

# Linear Prediction Approach for Accurate Dual-Channel Sine-Wave Parameter Estimation in White Gaussian Noise

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*The problem of sinusoidal parameter estimation at two channels with common frequency in white Gaussian noise is addressed. By making use of the linear prediction property, an iterative linear least squares (LLS) algorithm for accurate frequency estimation is devised. The remaining parameters are then determined according to the LLS fit with the use of the frequency estimate. It is proven that the variance of the frequency estimate achieves Cramér-Rao lower bound at sufficiently small noise conditions.*

*Keywords:* Sinusoidal parameter estimation, linear prediction, least squares, dual-channel.

## I. Introduction

In this letter, we address the problem of finding the sinusoidal parameters from noisy observations received at two channel outputs. This has applications such as velocity and size estimation in phase Doppler anemometry and impedance measurement [1]. In each channel, the noise-free signal is a real sinusoid with a DC offset. As the frequency is common, there are seven unknowns of interest, namely, one frequency as well as two amplitudes, phases, and DC offsets. In [2], [3], the nonlinear least squares (NLS) estimator is proposed, which first finds the frequency through a one-dimensional (1D) search, followed by a linear least squares (LLS) fit of the remaining parameters. Although its mean square error (MSE) performance can attain Cramér-Rao lower bound (CRLB) [2] in the presence of white Gaussian noise, there is no guarantee

of obtaining the global solution. It is because the 1D search in the multi-modal surface is typically performed in two steps. First, we evaluate the NLS objective function at a number of grid points, and the coarse frequency estimate is given by the grid point corresponding to the lowest function value. A local search based on a numerical method with the coarse estimate being the initial guess is then employed in the second step. When the number of grid points is not sufficiently large, it is possible that the coarse estimate corresponds to a local minimum, which results in a large frequency estimation error.

In this work, the linear prediction (LP) approach is utilized to develop an iterative LLS algorithm for frequency estimation using dual-channel data so that no 1D search is required. The remaining parameters are then solved straightforwardly according to an LLS procedure. It is worth pointing out that we have recently utilized this methodology in parameter estimation for wave equation [4]. Nevertheless, the LP relation in this work is different from that of [4], and we have also extended the idea to multiple channels. Moreover, it is proven that the variance of the frequency estimate attains the CRLB at sufficiently high signal-to-noise ratio (SNR) conditions.

## II. Proposed Method

The dual-channel sinusoidal signal model is

$$x_i(n) = s_i(n) + v_i(n), \quad i = 1, 2, \quad (1)$$

where

$$s_i(n) = \alpha_i \cos(\omega n + \phi_i) + C_i, \quad n = 1, \dots, N. \quad (2)$$

Denoting the amplitude, initial phase, and DC offset at the  $i$ -th

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channel are  $\alpha_i > 0$ ,  $\phi_i \in [0, 2\pi)$ , and  $C_i$ , respectively, while  $\omega \in [0, \pi)$  is the common frequency, and they are the unknown parameters to be estimated. For simplicity but without loss of generality, we assume that the additive noises  $v_1(n)$  and  $v_2(n)$  are uncorrelated white Gaussian processes with variances  $\sigma_1^2$  and  $\sigma_2^2$ , respectively. Here, we assume their ratio, denoted by  $r = \sigma_1^2 / \sigma_2^2$ , is known a priori.

According to [5],  $s_i(n)$  satisfies the following LP property:

$$s_i(n) - s_i(n-3) - \rho(s_i(n-1) - s_i(n-2)) = 0 \quad (3)$$

for  $n = 4, 5, \dots, N$ , where  $\rho = (2 \cos(\omega) + 1)$  is called the LP coefficient, which is linear in (3). Using (3), an LP error vector for the  $i$ -th channel, denoted by  $\mathbf{e}_i$ , is established as

$$\mathbf{e}_i = \mathbf{x}_{4i} - \mathbf{x}_{1i} - \tilde{\rho}(\mathbf{x}_{3i} - \mathbf{x}_{2i}), \quad i = 1, 2, \quad (4)$$

where  $\mathbf{x}_{mi} = [x_i(m) \ x_i(m+1) \ \dots \ x_i(m+N-4)]^T$ ,  $m = 1, 2, 3, 4$ , and  $\tilde{\rho}$  is the variable for  $\rho$ . Stacking the error vectors as  $\mathbf{e} = [\mathbf{e}_1^T \ \mathbf{e}_2^T]^T$ , the LLS estimate of  $\rho$ , denoted by  $\hat{\rho}$ , is

$$\hat{\rho} = \arg \min_{\tilde{\rho}} \mathbf{e}^T \mathbf{W} \mathbf{e} = \frac{\mathbf{z}_2^T \mathbf{W} \mathbf{z}_1}{\mathbf{z}_2^T \mathbf{W} \mathbf{z}_2}, \quad (5)$$

where  $\mathbf{z}_1 = [\mathbf{x}_{41}^T - \mathbf{x}_{11}^T \ \mathbf{x}_{42}^T - \mathbf{x}_{12}^T]^T$ ,  $\mathbf{z}_2 = [\mathbf{x}_{31}^T - \mathbf{x}_{21}^T \ \mathbf{x}_{32}^T - \mathbf{x}_{22}^T]^T$ , and  $\mathbf{W}$  is the weighting matrix and its optimal form is determined as [6]

$$\mathbf{W} = [E\{\mathbf{e}\mathbf{e}^T\} |_{\tilde{\rho}=\rho}]^{-1} = \text{blkdiag}(\mathbf{W}_{S1}, \mathbf{W}_{S2}), \quad (6)$$

where

$$\begin{aligned} \mathbf{W}_{S1}^{-1} &= E\{\mathbf{e}_1 \mathbf{e}_1^T\} |_{\tilde{\rho}=\rho} \\ &= \text{Toeplitz}([2(\rho^2 + 1) \quad -\rho^2 - 2\rho \quad 2\rho \quad -1 \quad 0 \quad \dots \quad 0]) \sigma_1^2 \end{aligned} \quad (7)$$

for  $i=1, 2$ . The  $E$  represents the expectation operator,  $\text{blkdiag}(\cdot)$  denotes the block diagonal matrix, and  $\text{Toeplitz}(\mathbf{u}^T)$  stands for the Toeplitz matrix with  $\mathbf{u}$  and  $\mathbf{u}^T$  being the first column and first row, respectively. As a result,  $\hat{\rho}$  is also expressed as

$$\begin{aligned} \hat{\rho} &= \frac{(\mathbf{x}_{31} - \mathbf{x}_{21})^T \mathbf{W}_{S1} (\mathbf{x}_{41} - \mathbf{x}_{11}) + (\mathbf{x}_{32} - \mathbf{x}_{22})^T \mathbf{W}_{S2} (\mathbf{x}_{42} - \mathbf{x}_{12})}{(\mathbf{x}_{31} - \mathbf{x}_{21})^T \mathbf{W}_{S1} (\mathbf{x}_{31} - \mathbf{x}_{21}) + (\mathbf{x}_{32} - \mathbf{x}_{22})^T \mathbf{W}_{S2} (\mathbf{x}_{32} - \mathbf{x}_{22})} \\ &= \frac{(\mathbf{x}_{31} - \mathbf{x}_{21})^T \mathbf{W}_S (\mathbf{x}_{41} - \mathbf{x}_{11}) + r(\mathbf{x}_{32} - \mathbf{x}_{22})^T \mathbf{W}_S (\mathbf{x}_{42} - \mathbf{x}_{12})}{(\mathbf{x}_{31} - \mathbf{x}_{21})^T \mathbf{W}_S (\mathbf{x}_{31} - \mathbf{x}_{21}) + r(\mathbf{x}_{32} - \mathbf{x}_{22})^T \mathbf{W}_S (\mathbf{x}_{32} - \mathbf{x}_{22})}, \end{aligned} \quad (8)$$

where

$$\mathbf{W}_S^{-1} = \text{Toeplitz}([2(\rho^2 + 1) \quad -\rho^2 - 2\rho \quad 2\rho \quad -1 \quad 0 \quad \dots \quad 0]). \quad (9)$$

As  $\mathbf{W}_S$  is a function of the unknown  $\rho$ , the following iterative LLS procedure is employed to determine the frequency:

**Step 1.** Set  $\mathbf{W}_S = \mathbf{I}_{N-3}$ , which is the  $(N-3)$  by  $(N-3)$

identity matrix.

**Step 2.** Compute  $\hat{\rho}$  using (8).

**Step 3.** Use  $\rho = \hat{\rho}$  to construct  $\mathbf{W}_S$  of (9).

**Step 4.** Repeat Steps 2 and 3 until a stopping criterion is reached.

**Step 5.** Compute the frequency estimate  $\hat{\omega}$  as  $\hat{\omega} = \cos^{-1}((\hat{\rho} - 1) / 2)$ .

With the use of  $\hat{\omega}$ , the estimates of  $\alpha_i$ ,  $\phi_i$ , and  $C_i$ , denoted by  $\hat{\alpha}_i$ ,  $\hat{\phi}_i$ , and  $\hat{C}_i$ , respectively, are obtained by minimizing the following LLS cost function:

$$(\Xi \boldsymbol{\kappa} - \mathbf{x})^T (\Xi \boldsymbol{\kappa} - \mathbf{x}), \quad (10)$$

where

$$\Xi = \text{blkdiag}(\Xi_1, \Xi_2),$$

$$\boldsymbol{\kappa} = [\boldsymbol{\kappa}_1^T, \boldsymbol{\kappa}_2^T]^T,$$

$$\boldsymbol{\kappa}_1 = [\alpha_1 \cos(\phi_1) \ \alpha_1 \sin(\phi_1) \ C_1]^T, \quad \boldsymbol{\kappa}_2 = [\alpha_2 \cos(\phi_2) \ \alpha_2 \sin(\phi_2) \ C_2]^T,$$

$$\mathbf{x} = [\mathbf{x}_1^T, \mathbf{x}_2^T]^T,$$

$$\mathbf{x}_1 = [x_1(1) \ x_1(2) \ \dots \ x_1(N)]^T, \quad \mathbf{x}_2 = [x_2(1) \ x_2(2) \ \dots \ x_2(N)]^T,$$

$$\Xi_1 = \Xi_2 = \begin{bmatrix} \cos(\hat{\omega}) & \cos(2\hat{\omega}) & \dots & \cos(N\hat{\omega}) \\ -\sin(\hat{\omega}) & -\sin(2\hat{\omega}) & \dots & -\sin(N\hat{\omega}) \\ 1 & 1 & \dots & 1 \end{bmatrix}^T. \quad (11)$$

The LLS estimate of  $\boldsymbol{\kappa}$  is

$$\hat{\boldsymbol{\kappa}} = [\hat{\boldsymbol{\kappa}}_1^T, \hat{\boldsymbol{\kappa}}_2^T]^T = (\Xi^T \Xi)^{-1} \Xi^T \mathbf{x}, \quad (12)$$

which gives  $\hat{\alpha}_i = \sqrt{[\hat{\boldsymbol{\kappa}}_i]_1^2 + [\hat{\boldsymbol{\kappa}}_i]_2^2}$ ,  $\hat{\phi}_i = \tan^{-1}([\hat{\boldsymbol{\kappa}}_i]_2 / [\hat{\boldsymbol{\kappa}}_i]_1)$ , and  $\hat{C}_i = [\hat{\boldsymbol{\kappa}}_i]_3$ ,  $i = 1, 2$ . Here,  $[\hat{\boldsymbol{\kappa}}_i]_l$ ,  $l = 1, 2, 3$ , denotes the  $l$ -th element of  $\hat{\boldsymbol{\kappa}}_i$ .

If the value of each DC offset is zero, the LP relation of (3) will be simplified and the number of unknowns is reduced to 5. We can still apply the proposed methodology to perform accurate parameter estimation.

### III. Variance Analysis

We now produce the variance of  $\hat{\omega}$  based on small error conditions such that  $\hat{\rho}$  is sufficiently close to  $\rho$ . For simplicity but without loss of generality, the noise variances  $\sigma_1^2$  and  $\sigma_2^2$  are set equal to  $\sigma^2$ . Let  $\mathbf{z}_i = \bar{\mathbf{z}}_i + \Delta \mathbf{z}_i$ ,  $i = 1, 2$ , where  $\bar{\mathbf{z}}_i$  and  $\Delta \mathbf{z}_i$  are the noise-free version and perturbation of  $\mathbf{z}_i$ , respectively. Upon parameter convergence and applying Taylor series expansion, we obtain from (5)

$$f(\hat{\rho}) = \mathbf{z}_2^T \mathbf{W} (\mathbf{z}_1 - \hat{\rho} \mathbf{z}_2) = 0 \approx f(\rho) + f'(\rho) \Delta \rho, \quad (13)$$

where  $\Delta\rho = \hat{\rho} - \rho$ . Using  $\bar{\mathbf{z}}_1 = \bar{\mathbf{z}}_2\rho$  and neglecting second-order perturbation terms,  $f(\rho)$  can be rewritten as

$$(\bar{\mathbf{z}}_2 + \Delta\mathbf{z}_2)^T \mathbf{W}((\bar{\mathbf{z}}_1 + \Delta\mathbf{z}_1) - \rho(\bar{\mathbf{z}}_2 + \Delta\mathbf{z}_2)) \approx \bar{\mathbf{z}}_2^T \mathbf{W}(\Delta\mathbf{z}_1 - \Delta\mathbf{z}_2\rho). \quad (14)$$

As only first-order terms are retained,  $f'(\rho)\Delta\rho$  is approximated as

$$f'(\rho)\Delta\rho \approx -\bar{\mathbf{z}}_2^T \mathbf{W}\bar{\mathbf{z}}_2\Delta\rho. \quad (15)$$

Based on (13) through (15), we have

$$\Delta\rho \approx \frac{\bar{\mathbf{z}}_2^T \mathbf{W}(\Delta\mathbf{z}_1 - \Delta\mathbf{z}_2\rho)}{\bar{\mathbf{z}}_2^T \mathbf{W}\bar{\mathbf{z}}_2}. \quad (16)$$

The variance of  $\hat{\rho}$ , denoted by  $\text{var}(\hat{\rho})$ , is obtained by squaring both sides of (16) and then taking the expected value:

$$\begin{aligned} \text{var}(\hat{\rho}) &= E\{(\Delta\rho)^2\} \\ &\approx \frac{\bar{\mathbf{z}}_2^T \mathbf{W} E\{(\Delta\mathbf{z}_1 - \Delta\mathbf{z}_2\rho)(\Delta\mathbf{z}_1 - \Delta\mathbf{z}_2\rho)^T\} \mathbf{W}\bar{\mathbf{z}}_2}{(\bar{\mathbf{z}}_2^T \mathbf{W}\bar{\mathbf{z}}_2)^2} \\ &\approx \frac{\sigma^2}{\bar{\mathbf{z}}_2^T \mathbf{W}\bar{\mathbf{z}}_2}. \end{aligned} \quad (17)$$

Finally, the variance of  $\hat{\omega}$ ,  $\text{var}(\hat{\omega})$ , is obtained from (17) with the use of  $\rho = (2 \cos(\omega) + 1)$  [5]:

$$\text{var}(\hat{\omega}) \approx \frac{\text{var}(\hat{\rho})}{4 \sin^2(\omega)} \approx \frac{\sigma^2}{4(\bar{\mathbf{z}}_2^T \mathbf{W}\bar{\mathbf{z}}_2) \sin^2(\omega)}. \quad (18)$$

#### IV. Simulation Results

Computer simulations are carried out to evaluate the proposed dual-channel sine-wave parameter estimator by comparing its MSE performance with the optimal benchmark of the CRLB as well as the NLS method [2]. We use the number of iterations as the stopping criterion in the iterative

LLS algorithm, which is assigned as 5. For [2],  $4N$  uniformly-spaced grid points between  $[0, \pi]$  are used to

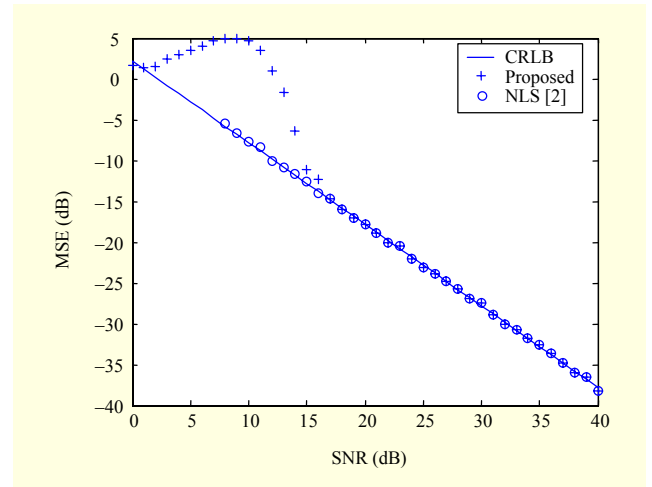


Fig. 2. Average MSE for amplitudes vs. SNR.

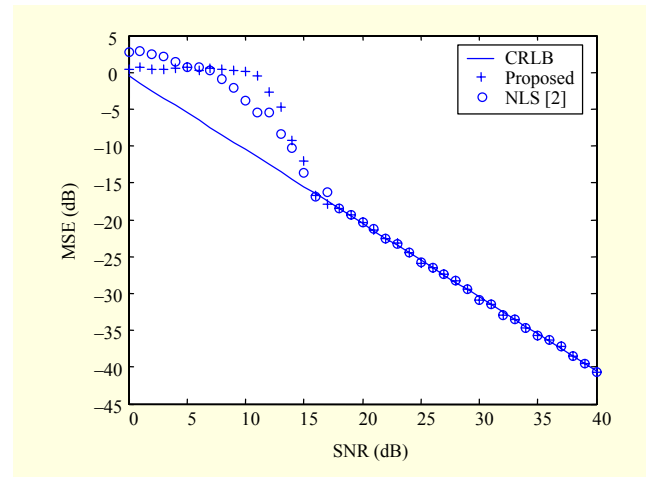


Fig. 3. Average MSE for phases vs. SNR.

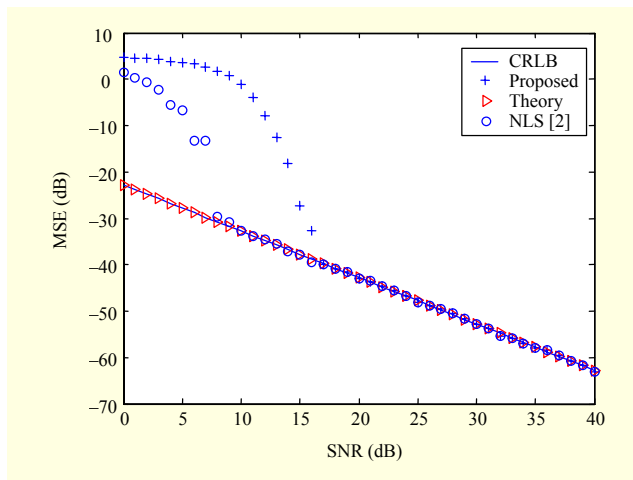


Fig. 1. MSE for frequency vs. SNR.

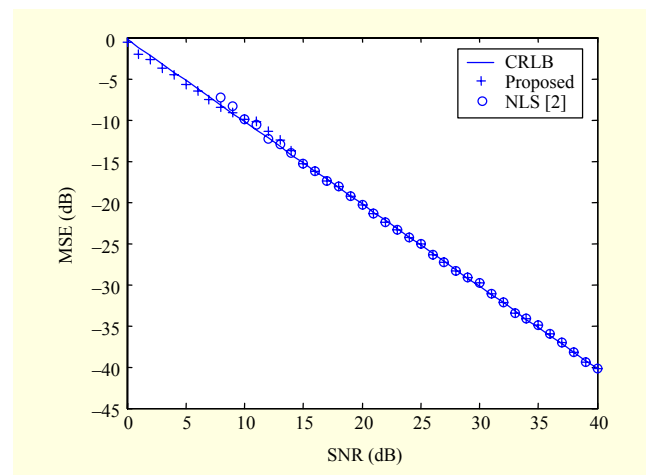


Fig. 4. Average MSE for offsets vs. SNR.

obtain the coarse estimate while the golden section search is employed for final estimation. The parameter settings are  $\omega = 0.3$ ,  $\alpha_1 = 3$ ,  $\alpha_2 = 2$ ,  $\phi_1 = 1$ ,  $\phi_2 = 2$ ,  $C_1 = 2$ ,  $C_2 = 2.5$ , and  $N = 20$ . We scale the white Gaussian noise sequences  $v_1(n)$  and  $v_2(n)$  to generate different SNR conditions, where  $\text{SNR} = (\alpha_1^2 / 2 + \alpha_2^2 / 2 + C_1^2 + C_2^2) / \sigma^2$ . For simplicity, the noise variances  $\sigma_1^2$  and  $\sigma_2^2$  are set as equal or  $r=1$ . All the results provided are averages of 500 independent runs.

Figures 1 through 4 show the MSEs for the frequency, amplitudes, phases, and offsets, respectively, at  $\text{SNR} \in [0, 40]$  dB. It is seen that all the LLS parameter estimates attain the optimum accuracy at sufficiently high SNR, that is, when  $\text{SNR} \geq 16$  dB. In this SNR range, the empirical MSE value also agrees well with the theoretical calculation of (18), which is equal to the CRLB. On the other hand, we observe that the NLS method gives better threshold performance in frequency and amplitude estimation but it has much larger errors in the amplitudes and offsets at smaller SNRs. Note that increasing the number of grid points in [2] can enhance the threshold performance of the frequency estimate but at the expense of higher computational requirement.

## V. Conclusion

An iterative LLS algorithm was devised to accurately estimate the parameters of dual-channel sinusoidal signals in white noise. The basic ideas are to utilize the LP property and LLS technique. The variance of the frequency estimate is derived and validated by simulations. It is also shown that the MSE performance of all parameter estimates attains CRLB in sufficiently high SNR conditions.

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