Force

1. Introduction

MW-class permanent magnet synchronous motor is designed on the special purpose. This structure of a large permanent magnet synchronous motor has a lot of slots and poles, and the characteristics of a noise and vibration are considered to depend on the driving environment and the purpose. But, the PM motor is needed to reduce a cogging torque because it is the cause of Noise and vibration. In general, skewing the magnetic or slot-teeth is used to reduce torque ripple, vibration and improving noise. However, vibration and noise characteristic is worse because the Lorentz force is caused by the stator current and the rotor magnet when a large permanent magnet synchronous motor is used a diagonal skew. So we apply the V-skew to reduce the z-axial force instead of the diagonal skew. Also the optimal skew angle can be found by reduction ratio of cogging torque according to the skew angle when V-skew is applied [1-3].

In this paper, we was verified by FEM 3D to find the optimal v-skew angle to minimize the cogging torque for the 16 pole 24slot motor.

2. Model Analysis

2.1 PMSM Reference Machines

In order to compare the impact of No-Skew, diagonal skew and V-Skew of permanent magnet on the rotor, PM

motors were designed in 3D as shown in Fig. 1. The skew angle of applied the permanent magnet is defined as shown in the Fig. 1.

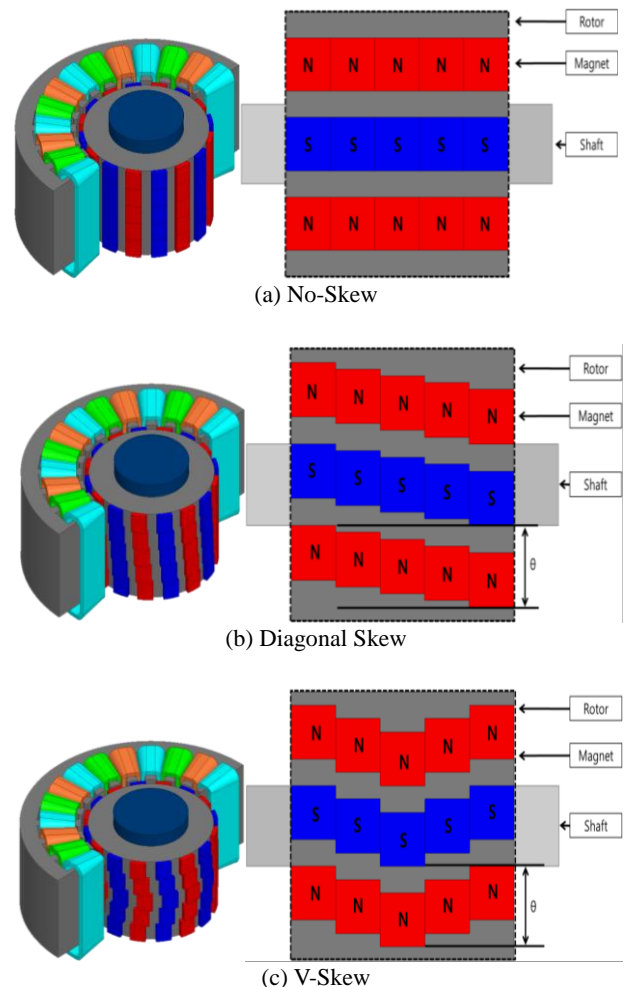


Fig. 1. 3D Modeling and schematic of skew diagram

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2.2 Comparing the Overlapping Area of the Slot and Magnet

Cogging torque is generated when reluctance of between the permanent magnet and the stator slot is different. Therefore, the overlapping area of the slot and magnet is related to cogging torque. So, Fig. 2 can be expressed to calculate the overlapping area of slot and the magnet when we are applying the general model and the skew model to predict the cogging torque.

Fig. 3 appears a ratio of the area of between a one slot and the magnet. This graph shows that if the V-skew is applied, the shape of the air gap flux is similar to the sin function and the loss of flux is less than to apply the diagonal skew.

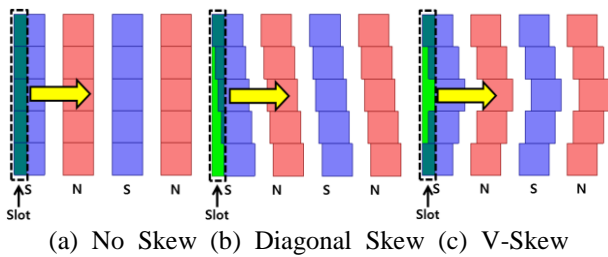


Fig. 2. Schematic view of Slot and Magnet Diagram

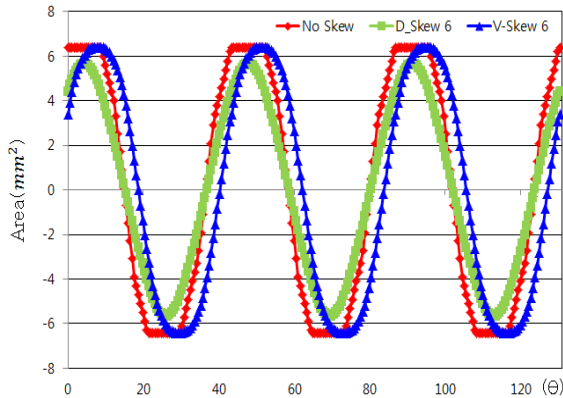


Fig. 3. Magnet area of one slot versus skew

2.3 Characteristic Analysis

Cogging torque is that the magnetic energy of the motor moves to the minimum position, so it is caused by the interaction of the stator slot and rotor magnet regardless of the load current. The frequency component and the shape of cogging torque can be varied by adjusting the number of slots and the magnet.

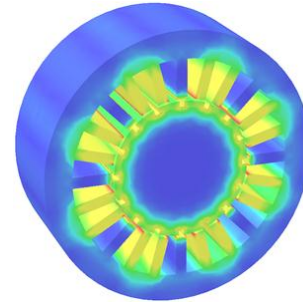
In general, equation (1) is expressed as cogging torque.

$$T_{Cogging Torque} = -\frac{\partial W_{me}(\Phi, x)}{\partial x} = -\frac{1}{2} \Phi^2 \frac{\partial R_g}{\partial x} [Nm] \quad (1)$$

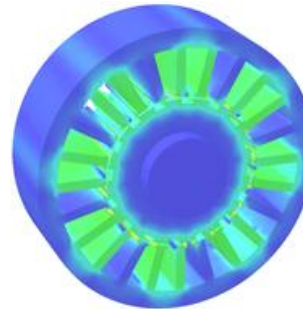
W_{me} = co-energy, we can see that the cogging torque is proportional to the change in flux linkage.

2.4 FEM 3D analysis

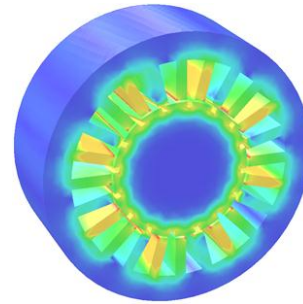
In order to get a magnetic flux density, cogging torque and torque ripple by skew, 3D FEM analysis was conducted. And the FFT analysis and the Z-axis force are obtained through the result of the 3D FEM analysis.



(a) No Skew



(b) Diagonal skew (θ=6)



(c) V-Skew (θ=6)



Fig. 4. Magnetic flux density

Fig. 4 shows that magnetic flux density in the slots is changed by the skew of the magnet. Also magnetic flux in the slot can be seen evenly distributed. Fig. 5 (a) and (b) show that overlapping area of the slots and magnets is changed in the form, such as V-Skew by skew angle. Considering these changes, the overlapping area of the slots and magnets does not shrink when skew angle is increased because the form of distribution of air gap flux density is a V shape. In addition, the V-skew angle should not continue to grow because the overhang is caused by a large V-skew angle at the end of the motor.

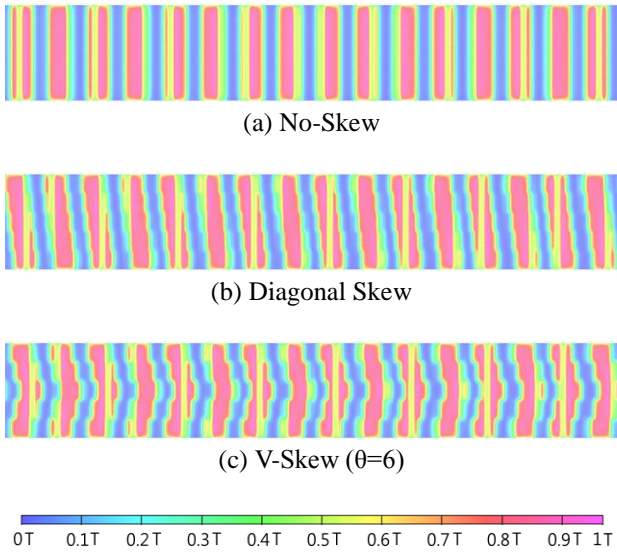


Fig. 5. Air Gap magnetic flux density

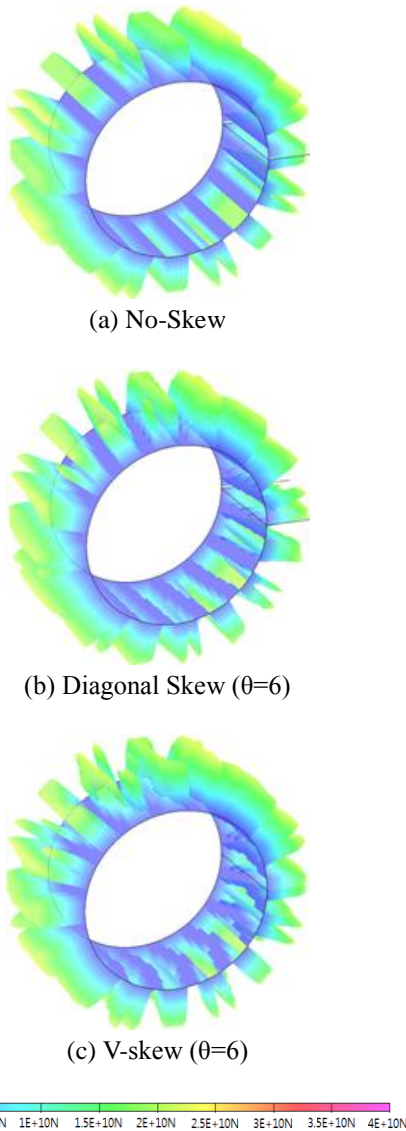


Fig. 6. Air gap force Distribution

Fig. 6 shows the distribution of the force for the No-Skew, diagonal skew and V-Skew the air gap. We can see the distribution of force in the air gap to change by the skew. So the result is predicted that changes in the value of the area of the graph can be used to predict the results.

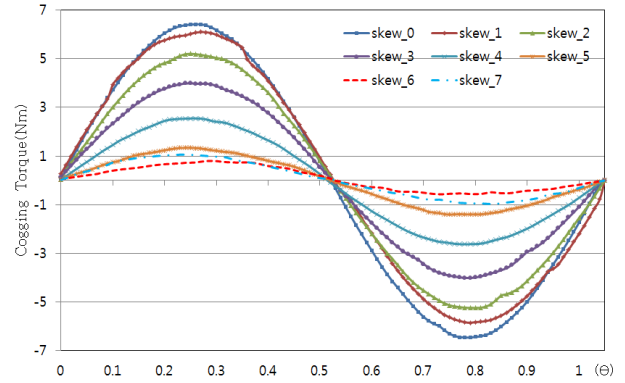


Fig. 7. Cogging torque versus V-Skew angle

Table1. Peak value of cogging torque versus V-Skew angle

Angle(θ)	0°	1°	2°	3°	4°	5°	6°	7°
Cogging Torque Peak Value(Nm)	6.41	6.09	5.2	3.99	2.54	1.34	0.8	1.0

The cogging torque by according to change in V-skew angle is shown in Fig. 7. The Fig.7 is shown that the cogging torque is the minimum when the V-Skew angle is 6.

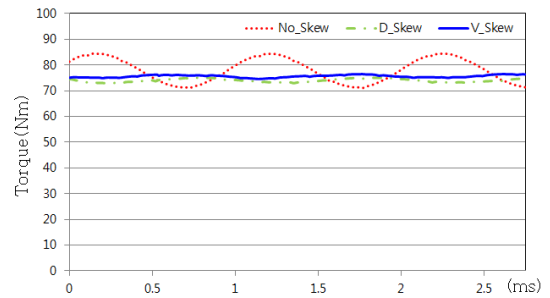


Fig. 8. Torque versus Skew angle

3. Conclusion

In this paper, we study to find the optimal v-skew by comparing the change of the cogging torque. Fig. 7, 8 shows that the v-skew angle is 6 degree is the minimum cogging torque and torque ripple. Namely, the optimal V-Skew is applied instead of one pitch of V-skew or diagonal skew. Through this, we are considering the optimal v-skew angle when we apply v-skew to a large permanent magnet motor. In the future, we research about the various impacts by v-skew on the motor.

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