

# Advanced Circuit-Level Model of Magnetic Tunnel Junction-based Spin-Torque Oscillator with Perpendicular Anisotropy Field

Miryeon Kim, Hyein Lim, Sora Ahn, Seungjun Lee, and Hyungsoon Shin

**Abstract**—Interest in spin-torque oscillators (STOs) has been increasing due to their potential use in communication devices. In particular the magnetic tunnel junction-based STO (MTJ-STO) with high perpendicular anisotropy is gaining attention since it can generate high output power. In this paper, a circuit-level model for an in-plane magnetized MTJ-STO with partial perpendicular anisotropy is proposed. The model includes the perpendicular torque and the shift field for more accurate modeling. The bias voltage dependence of perpendicular torque is represented as quadratic. The model is written in Verilog-A, and simulated using HSPICE simulator with a current-mirror circuit and a multi-stage wideband amplifier. The simulation results show the proposed model can accurately replicate the experimental data such that the power increases and the frequency decreases as the value of the perpendicular anisotropy gets close to the value of the demagnetizing field.

**Index Terms**—Spin-torque oscillator, magnetic tunnel junction, perpendicular anisotropy, perpendicular torque, circuit-level model

## I. INTRODUCTION

A nanoscale STO is suitable for high density integration and it can generate oscillations in several gigahertz ranges. For these reasons, interest in STOs has been increasing. However, their low output power has been a bottleneck for practical use. MTJ-STOs are preferred to giant magneto-resistance (GMR) STOs because they can generate higher power due to their large magneto-resistance (MR) ratio [1]. Also, the bias current to threshold current ratio ( $I/I_{th}$ ) is another important factor to obtain large power. The threshold current is proportional to the saturation magnetization ( $M_S$ ).  $M_S$  can be decreased by increasing perpendicular anisotropy ( $M_P$ ) because  $M_P$  compensates the demagnetizing field ( $H_d = 4\pi M_d$ ). Thus, the MTJ-STOs with strong perpendicular anisotropy is gaining high attention for their potential to provide enough power for practical use [2].

In this paper, a circuit-level model of an MTJ-STO with the partial perpendicular anisotropy is proposed. In the proposed model three major characteristics of an MTJ-STO which are generation frequency, power, and linewidth are represented as functions of bias current and applied magnetic field. The model considers the perpendicular torque and the shift field for more accurate calculation of effective field inside the free layer. The MTJ-STO model is written in Verilog-A which is a hardware-description language (HDL) providing full compatibility with circuit-simulators such as SPICE.

Section II presents the analytic model of MTJ-STOs with perpendicular anisotropy. Sections III and IV discuss the simulation results with the HSPICE and the

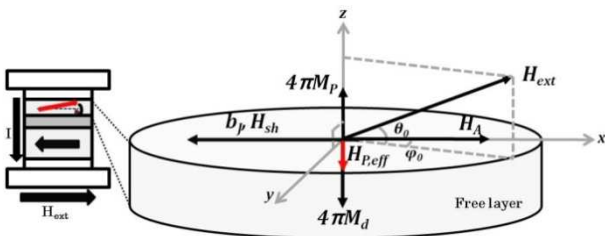
conclusion.

## II. ANALYTIC MODEL OF MTJ-STO

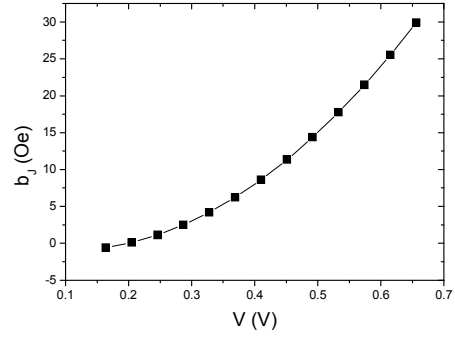
The three characteristics of MTJ-STOs - generation frequency ( $\omega_g$ ), mean oscillation power ( $P_{exp}$ ) and generation linewidth ( $2\Delta\omega$ ), are varied by the bias current and the magnitude and the direction of external magnetic field ( $H_{ext}$ ). As the three characteristics are directly related to the internal field of the free layer, it is important to calculate the effective field in the free layer accurately. The internal and external magnetic fields that exist in the free layer are shown in Fig. 1. Here the easy-axis and the hard-axis are represented by  $x$  and  $y$  axes, respectively. The  $z$  axis is orthogonal to the  $x-y$  plane. In-plane angle  $\varphi_0$  is the angle between  $H_{ext}$  and  $x$  axis. Out-of-plane angle  $\theta_0$  is the angle with respect to the  $x-y$  plane. Shape anisotropy field  $H_A$ , the perpendicular torque  $b_J$  and the shift field  $H_{sh}$  exist in  $x$  axis. In GMR-STOs the magnitude of  $b_J$  is very small, so it is usually ignored in the GMR-STO model. On the other hand,  $b_J$  must be included in the MTJ-STO model because the magnitude of  $b_J$  in MTJ-STOs can be as large as 30% of the in-plane torque ( $a_J$ ) [3]. In previous works, there are a couple of theories on the bias dependence of the  $b_J$  [3-5]. In this paper, the bias voltage dependence of  $b_J$  is represented as quadratic [6].

$$b_J = C_1 V + C_2 V^2 \quad (1)$$

Here,  $C_1 = -20 \text{OeV}^{-1}$  and  $C_2 = 100 \text{OeV}^{-2}$  have been chosen by comparing calculated data with experimental data [2]. Fig. 2 shows the  $b_J$  as a function of bias voltage. For more accurate modeling,  $H_{sh}$  should be included in the MTJ-STO model which is composed of dipolar coupling, orange-peel coupling, and inter-layer exchange coupling.



**Fig. 1.** The internal and external magnetic fields of the free layer.



**Fig. 2.** The perpendicular torque as a function of bias voltage.

For STOs with  $M_P$ , it is observed that  $H_d$  is compensated by  $M_P$ . To consider this effect, the effective perpendicular magnetic field ( $H_{P,eff}$ ) is defined as  $H_{P,eff} = 4\pi M_S = 4\pi(M_d - M_P)$  as shown in Fig. 1.

The magnitude  $H$ , the in-plane angle  $\varphi$ , and the out-of plane angle  $\theta$  of the effective magnetic field in the free layer is obtained from (2) [7].

$$H \sin \theta = H_{ext} \sin \theta_0 - H_{P,eff} \sin \theta \quad (2a)$$

$$H \cos \theta \cos \varphi = H_{ext} \cos \theta_0 \cos \varphi_0 + H_A \cos \theta \cos \varphi - H_{sh} - b_J \quad (2b)$$

$$H \cos \theta \sin \varphi = H_{ext} \cos \theta_0 \sin \varphi_0 \quad (2c)$$

Characteristic frequencies and some other coefficients of an MTJ-STO required to calculate  $\omega_g$ ,  $2\Delta\omega$ , and  $P_{exp}$  are determined from  $H$ ,  $\varphi$  and  $\theta$ . The more detailed explanation of these parameters can be found in [7].

The three characteristics  $\omega_g$ ,  $2\Delta\omega$ , and  $P_{exp}$  of MTJ-STOs are determined by (3).

$$\omega_g = \omega_0 + N\bar{p} \quad (3a)$$

$$2\Delta\omega = (1 + v^2)\Gamma_+(p_0) \frac{k_B T}{E(\bar{p})} \quad (3b)$$

$$P_{exp} = R_{rf} I^2 \psi^2 \quad (3c)$$

In (3),  $\omega_0$  and  $N$  are ferromagnetic resonance frequency and the coefficient of nonlinear frequency shift, respectively. Also,  $\bar{p}$  is dimensionless power and represented as  $\frac{Q\eta}{Q+\zeta} \times \left[ 1 + \frac{\exp(-(\zeta+Q)/Q^2\eta)}{E_\beta((\zeta+Q)/Q^2\eta)} \right] + \frac{\zeta-1}{\zeta+Q}$ . Here,

$Q$  is a nonlinear damping coefficient,  $\eta$  is effective noise power and  $\zeta$  is a dimensionless supercriticality parameter defined as  $I/I_{th}$ .  $E_\beta(x) = \int_1^\infty e^{-xt}/t^\beta dt$  is exponential integral function where  $\beta = -(1+Q)\zeta/Q^2\eta$ .  $\nu$  is normalized dimension-less nonlinear frequency shift,  $\Gamma_+(\rho_0)$  is positive damping rate,  $k_B$  is Boltzmann constant, and  $T$  is temperature in Kelvin.  $E(\bar{p})$  is oscillator energy and defined as  $\lambda\omega_0\bar{p}$  where  $\lambda = V_{eff}H_{P,eff}/\gamma$  and  $V_{eff}$  is the effective volume of the free layer and  $\gamma$  is gyromagnetic ratio.  $R_{rf}$  and  $\psi^2$  are magneto-resistance and the precession angle, respectively, and obtained from (4).

$$R_{rf} = \frac{R_L}{2[R(\theta_0) + R_L]^2} \times \left(\frac{dR}{d\theta}\right)^2 \quad (4a)$$

$$\psi^2 = \arccos^2(1 - 2(1 + \varepsilon^*)\bar{p}) \approx 4(1 + \varepsilon^*)\bar{p} \quad (4b)$$

In these equations,  $R_L$  is the load resistance.  $\varepsilon^*$  is ellipticity of precession, and it approaches to 0 as the magnetization of free layer becomes orthogonal to the free layer. In previous works,  $\varepsilon^*$  is limited to in-plane magnetization [8]. In our proposed model,  $\varepsilon^*$  is realized for both in-plane and out-of-plane magnetizations, and it is represented as (5).

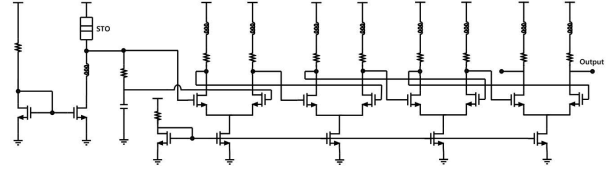
$$\varepsilon^* = \frac{H_{P,eff} \cos \theta}{(2H_{ext} + H_{P,eff})} \quad (5)$$

Threshold current  $I_{th}$  required for  $\zeta$  is defined as (6).

$$I_{th} = \frac{\Gamma_G}{\sigma} \quad (6a)$$

$$\sigma = \mu_0\sigma_0 = \frac{\mu_0\mathcal{E}\mu_B}{2e(M_d - M_p)LS} \quad (6b)$$

Here,  $\Gamma_G$  is linear damping rate,  $\mu_0$  is permeability,  $\mathcal{E}$  is dimensionless spin-polarization efficiency,  $\mathcal{S}$  is spectroscopic Lande factor,  $\mu_B$  is Bohr magneton,  $e$  is the modulus of electron charge,  $L$  is the thickness of the free layer, and  $S$  is the area of the free layer. It is worth noting that  $I_{th}$  decreases as the value of  $M_p$  in the free layer increases.



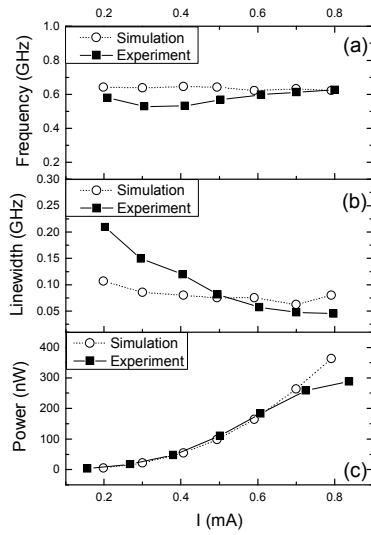
**Fig. 3.** Circuit schematic of an MTJ-STO with the current-mirror circuit and the 4-stage common source amplifier.

### III. SIMULATION RESULTS

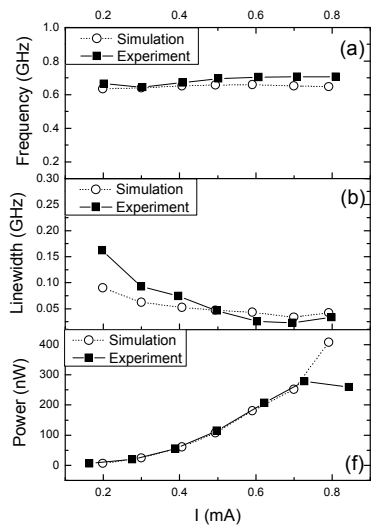
#### 1. Characteristics of MTJ-STOs with Bias Current

The proposed MTJ-STO model is written in Verilog-A HDL which provides full compatibility with circuit simulators such as SPICE. In order to verify its accuracy, the model is simulated using HSPICE simulator with a current-mirror circuit and a multi-stage wideband amplifier. The schematic of the circuit is shown in Fig. 3. The dimension of MTJ-STO under simulation is  $170\text{ nm} \times 60\text{ nm}$ , thickness of free layer is  $1.7\text{ nm}$ , and  $H_A$  is  $60\text{ Oe}$ . The MR ratio of MTJ-STO is 102% [2]. The bandwidth of the amplifier in Fig. 3 is about 8 GHz and the power gain is 40 dB.

In Figs. 4 and 5, the simulation results of the three characteristics of the MTJ-STO with the perpendicular anisotropy are compared with the experimental data in [2] for different direction and magnitude of the external magnetic field. The calculated  $I_{th}$  from (6) is 0.08 mA which is the same value of  $I_{th}$  in [2]. Also,  $M_p = 1.1875\text{ kemu/cm}^3$  has been chosen by comparing the simulation data with the experimental data which is similar to  $M_d = 1.2\text{ kemu/cm}^3$  [2]. Although the MTJ-STO has strong perpendicular anisotropy field, it remains in-plane magnetized. As can be seen, the simulation results are in good agreement with the experimental data for both in-plane and out-of-plane fields. In Figs. 4(b) and 5(b), the simulation results of generation linewidth and the experimental data have little discrepancy as  $I$  gets close to  $I_{th}$ . In this region, STOs operate at thermally excited ferromagnetic resonance (T-FMR) mode [1]. Currently, the proposed model focuses on steady-state oscillation and does not include T-FMR mode because that region is out of normal operating condition in real application.



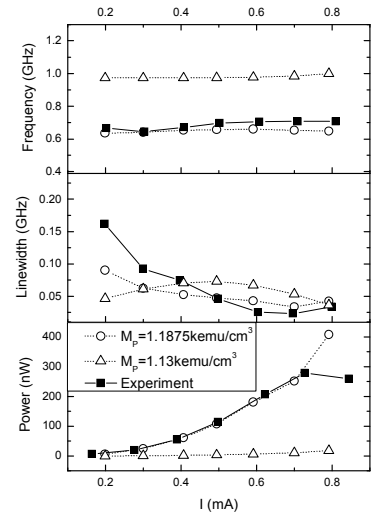
**Fig. 4.** Characteristics of the MTJ-STO as a function of bias current for in-plane field ( $H_{ext} = 220Oe$ ,  $\theta_0 = 0^\circ$  and  $\varphi_0 = -60^\circ$ ).



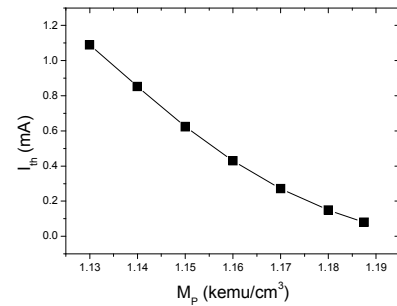
**Fig. 5.** Characteristics of MTJ-STOs as a function of bias current for out-of-plane field ( $H_{ext} = 264Oe$ ,  $\theta_0 = 40.4^\circ$  and  $\varphi_0 = -60^\circ$ ).

**2. Characteristics of MTJ-STOs with Perpendicular Anisotropy**

Fig. 6 shows the three characteristics of an MTJ-STO as a function of bias current for the out-of-plane field with  $M_p = 1.1857 \text{ kemu/cm}^3$  and  $1.13 \text{ kemu/cm}^3$ . The relation between  $I_{th}$  and  $M_p$  is shown in Fig. 7. As shown in Fig. 7, the value of  $I_{th}$  tends to decrease with increasing of  $M_p$ . For example,  $I_{th}$  are 0.08 mA and



**Fig. 6.** Characteristics of MTJ-STOs as a function of bias current for different  $M_p$  with  $H_{ext} = 264Oe$ ,  $\theta_0 = 40.4^\circ$  and  $\varphi_0 = -60^\circ$ .

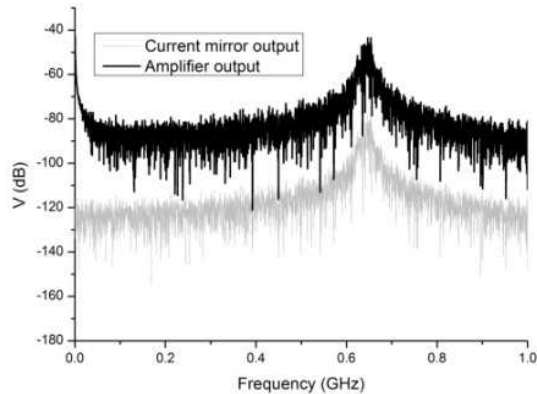


**Fig. 7.** Threshold current as a function of perpendicular anisotropy.

1.09 mA at  $M_p = 1.1857 \text{ kemu/cm}^3$  and  $1.13 \text{ kemu/cm}^3$ , respectively.  $P_{exp}$  of the MTJ-STO is proportional to  $\zeta$ . Therefore, as shown in Fig. 6, difference of  $P_{exp}$  between two MTJ-STOs is about  $0.24 \mu W$  at the same value of  $I = 0.7 \text{ mA}$ . In addition,  $\omega_g$  of the MTJ-STO with strong  $M_p$  is lower than that with weaker  $M_p$  by approximately 0.4 GHz. That is because  $M_p$  compensates  $H_d$ .

**3. Results of Circuit-level Simulation**

Fig. 8 shows the simulation results with HSPICE on a circuit shown in Fig. 3. Frequency spectrum of the output signals with out-of-plane field from the current-mirror stage and the 4-stage wideband amplifier are shown. A single frequency peak is shown at 0.65 GHz as expected in Fig. 5. The output signal of the amplifier has about 36



**Fig. 8.** The frequency spectrum of the output signal from the current-mirror stage and the amplifier stage.

dB power gain over the current mirror output.

#### IV. CONCLUSIONS

A circuit-level model of an in-plane magnetized MTJ-STO with partial perpendicular anisotropy has been proposed. The MTJ-STO with the perpendicular anisotropy has low threshold current because the effect of the demagnetizing field is decreased. Thus, the MTJ-STO with stronger perpendicular anisotropy produces larger power at the same level of bias current. The simulation results show the proposed model can accurately replicate the experimental data such that the power increases and the frequency decreases as the value of the perpendicular anisotropy gets close to the value of the demagnetizing field. Simulation results also confirmed that the proposed MTJ-STO model is fully compatible with arbitrary CMOS circuits.

#### ACKNOWLEDGMENTS

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