Analysis of marine accident probability in Mokpo waterways

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Abstract: The maritime risk assessment is important not only to evaluate the safety level of the ports and waterways but also to reduce potential maritime accidents at sea in terms of the proactive measures of the maritime accidents. In this paper, the collision risk assessment in Mokpo waterways has been carried out based on the IALA recommended model, IWRAP. To evaluate the accident probabilities in Mokpo waterways, all data of vessels were collected from AIS and Radar observations data and the computer simulations were carried out.

To assess the risk on the traffic, the scenario-base approach has been applied to the Mokpo waterway by using the maritime accident statics over the past 5 years.

Key words : accident probability, geometrical probability, causation probability, collision risk, AIS

1. Introduction

The Mokpo waterways are geographically surrounded by many islands. Many fishing vessels and tugs across the waterways disturb the safe passage of vessels on the route. The maritime risk assessment is important not only to evaluate the safety level of the ports and waterways but also to reduce maritime accidents at sea in terms of the proactive measures of the maritime accidents. However there are no quantitative risk assessment methods in Korea. The maritime safety assessment has been dependent on the qualitative method by some stakeholders including pilots, mariners. Recently, the risk assessment for the maritime traffic in waterways has been carried out several researchers(Kim et al, 2010; Yim and Kim, 2010). Fujii and Macduff modelled systematically the maritime accident probabilities which were based on the geometrical approaches among the vessels on collision and grounding courses(Fujii Y, et.al., 1974; Macduff T, 1974). With minor modification of Fujii's work, Pedersen evaluated the safety of navigation in many European waters(Pedersen P.T, 1995). Basically the IALA risk management tool, IWRAP(IALA Waterway Risk Assessment Programme), is theoretically based on Fujii and Macduff, and then evaluates quantitatively both collision and grounding risk in waterways(Peter Friis-Hansen, 2008; IALA, 2009). It is reported that the risk assessment by the IWRAP MK II agrees with the real situations in the European Waters (Kujala P. et al, 2009; Ylitalo J., 2009).

In this paper, the collision risk of the maritime traffic in Mokpo waterways was evaluated based on the Pedersen model(Pedersen P.T, 1995) which also consist of a part of IWRAP model. Taking the maritime accidents statistics into account, the frequency of collisions is computed for crossing situations and head-on situations. Especially, all the traffic data are collected from AIS as well as Radar observations. The accident probabilities are analyzed to determine the collision risk by the maritime traffic in the Mokpo waterways.

2. The traffic characteristics of Mokpo waterways

The vessels less than 100m including passenger ships, and towing vessels occupy more than 80% of maritime traffic in Mokpo waterways. Many fishing vessels navigate across the Mokpo waterways which are spatially restricted. In spring and autumn, the visibility of the waterways may be severely reduced. Fishing nets around the waterways may also be severe obstracles for the inbound and outbound vessels. Those vessels may be frequently exposed a dangerous situation on the Mokpo port entrance route.

Figure 1 represents Mokpo waterways and the locations of the collision/grounding accidents for the last 5 years. As shown in Fig. 1, many vessels are encountered with crossing situations around Bulmugido.

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Fig. 1 Mokpo waterways and the collision/grounding accident locations.

3. Risk modeling using ship traffic data

Marine accident probabilities are often modeled on basis of the works of Fujii and Macduff(Fujii Y et. al., 1974; Macduff T, 1974). Generally, the frequency of the collisions N_O , is defined as Eq.(1).

$$N_O = N_G \times P_C \tag{1}$$

where N_G is the geometrical number of collision candidates that are on a collision course. In other words, N_G accidents would occur if no the manoeuvres for collision were ever made. \boldsymbol{P}_{C} is the causation factor that is the probability of failing to avoid the accident while being on a collision course. From Eq.(1), it follows that N_O corresponds to the number of vessels to be probably in collision among N_g . Eq.(1) may be also used to calculate the frequency of grounding with N_G where corresponds to the geometrical number of grounding candidates. In this paper, Eq.(1) is used to compute the frequency of collisions.

3.1 Determination collision candidates of in crossing

It is known that the number of crossing collision candidates is determined by Eq.(2)(Peter Friis-Hansen, 2008).

$$N_{G}^{crossing} = \sum_{i,j} \frac{Q_{i}^{(1)} Q_{j}^{(2)}}{V_{i}^{(1)} V_{j}^{(2)}} D_{ij} V_{ij} \frac{1}{\sin\theta}$$
(2)
for 10° < $|\theta| < 170°$

where $Q_i^{(1)}$ is the number of movements of ship class i over the period of interest in waterway 1, $Q_i^{(2)}$ is the number of Fig. 3 Definition of geometrical collision diameter D_{ij}

movements of ship class j over the period of interest in waterway 2. In Fig. 2, the two vessels arriving from waterway 1 and waterway 2 are expected to be encountered. The ship from waterway 1 approaches the ship on waterway 2 with the relative velocity, V_{ij} of crossing as Eq.(3).

$$V_{ij} = \sqrt{(V_i^{(1)})^2 + (V_j^{(2)})^2 - 2V_i^{(1)}V_j^{(2)}\cos\theta}$$
(3)

where $V_i^{(1)}$ is the velocity of vessel for ship class i in waterway 1, $V_j^{(2)}$ is the velocity of ship class j in waterway 2 and θ stands for the crossing angle between the two waterways.



Fig. 2 Crossing waterways with risk area of ship-ship collision

 ${\cal D}_{ii}$ is the geometric collision diameter as illustrated in Fig. 3 and calculated by Eq.(4).

$$D_{ij} = \frac{L_i^{(1)} V_j^{(2)} + L_j^{(2)} V_i^{(1)}}{V_{ij}} \sin\theta + B_j^{(2)} \left\{ 1 - \left(\sin\theta \frac{V_i^{(1)}}{V_{ij}} \right)^2 \right\}^{\frac{1}{2}} (4)$$

$$+ B_i^{(1)} \left\{ 1 - \left(\sin\theta \frac{V_j^{(2)}}{V_{ij}} \right)^2 \right\}^{\frac{1}{2}}$$

where $L_i^{(1)}$ is the length of vessel in ship class *i* in the waterway 1, $L_j^{(2)}$ is the length of vessel in ship class *j* in the waterway 2. B_i and B_j are the breadth of vessel of ship class *i* and *j*, respectively.

3.2 Determination of collision candidates in head-on

The number of head-on collision candidates is computed by Eq.(5).

$$N_G^{head-on} = Lw \sum_{i,j} P_{G_{i,j}}^{head-on} \frac{V_{ij}}{V_i^{(1)} V_j^{(2)}} (Q_i^{(1)} Q_j^{(2)})$$
(5)

where L_w is the length of the waterway as shown in Fig. 4.



Fig. 4 Parallel waterways

 P_G is the probability that two ships will collide in a head on situation. This probability is expressed as Eq.(6).

$$P_{G_{i,j}}^{head-on} = \varPhi\left(\frac{B_{ij} - \mu_{ij}}{\sigma_{ij}}\right) - \varPhi\left(-\frac{B_{ij} + \mu_{ij}}{\sigma_{ij}}\right)$$
(6)

where $\Phi(x)$ is the standard normal distribution function of the random variable x, $\mu_{ij} = \mu_i + \mu_j$ is the mean sailing distance between the two vessels, $\sigma_{ij} = \sqrt{\sigma_i + \sigma_j}$ is the standard deviation of the joint distribution, and $B_{ij} = \frac{B_i + B_j}{2}$ is the average vessel breadth.

3.3 Determination of causation factor

The causation factor, P_C is the reduction factor with which the number of accident candidates has to be multiplied to get the estimated frequency of marine accidents. However, P_C is uncountable and then not tractable to calculate.

 P_C can be estimated by the scenario-based approach which is based on actual accidents or the synthesis approach which is calculated by Bayesian Belief Network(BBN) (Trucco et al, 2008). For simplicity, herein the scenario approach is applied to obtain P_C . Using the actual accidents over the last 5 years as shown in Table 1, the P_C can be calculated as Eq.(7).

$$P_C = \frac{N_C}{N_T} \tag{7}$$

where N_C is the number of maritime accidents calculated for the past 5 years and N_T is the number of maritime traffic for the same period.

Table 1 Causation probability by scenario-based approach

Year	N_T	N_C	P_C
2006	35,857	3	$8.4 imes 10^{-5}$
2007	37,241	3	$8.1 imes 10^{-5}$
2008	42,408	3	$7.1 imes 10^{-5}$
2009	42,958	4	$9.3\! imes\!10^{-5}$
2010	58,646	1	1.7×10^{-5}
total	217,110	14	$6.4 imes 10^{-5}$

On the other hand, it is found that P_C , from the results of IWRAP, is higher than those estimated by the scenario-based approach. Table 2 shows the default causation factors in IWRAP for the encounter type. Actually the IWRAP uses the synthesis approach based on BBN.

Table 2 Default causation factors in IWRAP

Type of encounter	P_C
Head-on	$0.5 imes 10^{-4}$
Overtaking	1.1×10^{-4}
Crossing	$1.3 imes 10^{-4}$
Bend	$1.3 imes 10^{-4}$
Merging	$1.3 imes 10^{-4}$
Grounding - forget to turn	$1.6 imes 10^{-4}$

4. Collision probability of Mokpo waterways

To evaluate the maritime accident probabilities in Mokpo waterways, the computer simulation using matlab has been carried out. The data of all vessels were collected from AIS and Radar observations for crossing and head-on situations. N_G were calculated from Eq.(2) and Eq.(5), respectively.

4.1 Crossing section : Around Bulmugido

As shown in Fig.5, many vessels are crossing the West-East passage.



Fig. 5 Crossing section in Mokpo Waterway

Mainly passenger ships and high speed crafts over 20knots are navigating on the route. Half of passenger ships from Mokpo–Gu are passing this fairway. The cargo ships occupy more than 60% of the vessels which are navigating northward or southward, and the towing ships 10%, otherships 30%. For West–East passage, most ships consist of passenger ships and encounter in crossing with North–South bound vessels. The number of vessels, average velocity, length, width of crossing section for a year are presented in Table 3.

Table 3 Vessels distribution observed in Mokpo Waterway

Type of Vessels		Number of vessels	Velocity (knot)	Length (L)	Width (B)
West-East	Passenger ships	4800	11	50	11
passage	High speed crafts	3840	25	38	10
	Towing ships	1322	6	150	12
North–South passage	Cargo ships	9732	10	70	13
	Other ships	3600	11	25	7

The collision candidates, N_G are calculated by Eq.(2) then N_G for the cross section in Fig. 5 is presented in Table 4.

 Table 4 Collision candidates of crossing section sorted by ship types

West-East passage		North-South passage		
Passenger ships	High speed crafts	Towing ships	Cargo ships	Other ships
64	38	23	66	14

 N_O in the crossing section is calculated by Eq.(1). The results are presented in Table 5. From Eq.(1) and Table 5, N_O stands for the frequency of collisions among N_g . Using the scenario based P_C , N_O is two times as high as the IWRAP default one. It is questionable for the reason why P_C has big difference between the scenario-based approach and the synthetic approach adopted in the IWRAP. However, it should be noted that P_C considers human elements and other environmental factors when it is calculated by BBN (Trucco P. et al, 2008). As mentioned in section 3.3, the IWRAP uses BBN to calculate P_C .

 Table 5 Frequency of collision for crossing situations in Mokpo Waterways

N_G	P_C	N_O
205	$6.4 imes 10^{-5}$ (scenario-based approach)	0.013
205	1.3×10^{-4} (synthesis approach : IWRAP)	0.027

4.2 Head-on section : around Mokpo bridge

Figure 6 shows the head-on section around Mokpo bridge, the passenger ships occupy 20%, the towing ships 10%, cargo ship 5%, other ships 65%. The number of vessels, velocity, length, width of crossing section for 1 year also are presented in Table 6. The daily data was collected for the traffic peak time, $08:00 \sim 12:00$ hours.



Fig. 6 Head-on section of Mokpo waterway

Table 7 shows N_G , which is calculated by Eq.(5) and represents the collision candidates in the head-on section sorted by ship types. Using N_G , the frequency of collisions N_O in Mokpo waterway is calculated by Eq.(1). and presented in Table 8.

Type of Vessels	Number of vessels	Velocity (knot)	Length (L)	Width (B)
Passenger ships	599	12.5	50	12
Cargo ships	150	8.3	90	15
Towing ships	263	5.5	150	20
Other ships	1805	9.8	20	8

Table 6 Ships navigating around head-on section

Table 7 Collision candidates in the head-on section sorted by ship types

Passenger ships	Cargo ships	Towing ships	Other ships
50	23	34	534

 Table 8 Frequency of Collisions for head-on situations in Mokpo Waterways

N_G	P_C	N_o
714	$\begin{array}{c} 6.4\times 10^{-5} \\ (\text{scenario-based} \ P_{C}) \end{array}$	0.046
	$\begin{array}{c} 0.5\times 10^{-4} \\ (\text{IWRAP default } P_{C}) \end{array}$	0.036

5. Conclusions

It is expected that the maritime risk assessment in Mokpo waterway contributes to the improvement of the safety and environment protection at sea by taking the proactive measures against potential risks at sea. Our approach is based on the IALA model-IWRAP. However, we used the collision accident statistics to compute the causation factor and then the collision frequency, while the IWRAP uses the BBN. Our approach was applied to assess the collision risk in Mokpo waterways. The causation factor is a key parameter to determine the collision frequency for a certain waterway, even though the collision candidates are apparently affected by the number of movements of ships due to its geometric model. It is not tractable to obtain the accurate causation factor due to human elements which affects vessel maneuver. Regardless of this, our approach helps to decide the potential risk for a collision in the Mokpo waterway by using the statistical data of the past accidents.

The frequency of collisions by the scenario based approach has been found to be less than IWRAP default value. To increase the reliability of the collision frequency, the casuation factor should be modelled by considering not only the vessel velocity, vessel traffic density, but also sea conditions, weather conditions, other human elements.

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