



# Low-Firing Pb(Zr,Ti)O<sub>3</sub>-Based Multilayer Ceramic Actuators Using Ag Inner Electrode

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We investigated the low firing of Li<sub>2</sub>CO<sub>3</sub> added 0.2Pb(Mg<sub>1/3</sub>Nb<sub>2/3</sub>)O<sub>3</sub> - 0.3Pb(Fe<sub>1/2</sub>Nb<sub>1/2</sub>) - 0.5Pb(Zr<sub>0.475</sub>Ti<sub>0.525</sub>)O<sub>3</sub> (PMN-PFN-PZT) ceramics and multilayer actuators (MLAs) using Ag inner electrodes. It was found that 0.1 wt% Li<sub>2</sub>CO<sub>3</sub> was quite effective in lowering the sintering temperature of PMN-PFN-PZT ceramics from 1,100 °C down to 900 °C without deteriorating their piezoelectric ceramics ( $d_{33} = 425$  pC/N and  $k_p = 61.9\%$ ). However, excess Li<sub>2</sub>CO<sub>3</sub> up to 0.3 wt% brings about unwanted problems such as the formation of a LiPbO<sub>2</sub> secondary phase and subsequent degradation in the piezoelectric properties. Using 0.1 wt% Li<sub>2</sub>CO<sub>3</sub> added PMN-PFN-PZT ceramics, MLAs with Ag inner electrodes were successfully fabricated, resulting in a normalized strain of 580 pm/V at an electric field of 1.5 kV/mm.

**Keywords:** Piezoelectric ceramics, Multilayer actuator, Internal electrode, Low firing

## 1. INTRODUCTION

Piezoelectric and electrostrictive actuators are widely used in applications requiring precision displacement control or high generative force (i.e., optical stage, precision mechatronic systems, and semiconductor devices) [1,2]. In particular, multilayer actuators (MLAs) using Pb(Zr,Ti)O<sub>3</sub> (PZT) ceramics have attracted much attention because of their merits, such as rapid operation, low power consumption, high precision control, and little noise [3,4] compared with conventional electromagnetic actuators.

Currently, most MLAs adopt expensive AgPd alloys as internal electrodes because they are stable between piezoelectric ceramic layers throughout a high-temperature sintering process. Therefore, there is ample necessity to explore inexpensive conducting materials as an internal electrode for low-cost and low-

firing MLAs. For utilization of Ag as an inner electrode, co-firing temperature should be lower than the melting point of Ag, which makes it difficult to attain excellent piezoelectric properties, since they are generally improved with microstructural evolution. To overcome such problems, the low-temperature sintering of PZT ceramics has been attempted by a variety of approaches: sol-gel method [5], reactive sintering [6], fine powders prepared by high-energy ball-milling [7,8], and low-melting sintering aids, such as Li<sub>2</sub>O [9], LiBiO<sub>2</sub> [10], LiSbO<sub>3</sub> [11], Li<sub>2</sub>CO<sub>3</sub> [12], and CuO [13,14].

In contrast, piezoelectric ceramics should possess high electric field-induced strain (EFIS) properties if they are to be applied to MLAs. It was reported that Pb(Mg<sub>1/3</sub>Nb<sub>2/3</sub>)O<sub>3</sub>-Pb(Zr,Ti)O<sub>3</sub> (PMN-PZT) ceramics exhibit high piezoelectric constants as well as EFIS near the morphotropic phase boundary [14-17]. Moreover, our recent study on Pb(Fe<sub>1/2</sub>Nb<sub>1/2</sub>) added PMN-PZT complex perovskite ceramics demonstrated enhancement in their dielectric and pyroelectric properties by adding Li<sub>2</sub>CO<sub>3</sub> as a sintering aid [15]. Therefore, this study investigates the effects of Li<sub>2</sub>CO<sub>3</sub> on the sintering behavior and piezoelectric properties of 0.2Pb(Mg<sub>1/3</sub>Nb<sub>2/3</sub>)O<sub>3</sub> - 0.5Pb(Zr<sub>0.475</sub>Ti<sub>0.525</sub>)O<sub>3</sub> - 0.3Pb(Fe<sub>1/2</sub>Nb<sub>1/2</sub>) (hereinafter, PMN-PFN-PZT) ceramics and the possibility of

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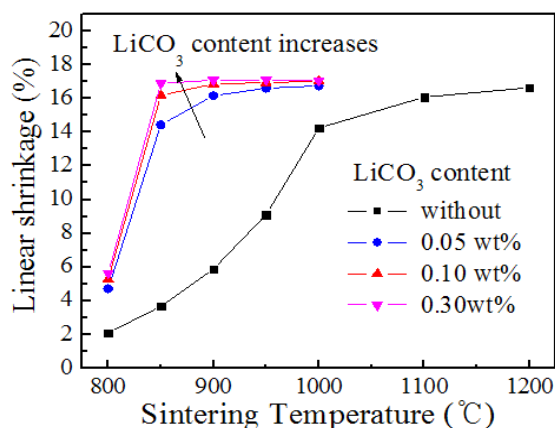


Fig. 1. Effect of  $\text{Li}_2\text{CO}_3$  addition on the firing shrinkage of PMN-PFN-PZT ceramics.

their application to low-firing MLAs using Ag inner electrodes.

## 2. EXPERIMENTS

Ceramic powder, with a composition of PMN-PFN-PZT, was synthesized using the columbite precursor method, which consists of a two-stage calcination process. In the first step, a mixture of  $\text{MgO}$ ,  $\text{Fe}_2\text{O}_3$ ,  $\text{Nb}_2\text{O}_5$ ,  $\text{ZrO}_2$ , and  $\text{TiO}_2$  powders (99.5% purity; Cerac Specialty Inorganics, Milwaukee, WI, USA) was properly weighed, according to the formula, and ball-milled with zirconia balls and deionized water for 24 hours. The mixed powders were dried and then calcined at  $1,100^\circ\text{C}$  for 2 hours, to form a columbite phase of  $(\text{Mg,Fe})\text{Nb}_2(\text{Zr,Ti})\text{O}_6$ . In the second step, a stoichiometric amount of  $\text{PbO}$ , with 99.5% purity, (supplied by the same company) was added and mixed with calcined powders by ball-milling for 24 hours again. After drying, it was re-calcined at  $850^\circ\text{C}$  for 2 hours. Before milling the calcined powders,  $\text{Li}_2\text{CO}_3$  was added as a sintering aid in the range of 0.05 to 0.3 wt%. Ceramic pellets with a 12-mm diameter were prepared by dry pressing at 98 MPa and fired at temperatures between  $800^\circ\text{C}$  and  $200^\circ\text{C}$  for 2 hours, in air.

MLAs were prepared using 0.1 wt%  $\text{Li}_2\text{CO}_3$  added PMN-PFN-PZT powders and thick film Ag. Piezoelectric ceramic sheets were obtained by tape casting ceramic slurry containing a mixture of piezoelectric powders, organic binders, a plasticizer, and solvents. The green sheets were cut into  $10 \times 10 \text{ cm}^2$  using a knife cutting machine. Ag paste was screen-printed on the ceramic sheet, and then laminated with 12-layers of ceramic sheets. After cutting into  $10 \text{ (W)} \times 15 \text{ (L)} \text{ mm}^2$ , the samples were soaked at  $500^\circ\text{C}$  for 6 hours, in air, to remove organic additives, and then co-fired at  $850\text{--}950^\circ\text{C}$  for 5 hours, in air.

## 3. RESULTS AND DISCUSSION

Figure 1 shows the firing shrinkage of PMN-PFN-PZT ceramics as a function of sintering temperature ( $T_s$ ) and the amount of  $\text{Li}_2\text{CO}_3$  sintering aid. Without  $\text{Li}_2\text{CO}_3$  addition, it is seen that sufficient densification occurs at temperatures higher than  $1,100^\circ\text{C}$ , while  $\text{Li}_2\text{CO}_3$  added specimens exhibit densification at a temperature as low as  $900^\circ\text{C}$ , indicating that  $\text{Li}_2\text{CO}_3$  is quite useful to lower  $T_s$  by at least  $200^\circ\text{C}$ , similarly to previous reports on  $\text{Li}_2\text{CO}_3$  added PMN-PZT ceramics [12,15].

The effect of  $\text{Li}_2\text{CO}_3$  on the sintering behavior is more clearly understood from microstructural observation. Figure 2 displays

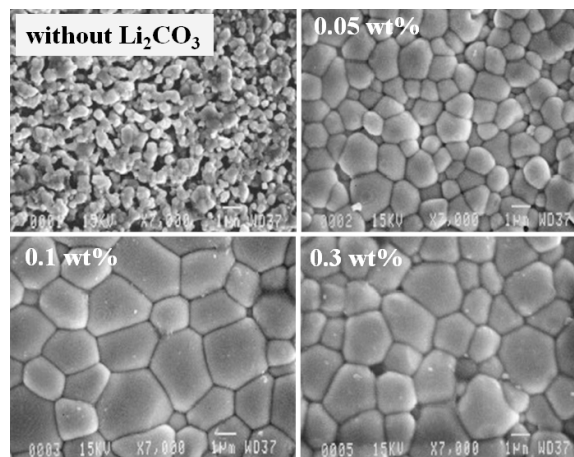


Fig. 2. Surface micrographs of PMN-PFN-PZT ceramics sintered at  $900^\circ\text{C}$  for 2 hours; (a) without, (b) 0.05 wt%, (c) 0.1 wt%, (d) 0.3 wt%  $\text{Li}_2\text{CO}_3$  added specimens.

the surface micrographs of specimens sintered at  $900^\circ\text{C}$  for 2 hours. As seen in Fig. 2(a), a specimen sintered without  $\text{Li}_2\text{CO}_3$  reveals little grain growth and densification because the particle size is almost similar to that of a green compact ( $\sim 0.5 \mu\text{m}$ ), and many pores can be also observed. However,  $\text{Li}_2\text{CO}_3$  added specimens show dense microstructures and significant grain growth; the average grain size for 0.05, 0.1, and 0.3 wt%  $\text{Li}_2\text{CO}_3$  is 1.4, 2.2, and  $1.8 \mu\text{m}$ , respectively.

Such an enhancement in density and grain size by  $\text{Li}_2\text{CO}_3$  was also observed in our previous work on PMN-PZT ceramics with added  $\text{Li}_2\text{CO}_3$  [7] or  $\text{Li}_2\text{O}$  [9]. A possible explanation is that sintering is enhanced by formation of a transient liquid phase at the initial stage [16], which is in turn dissolved into a matrix at a later stage of sintering. In this work, a low-melting Li compound was also detected from X-ray diffraction (XRD) analysis at high  $\text{Li}_2\text{CO}_3$  levels, as shown in Fig. 3, which compares XRD reflections of specimens for different  $\text{Li}_2\text{CO}_3$  amounts. All specimens correspond to perovskite symmetry, while a secondary phase that is identified as  $\text{LiPbO}_2$  is observed when the amount of  $\text{Li}_2\text{CO}_3$  reaches 0.3 wt%.

Figure 4 presents the piezoelectric constant  $d_{33}$  and planar piezoelectric coupling coefficient of PMN-PFN-PZT ceramics as a function of  $\text{Li}_2\text{CO}_3$  content. Both  $d_{33}$  and  $k_p$  reach their highest levels when  $\text{Li}_2\text{CO}_3$  content goes to 0.1 wt%, whose values are 425 pC/N and 61.9%, respectively. Further addition of  $\text{Li}_2\text{CO}_3$  results in drops in both  $d_{33}$  and  $k_p$ , which is believed to be due to the combined effects of decreased grain size, as seen in Fig. 2, and the secondary phase that was identified by XRD in Fig. 3. It should also be noted that the grain-size dependence of the piezoelectric constants in this work is very similar to a report by Swartz [17]. This phenomenon might be attributed to the inhibition of domain wall movement by grain boundaries whose effect becomes stronger as the grain size decreases.

MLAs were fabricated by laminating PMN-PFN-PZT green sheets with a screen-printed Ag-ceramic electrode. After co-firing, the dimension of a MLA was about  $8 \text{ (W)} \times 12 \text{ (L)} \times 1 \text{ (T)} \text{ mm}^3$ , in which 12 ceramic and 11 Ag inner electrode layers are alternatively stacked. The fractured surface of specimens sintered at 850, 900, and  $950^\circ\text{C}$  was observed using a scanning electron microscope and the results are provided in Fig. 5. Low-magnification micrographs (left column of Fig. 5) show well laminated multilayers with clear interfaces and a uniform thickness of about  $80 \mu\text{m}$  in piezoelectric layers.

In the case of inner electrode layers, the morphologies are

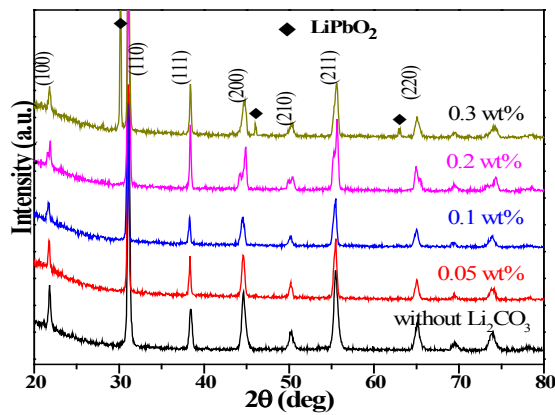


Fig. 3. X-ray diffraction patterns of PMN-PFN-PZT ceramics sintered with different amounts of  $\text{Li}_2\text{CO}_3$  sintering aid.

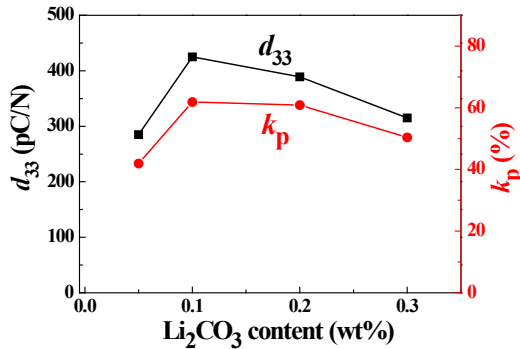


Fig. 4. The piezoelectric coefficient ( $d_{33}$ ) and planar piezoelectric coupling coefficient ( $k_p$ ) of PMN-PFN-PZT ceramics as a function of  $\text{Li}_2\text{CO}_3$  content.

more clearly seen in higher-magnification micrographs (right column). The Ag thickness is not uniform in a range of 3–5  $\mu\text{m}$ , moreover, their connectivity is broken when  $T_s = 950^\circ\text{C}$ , as indicated by arrows (region A), which seems to be due to the viscous flow of Ag near its melting point of about  $962^\circ\text{C}$  [18]. It was also reported that Ag thick films become unstable at  $950^\circ\text{C}$  in the case of the PMN-PZT/Ag multilayers [19].

EFIS was measured for a MLA sintered at  $900^\circ\text{C}$ , and the result is displayed in Fig. 6. The normalized strain  $S_{\text{max}}/E_{\text{max}}$  was measured as 580 pm/V, which is higher than the small signal  $d_{33}$  of 425 pC/N characterized with a Berlincourt  $d_{33}$  meter, as seen in Fig. 4, and is promising for high strain actuator applications. The difference between  $d_{33}$  and  $S_{\text{max}}/E_{\text{max}}$  indicates that piezoelectric constant obtained from the piezoelectric effect is different from that measured from the converse piezoelectric effect. Such a difference seems to be larger in lead-free piezoelectrics [20,21] than in Pb-based ones, even though exact understanding is still lacking.

#### 4. CONCLUSIONS

The effects of  $\text{Li}_2\text{CO}_3$  on the sintering behavior and piezoelectric properties of PMN-PFN-PZT ceramics have been investigated. It was found that  $\text{Li}_2\text{CO}_3$  is quite effective in lowering  $T_s$  from  $1,100^\circ\text{C}$  down to  $900^\circ\text{C}$  in PMN-PFN-PZT ceramics without degradation of their piezoelectric ceramics. However, excess  $\text{Li}_2\text{CO}_3$  up to 0.3 wt% brings about problems, such as the formation of

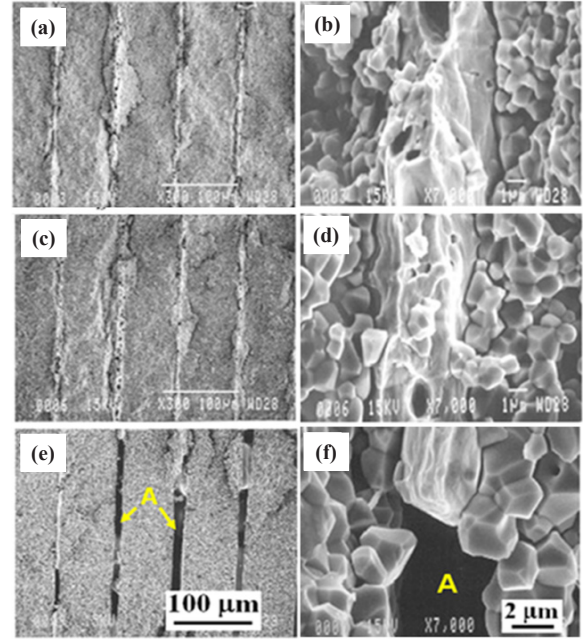


Fig. 5. The fractured cross-sectional micrographs of 0.1 wt%  $\text{Li}_2\text{CO}_3$  added PMN-PFN-PZT/Ag MLAs co-fired at different temperatures for 5 hours. The sintering temperature was  $850^\circ\text{C}$  for (a) and (b),  $900^\circ\text{C}$  for (c) and (d), and  $950^\circ\text{C}$  for (e) and (f), respectively.

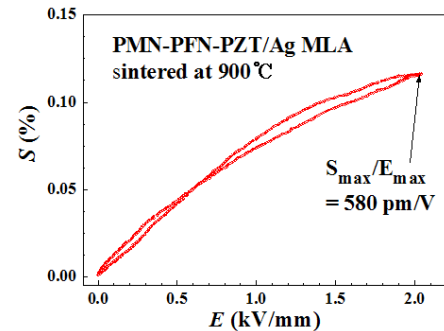


Fig. 6. Unipolar strain versus electric-field ( $S$ - $E$ ) hysteresis loop of 0.1 wt%  $\text{Li}_2\text{CO}_3$  added PMN-PFN-PZT/Ag MLAs co-fired at  $900^\circ\text{C}$  for 5 hours.

an unwanted  $\text{Li}_2\text{PbO}_3$  secondary phase and subsequent degradation in the piezoelectric properties. Using 0.1 wt%  $\text{Li}_2\text{CO}_3$  added PMN-PFN-PZT ceramics, MLAs using Ag inner electrodes were successfully fabricated, resulting in a normalized strain of 580 pm/V at a dc field of 1.5 kV/mm. This result is very promising for low-cost MLAs.

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