

A Comparative QSPR Study of Alkanes with the Help of Computational Chemistry

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The development of a variety of methods like AM1, PM3, PM5 and DFT now allows the calculation of atomic and molecular properties with high precision as well as the treatment of large molecules with predictive power. In this paper, these methods have been used to calculate a number of quantum chemical descriptors (like Klopman atomic softness in terms of E_n^{\ddagger} and E_m^{\ddagger} , chemical hardness, global softness, electronegativity, chemical potential, electrophilicity index, heat of formation, total energy etc.) for 75 alkanes to predict their boiling point values. The 3D modeling, geometry optimization and semiempirical & DFT calculations of all the alkanes have been made with the help of CAChe software. The calculated quantum chemical descriptors have been correlated with observed boiling point by using multiple linear regression (MLR) analysis. The predicted values of boiling point are very close to the observed values. The values of correlation coefficient (r^2) and cross validation coefficient (r_{cv}^2) also indicates the generated QSPR models are valuable and the comparison of all the methods indicate that the DFT method is most reliable while the addition of Klopman atomic softness E_n^{\ddagger} in DFT method improves the result and provides best correlation.

Key Word : DFT, Semiempirical methods, QSPR, Boiling point, Klopman atomic softness

Introduction

In our previous communications¹⁻⁶ we have employed semiempirical techniques to develop QSAR/QSPR models in which the quantum chemical descriptors have been successfully correlated with observed biological activity. Density functional theory (DFT)⁷⁻⁸ founded within the two basic theorems provided by Hohenberg and Kohn in 1960s⁹. The performance of DFT method in description of structural, energetic and magnetic molecular properties has been reviewed quite substantially in recent time. DFT methods are in general capable of generating a variety of isolated molecular properties such as ionization energies,¹⁰⁻¹¹ dipole moment,¹²⁻¹³ electrostatic potential,¹⁴⁻¹⁵ electron affinities,¹⁶⁻¹⁷ electronegativities¹⁶⁻¹⁷ and chemical hardness¹⁶⁻¹⁷ etc. quite accurately.

Thanikaivelan *et al.*¹⁸ presented a QSPR model for the prediction of boiling points of alkanes using ionization potential as quantum chemical descriptor (r^2 0.968, SE 8.7 degree). Grigoras¹⁹ QSPR model (r^2 0.941, SE 14.1 degree) for the prediction of boiling point employs MSI (molecular surface interactions) descriptors calculated from atomic surface areas and EHT net atomic charges. Murugan *et al.*²⁰ also found similar results like Grogros¹⁹ by independent correlations of boiling points, melting points and flash points of substituted pyridines (r^2 0.943 and SE 14.5 degree). Balban *et al.*²¹ presented the molecular descriptors based QSPR study of ketones and aldehydes (r^2 0.970, SE 6.49 degree), esters (r^2 0.987, SE 4.0 degree) and the combination of these two series of compounds (r^2 0.964 and SE 6.93 degree). Katritzky *et al.*²² employed the CODESSA software package²³⁻²⁴ to derive QSPR models for the boiling point of 298 diverse organic compounds. Their best 2-parameter regression (r^2 0.954, SE 16.15 degree) was obtained with the SQRC (Grav Ind all bonds) and the HA dependent HDCA-2/TMSA descriptors.²⁵ Katritzky *et al.*²² extended their QSPR

approach²⁶ to a set of 584 diverse organic compounds representative of all major classes of organic compounds containing C, H, O, N, S, F, Cl, Br, and I. The best correlations were obtained by a 6- and an 8-parameter model, (r^2 0.946, SE 18.9 degree). Cocchi *et al.*²⁷ presented the QSPR model for the boiling point prediction by using GOLPE²⁸ procedure (r^2 0.931, SE 17.27 degree). GOLPE procedure is based on statistical design and is aimed to improve the predictive ability of the models. Although numerous attempts have been made to correlate physical properties of organic compounds (particularly boiling point) with structural parameters,¹⁸⁻³⁵ there are very few papers employing quantum chemical descriptors for this purpose.^{20,55} In present work we have collected 75 alkanes³⁶ for the prediction of their boiling point values with the help of quantum chemical descriptors. The comparative QSPR models have been made with the help of AM1,³⁷ PM3,³⁸ PM5³⁹ and DFT⁷⁻⁸ methods. As we expected, the DFT method based model provides better result than the semiempirical method based models. We also have calculated Klopman atomic softness⁴⁰ values in terms of E_n^{\ddagger} at all the atoms of alkanes. The addition of highest E_n^{\ddagger} values of the atom in DFT model surprisingly improve the result of the model (especially in the values of standard error) and provide best correlation. These results are better than the previously known quantum chemical descriptor based study of boiling point.^{20,55}

Theory

In DFT the electronegativity commonly known by chemist is defined as negative of partial derivative of energy E of an atomic or molecular system with respect to the number of electron N for a constant external potential $\nu(r)$ ¹⁷

$$\mu = -\chi = -(\partial E / \partial N)_{\nu(r)} \quad (1)$$

In accordance with the earlier work of Iczkowski and Margrave,⁴¹ it should be remarked that when assuming a quadratic relationship between E and N and in a finite difference approximation equation-1 may be rewritten as

$$\chi = -\mu = -(I+A)/2 \quad (2)$$

where I and A are the vertical ionization energy and electron affinity respectively, thereby recovering the electronegativity definition of Mulliken.⁴² More over theoretical justification was provided for Sanderson's principle of electronegativity equalization which state that when two or more atoms come together to form molecule, their electronegativities become adjusted to the same intermediate value.⁴³⁻⁴⁵ The absolute hardness h is defined as,⁴⁶

$$\begin{aligned} \eta &= 1/2(\delta\mu/\delta N)v(r) \\ &= 1/2(\delta^2E/\delta N^2)v(r) \end{aligned} \quad (3)$$

Where E is the total energy, N the number of electrons of the chemical species and n(r) the external potential. The operational definition of absolute hardness and electro negativity is as

$$\eta = 1/2(I-A) \quad (4)$$

According to the Koopman's theorem, the I is simply the eigen value of HOMO with change of sign and A is the eigen value of LUMO with change of sign,¹⁷ hence the equation-2 and equation-4 may be written as

$$\eta = 1/2(E_{\text{LUMO}} - E_{\text{HOMO}}) \quad (5)$$

$$\chi = -\mu = -1/2(E_{\text{LUMO}} - E_{\text{HOMO}}) \quad (6)$$

We have also taken a general but important property of a molecular system the molecular weight as a descriptor. In the matter of QSPR of chemical system the total energy also plays important role. Total energy of a molecular system is the sum of the total electronic energy, E_{ee} and the energy of internuclear repulsion, E_{nr} . The total electronic energy of the system is given by,⁴⁷⁻⁴⁸

$$E = 1/2 P(H+F), \quad (7)$$

where P is density matrix and H is one-electron matrix.

The softness of an atom in a molecule was described by Klopman⁴⁰ and modified by Singh *et al.*^{2,49} The Klopman equation is as follows.

$$E_m^\ddagger = IP_m - a^2(IP_m - EA_m) - [\chi_r(C_r^m)^2 / R_r] (1 - 1/\epsilon) \times [q_r + 2b^2 \chi_r(C_r^m)^2] \quad (8)$$

$$E_m^\ddagger = IP_n - b^2(IP_n - EA_n) - [\chi_s(C_s^n)^2 / R_s] (1 - 1/\epsilon) \times [q_s + 2b^2 \chi_s(C_s^n)^2] \quad (9)$$

Where

E_n^\ddagger = Softness of a Lewis acid

E_m^\ddagger = Softness of a Lewis base

IP = Ionization potential of an atom in a molecule

EA = Electron affinity of an atom in a molecule

R and q = Radius and charge of atom s & r

C = Electron density

$\chi_r \geq q - (q-1)\sqrt{k}$ and $k = 0.75$

a & b = Variational parameter defined as $a^2 + b^2 = 1$

The ionization potential (IP) of an atom in a molecule, electron affinity (EA) of an atom in a molecule, charge (q) of an atom in a molecule and electron density (C) of an atom in a molecule are essential requirements for the solution of Klopman equations. The method for the calculation of ionization potential of an atom in a molecule (IP) has been described by Dewar and Morita.⁵⁰ Method for the calculation of electron affinity of an atom in a molecule (EA) has been described by us earlier.² The charge and electron density of an atom in a molecule can be obtained by the quantum chemical calculations. The softness values represented by E_n^\ddagger describe the electrophilic character of the molecule, whereas the softness values represented by E_m^\ddagger describe the nucleophilic character of the compound.⁵¹ Both E_n^\ddagger and E_m^\ddagger have been evaluated at all the atoms of each alkanes. The most reactive site as an acid will be that site which has the highest value of E_n^\ddagger and the most reactive site as a base will be that site which has the highest value of E_m^\ddagger . We have used highest E_n^\ddagger values as a descriptor because it provides better correlation. Charge and electron density have been calculated at the atom for which the E_n^\ddagger value is highest. Dielectric constant of water⁵² is used in all the Klopman atomic softness calculations.

Materials and Method

75 alkanes have been used as study material reported under Table-1 along with their observed boiling point values.³⁶ For QSPR prediction, the 3D modeling and geometry optimization of all the alkanes have been carried out with the help of CAChe Pro software by using semiempirical (AM1, PM3 and PMS) and DFT method. The DFT calculations have been made by using the B88-PW91 functional with DZVP basis set. The values of various descriptors like molecular weight (Mw), HOMO energy (eV) (E_{HOMO}), LUMO energy (eV) (E_{LUMO}), ionization potential (eV) (I), electron affinity (eV) (A), chemical hardness (η), global softness (S), electronegativity (χ), chemical potential (μ), electrophilicity index (ω), total energy (Hartree) (T_E), Klopman atomic softness (in terms of E_n^\ddagger and E_m^\ddagger) have been obtained from the quantum chemical calculations or calculated by solving the equations given in theory.

Multiple Linear Regression Analysis (MLR). The Project Leader program associated with CAChe Pro of Fujitsu and DATA Fit program, have been used for multiple linear regression (MLR) analysis. The Quantum chemical descriptors used as independent variables and the boiling point values as the dependent variable. In the statistical analyses, the systematic search was performed to determine the significant descriptors. In order to explore the reliability of the proposed model we have used the cross-validation method. Prediction error sum of squares (PRESS) is a standard index

Table 1. The name of alkanes used as study material

| No. | Name | No. | Name |
|-----|----------------------------------|-----|---|
| 1 | hexane | 39 | 2,4-dimethylhexane |
| 2 | 2-methylpentane | 40 | 2,2-dimethylhexane |
| 3 | 2,2-dimethylbutane | 41 | 3-ethyl-2-methylpentane |
| 4 | isopropylcyclopropane | 42 | 2,2,4-trimethylpentane |
| 5 | 1-ethyl-2-methylcyclopropane | 43 | 3-ethyl-3-methylpentane |
| 6 | 1,1,2-trimethylcyclopropane | 44 | pentacyclopropane |
| 7 | ethylcyclobutane | 45 | (1-methylbutyl)cyclopropane |
| 8 | 1,1-dimethylcyclobutane | 46 | 1-butyl-2-methylcyclopropane |
| 9 | methylcyclopentane | 47 | (1,2-dimethylpropyl)cyclopropane |
| 10 | 1,1'-bi(cyclopropyl) | 48 | 1-isobutyl-2-methylcyclopropane |
| 11 | bicyclo[2.2.0]hexane | 49 | 2-ethyl-1,1,2-trimethylcyclopropane |
| 12 | 1-methylbicyclo[2.1.0]pentane | 50 | 1,1,2,2,3-pentamethylcyclopropane |
| 13 | heptane | 51 | sec-butylcyclobutane |
| 14 | 2-methylhexane | 52 | 1,2-diethylcyclobutane |
| 15 | 2,4-dimethylpentane | 53 | propylcyclopentane |
| 16 | 2,3-dimethylpentane | 54 | isopropylcyclopentane |
| 17 | 2,2,3-trimethylbutane | 55 | 1,2,4-trimethylcyclopentane |
| 18 | butylcyclopropane | 56 | 1-ethyl-1-methylcyclopentane |
| 19 | 1,2-diethylcyclopropane | 57 | 1,1,2-trimethylcyclopentane |
| 20 | 1-methyl-1-propylcyclopropane | 58 | 1-ethyl-cyclohexane |
| 21 | 1,1-diethylcyclopropane | 59 | 1,2-dimethylcyclohexane |
| 22 | 1-isopropyl-1-methylcyclopropane | 60 | 1,1-dimethylcyclohexane |
| 23 | 1-ethyl-1,2-dimethylcyclopropane | 61 | (2-cyclopropylethyl)cyclopropane |
| 24 | 1,1,2,2-tetramethylcyclopropane | 62 | bicyclo[3.3.0]octane |
| 25 | isopropylcyclobutane | 63 | bicyclo[5.1.0]octane |
| 26 | 1-ethyl-3-methylcyclobutane | 64 | 2-methylbicyclo[2.2.1]heptane |
| 27 | 1,3-dimethylcyclopentane | 65 | 2-methylbicyclo[3.2.0]heptane |
| 28 | 1,2-dimethylcyclopentane | 66 | 1-methylbicyclo[2.2.1]heptane |
| 29 | cycloheptane | 67 | 1-methylbicyclo[4.1.0]heptane |
| 30 | (cyclopropylmethyl)cyclopropane | 68 | 3,3-dimethylbicyclo[3.1.0]hexane |
| 31 | bicyclo[3.2.0]heptane | 69 | 2,2,4,4-tetramethylbicyclo[1.1.0]butane |
| 32 | 2-methylbicyclo[3.1.0]hexane | 70 | 1,2,2,3-tetramethylbicyclo[1.1.0]butane |
| 33 | 1,2-diethyl-3-methylcyclopropane | 71 | tricyclo[5.1.0.0 3,5]octane |
| 34 | 1-methylbicyclo[3.1.0]hexane | 72 | tricyclo[3.2.1.0 2,4]octane |
| 35 | tricyclo[4.1.0.0 2,4]heptane | 73 | 3-methyltetracyclo[2.2.1.0]heptane |
| 36 | 2-methylpentane | 74 | 1-methylcyclohexane |
| 37 | 3-methylpentane | 75 | 2,2,3-trimethylpentane |
| 38 | 3-ethylhexane | | |

to measure the accuracy of a modeling method based on the cross-validation technique. The r_{cv}^2 can easily be calculated by using equation-10 based on the PRESS and SSY (Sum of squares of deviations of the experimental values from their mean).

$$r_{cv}^2 = 1 - \frac{PRESS}{SSY} = 1 - \frac{\sum_{i=1}^n (y_{exp} - y_{pred})^2}{\sum_{i=1}^n (y_{exp} - \bar{y})^2} \quad (10)$$

Various regression equations have been developed by using selected quantum chemical descriptors. The best fitted regression equations have been used for the calculation of boiling points (BP_{Pred}). In Models 1-4, the use of three descriptors (chemical hardness, total energy and molecular weight) as

independent variables gave nice correlation. In Model-5, the use of E_n^\ddagger values in combination with above three descriptors as independent variables provide best result.

Results and Discussion

Previously a number of descriptors have been identified and they are capable to correlate successfully the properties with structure of a chemical system.^{1-4,53-54} In this paper we are using chemical hardness (η), total energy (T_E in Hartree), molecular weight (M_w) and Klopman atomic softness (E_n^\ddagger) as descriptor for the prediction of boiling point of alkanes. The importance of hardness and total energy for the prediction was described earlier by Karlsen *et al.*⁵⁵ Generally, the boiling point increases as the length of the carbon atom chain increase, so the molecular weight can be an important

Table 2. The AM1 based global descriptors and observed & predicted boiling points

| No. | M _w | E _T | η | BPObs | BPPred | Residual | No. | M _w | E _T | η | BPObs | BPPred | Residual |
|-----|----------------|----------------|--------|-------|--------|----------|-----------------|----------------|----------------|--------|-------|--------|----------|
| 1 | 86.177 | -44.281 | 7.411 | 68.7 | 56.66 | 12.04 | 39 | 114.230 | -58.572 | 7.302 | 109.4 | 113.49 | -4.09 |
| 2 | 86.177 | -44.282 | 7.409 | 60.3 | 56.62 | 3.68 | 40 | 114.230 | -58.583 | 7.348 | 106.8 | 113.54 | -6.74 |
| 3 | 86.177 | -44.286 | 7.468 | 49.7 | 57.03 | -7.33 | 41 | 114.230 | -58.566 | 7.250 | 115.6 | 113.19 | 2.41 |
| 4 | 84.161 | -42.761 | 6.857 | 58.3 | 64.39 | -6.09 | 42 | 114.230 | -58.576 | 7.326 | 99.2 | 113.55 | -14.35 |
| 5 | 84.161 | -42.765 | 6.719 | 63.0 | 62.98 | 0.02 | 43 | 114.230 | -58.565 | 7.239 | 118.2 | 113.13 | 5.07 |
| 6 | 84.161 | -42.662 | 6.541 | 52.6 | 64.88 | -12.28 | 44 | 112.214 | -57.060 | 6.873 | 128.0 | 122.11 | 5.90 |
| 7 | 84.161 | -42.830 | 7.259 | 70.7 | 65.76 | 4.94 | 45 | 112.214 | -57.055 | 6.829 | 117.7 | 121.86 | -4.16 |
| 8 | 84.161 | -42.835 | 7.201 | 53.6 | 65.05 | -11.45 | 46 | 112.214 | -57.063 | 6.697 | 124.0 | 120.33 | 3.67 |
| 9 | 84.161 | -42.871 | 7.289 | 71.8 | 64.63 | 7.17 | 47 | 112.214 | -57.060 | 6.894 | 115.5 | 122.29 | -6.79 |
| 10 | 82.145 | -41.246 | 6.503 | 76.0 | 73.81 | 2.19 | 48 | 112.214 | -57.062 | 6.694 | 110.0 | 120.36 | -10.36 |
| 11 | 82.145 | -41.195 | 6.041 | 83.0 | 71.27 | 11.73 | 49 | 112.214 | -57.067 | 6.417 | 104.5 | 117.59 | -13.09 |
| 12 | 82.145 | -41.286 | 6.258 | 60.5 | 70.16 | -9.66 | 50 | 112.214 | -57.067 | 6.353 | 100.5 | 116.98 | -16.48 |
| 13 | 100.203 | -51.429 | 7.377 | 98.5 | 85.17 | 13.33 | 51 | 112.214 | -57.126 | 7.205 | 123.0 | 122.92 | 0.08 |
| 14 | 100.203 | -51.430 | 7.361 | 90.0 | 84.99 | 5.01 | 52 | 112.214 | -57.126 | 7.122 | 119.0 | 122.14 | -3.14 |
| 15 | 100.203 | -51.430 | 7.359 | 80.5 | 84.96 | -4.46 | 53 | 112.214 | -57.166 | 7.260 | 131.0 | 122.04 | 8.96 |
| 16 | 100.203 | -51.426 | 7.362 | 89.8 | 85.14 | 4.66 | 54 | 112.214 | -57.168 | 7.217 | 126.4 | 121.58 | 4.82 |
| 17 | 100.203 | -51.431 | 7.310 | 80.9 | 84.47 | -3.57 | 55 | 112.214 | -57.168 | 7.221 | 115.0 | 121.60 | -6.60 |
| 18 | 98.188 | -49.911 | 6.878 | 98.0 | 93.34 | 4.67 | 56 | 112.214 | -57.166 | 7.236 | 121.5 | 121.82 | -0.32 |
| 19 | 98.188 | -49.912 | 6.745 | 90.0 | 92.05 | -2.05 | 57 | 112.214 | -57.168 | 7.211 | 114.0 | 121.51 | -7.51 |
| 20 | 98.188 | -49.916 | 6.676 | 84.9 | 91.30 | -6.40 | 58 | 112.214 | -57.182 | 7.169 | 131.8 | 120.64 | 11.16 |
| 21 | 98.188 | -49.908 | 6.639 | 88.6 | 91.21 | -2.61 | 59 | 112.214 | -57.185 | 7.196 | 126.6 | 120.77 | 5.83 |
| 22 | 98.188 | -49.913 | 6.661 | 81.5 | 91.24 | -9.74 | 60 | 112.214 | -57.183 | 7.162 | 119.5 | 120.53 | -1.03 |
| 23 | 98.188 | -49.917 | 6.551 | 85.2 | 90.09 | -4.89 | 61 | 110.199 | -55.542 | 6.755 | 129.0 | 133.84 | -4.84 |
| 24 | 98.188 | -49.920 | 6.453 | 78.0 | 89.06 | -11.06 | 62 | 110.199 | -55.725 | 7.093 | 137.0 | 130.67 | 6.33 |
| 25 | 98.188 | -49.981 | 7.230 | 92.7 | 94.24 | -1.54 | 63 | 110.199 | -55.654 | 6.694 | 141.0 | 129.38 | 11.62 |
| 26 | 98.188 | -49.980 | 7.150 | 89.5 | 93.52 | -4.02 | 64 | 110.199 | -55.652 | 5.566 | 125.0 | 118.87 | 6.13 |
| 27 | 98.188 | -50.020 | 7.253 | 91.3 | 93.07 | -1.77 | 65 | 110.199 | -55.620 | 6.628 | 130.5 | 129.95 | 0.56 |
| 28 | 98.188 | -50.019 | 7.266 | 95.6 | 93.23 | 2.37 | 66 | 110.199 | -55.739 | 4.404 | 117.0 | 105.00 | 12.00 |
| 29 | 98.188 | -50.019 | 7.258 | 118.4 | 93.17 | 25.23 | 67 | 110.199 | -55.660 | 6.545 | 125.0 | 127.76 | -2.76 |
| 30 | 96.172 | -48.393 | 6.760 | 102.0 | 105.09 | -3.09 | 68 ^a | 110.199 | -55.651 | 6.673 | 115.0 | 129.29 | -14.29 |
| 31 | 96.172 | -48.473 | 6.650 | 110.5 | 101.28 | 9.22 | 69 ^a | 110.199 | -55.470 | 5.997 | 104.0 | 129.22 | -25.22 |
| 32 | 96.172 | -48.502 | 6.658 | 100.0 | 100.37 | -0.37 | 70 ^a | 110.199 | -55.476 | 5.625 | 105.0 | 125.53 | -20.53 |
| 33 | 96.172 | -48.505 | 6.585 | 103.0 | 99.55 | 3.45 | 71 | 108.183 | -54.139 | 6.535 | 142.0 | 140.64 | 1.36 |
| 34 | 96.172 | -48.506 | 6.482 | 92.0 | 98.57 | -6.57 | 72 | 108.183 | -53.849 | 4.273 | 136.0 | 129.48 | 6.52 |
| 35 | 94.156 | -46.984 | 6.525 | 105.0 | 111.96 | -6.96 | 73 | 110.199 | -55.732 | 6.469 | 120.5 | 124.57 | -4.07 |
| 36 | 114.230 | -58.578 | 7.334 | 117.6 | 113.55 | 4.05 | 74 | 98.188 | -50.036 | 7.216 | 101.0 | 92.17 | 8.83 |
| 37 | 114.230 | -58.575 | 7.314 | 118.9 | 113.47 | 5.44 | 75 | 114.230 | -58.577 | 7.303 | 109.8 | 113.32 | -3.52 |

M_w is the molecular weight, E_T is the total energy, η is the chemical hardness, BPObs is the observed boiling point in centigrade and BPPred is the predicted boiling point with the help of the AM1 method. ^adata points are not included in deriving regression equation. Residual is the difference between observed and predicted boiling point.

descriptor for the prediction of boiling point. It is known that the charge and electron density are important in many physico-chemical properties of the compound.⁵⁵ Klopman atomic softness strongly depends on the charge and electron density of atom and has been proven a useful quantum chemical descriptor.³⁻⁴

The values of all these descriptors for all the alkanes have been calculated with the help of AM1, PM3, PMS and DFT methods by using CAChe Pro software. To make QSPR model based on AM1 method we have generated various equations by employing all the independent variables and the best-fitted equation of this class is equation-11. The predicted boiling point (BPPred) from equation-11 is reported under Table 2. The statistical quality of the equation is good as is clear from its correlation coefficient r² value, which is

0.891, and the cross validation coefficient r_{cv}² value, which is 0.885. In this model compounds 68, 69 and 70 have been identified as outlier and the descriptor values of these compounds are not included in deriving regression equation. The Plot of experimental vs. predicted boiling point values for this model is given in Figure 1.

$$\text{B.P. AM1} = 19.69 \text{ M}_w + 34.6063 \text{ E}_T + 9.36229 \eta - 177.126 \\ r_{cv}^2 = 0.885 \quad r^2 = 0.891, \text{ SE} = 7.9, \text{ Degree of freedom} = 0.88 \quad (11)$$

The second QSPR model has been made with the help of PM3 based results. In this model we have generated various equations by employing several quantum chemical descriptors and the only best fitted equation is reported here. The

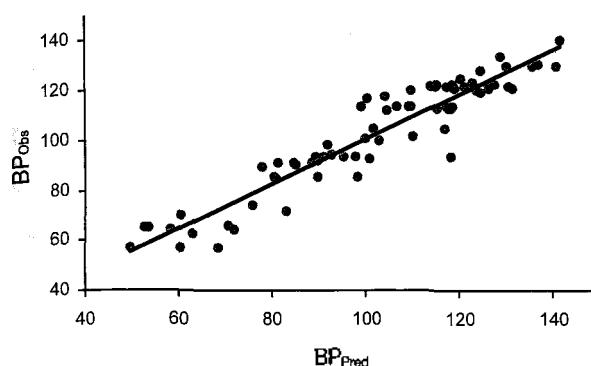


Figure 1. The trend of observed and predicted boiling points using AM1 based model

Table 3. The PM3 based global descriptors and observed & predicted boiling points

| No. | M _w | E _T | η | BP _{Obs} | BP _{Pred} | Residual | No. | M _w | E _T | η | BP _{Obs} | BP _{Pred} | Residual |
|-----------------|----------------|----------------|--------|-------------------|--------------------|----------|-----------------|----------------|----------------|--------|-------------------|--------------------|----------|
| 1 | 86.177 | -44.397 | 7.3205 | 68.7 | 58.30 | 10.40 | 39 | 114.230 | -58.718 | 7.3040 | 109.4 | 114.10 | -4.70 |
| 2 | 86.177 | -44.402 | 7.3350 | 60.3 | 58.48 | 1.82 | 40 | 114.230 | -58.732 | 7.2290 | 106.8 | 111.90 | -5.10 |
| 3 | 86.177 | -44.413 | 7.4955 | 49.7 | 61.90 | -12.20 | 41 | 114.230 | -58.709 | 7.0470 | 115.6 | 108.30 | 7.30 |
| 4 | 84.161 | -42.846 | 6.9980 | 58.3 | 64.35 | -6.05 | 42 | 114.230 | -58.732 | 7.2870 | 99.2 | 113.20 | -14.00 |
| 5 | 84.161 | -42.855 | 6.8850 | 63.0 | 61.38 | 1.62 | 43 | 114.230 | -58.710 | 7.1405 | 118.2 | 110.50 | 7.70 |
| 6 | 84.161 | -42.663 | 6.4110 | 52.6 | 56.68 | -4.08 | 44 | 112.214 | -57.164 | 6.9985 | 128.0 | 120.70 | 7.30 |
| 7 | 84.161 | -42.913 | 7.2165 | 70.7 | 67.24 | 3.46 | 45 | 112.214 | -57.161 | 6.9385 | 117.7 | 119.40 | -1.70 |
| 8 | 84.161 | -42.931 | 7.2790 | 53.6 | 68.11 | -14.51 | 46 | 112.214 | -57.178 | 6.8475 | 124.0 | 116.60 | 7.40 |
| 9 | 84.161 | -42.960 | 7.2605 | 71.8 | 66.70 | 5.10 | 47 | 112.214 | -57.170 | 7.0420 | 115.5 | 121.50 | -6.00 |
| 10 | 82.145 | -41.291 | 6.6415 | 76.0 | 69.77 | 6.23 | 48 | 112.214 | -57.180 | 6.8315 | 110.0 | 116.20 | -6.20 |
| 11a | 82.145 | -41.250 | 6.0965 | 83.0 | 58.25 | 24.75 | 49 | 112.214 | -57.207 | 6.5700 | 104.5 | 109.10 | -4.60 |
| 12 | 82.145 | -41.362 | 6.4390 | 60.5 | 62.57 | -2.07 | 50 | 112.214 | -57.215 | 6.5060 | 100.5 | 107.30 | -6.80 |
| 13 | 100.203 | -51.557 | 7.2865 | 98.5 | 85.62 | 12.88 | 51 | 112.214 | -57.234 | 7.1665 | 123.0 | 122.30 | 0.70 |
| 14 | 100.203 | -51.562 | 7.2670 | 90.0 | 84.99 | 5.01 | 52 | 112.214 | -57.241 | 7.1545 | 119.0 | 121.80 | -2.80 |
| 15 | 100.203 | -51.567 | 7.3230 | 80.5 | 86.15 | -5.65 | 53 | 112.214 | -57.277 | 7.1970 | 131.0 | 121.50 | 9.50 |
| 16 | 100.203 | -51.557 | 7.3830 | 89.8 | 87.88 | 1.92 | 54 | 112.214 | -57.280 | 7.1865 | 126.4 | 121.20 | 5.20 |
| 17 | 100.203 | -51.570 | 7.3630 | 80.9 | 86.96 | -6.06 | 55 | 112.214 | -57.292 | 7.2615 | 115.0 | 122.50 | -7.50 |
| 18 | 98.188 | -50.005 | 7.0025 | 98.0 | 92.63 | 5.37 | 56 | 112.214 | -57.284 | 7.2390 | 121.5 | 122.30 | -0.80 |
| 19 | 98.188 | -50.015 | 6.8515 | 90.0 | 88.69 | 1.31 | 57 | 112.214 | -57.292 | 7.2200 | 114.0 | 121.60 | -7.60 |
| 20 | 98.188 | -50.022 | 6.8290 | 84.9 | 87.93 | -3.03 | 58 | 112.214 | -57.287 | 7.2290 | 131.8 | 121.90 | 9.90 |
| 21 | 98.188 | -50.010 | 6.7490 | 88.6 | 86.44 | 2.16 | 59 | 112.214 | -57.298 | 7.3165 | 126.6 | 123.60 | 3.00 |
| 22 | 98.188 | -50.022 | 6.8185 | 81.5 | 87.69 | -6.19 | 60 | 112.214 | -57.293 | 7.2430 | 119.5 | 122.10 | -2.60 |
| 23 | 98.188 | -50.031 | 6.7045 | 85.2 | 84.67 | 0.53 | 61 | 110.199 | -55.612 | 6.8725 | 129.0 | 131.40 | -2.40 |
| 24 | 98.188 | -50.044 | 6.6070 | 78.0 | 81.93 | -3.93 | 62 | 110.199 | -55.812 | 7.0845 | 137.0 | 129.60 | 7.40 |
| 25 | 98.188 | -50.078 | 7.1900 | 92.7 | 94.58 | -1.88 | 63 | 110.199 | -55.723 | 6.8300 | 141.0 | 126.60 | 14.40 |
| 26 | 98.188 | -50.083 | 7.1930 | 89.5 | 94.48 | -4.98 | 64 | 110.199 | -55.820 | 6.8865 | 125.0 | 124.70 | 0.30 |
| 27 | 98.188 | -50.127 | 7.2505 | 91.3 | 94.35 | -3.05 | 65 | 110.199 | -55.711 | 6.7545 | 130.5 | 125.30 | 5.20 |
| 29 ^a | 98.188 | -50.106 | 7.2585 | 95.6 | 95.25 | 0.35 | 66 | 110.199 | -55.835 | 7.1915 | 117.0 | 131.40 | -14.40 |
| 28 | 98.188 | -50.125 | 7.2385 | 118.4 | 94.12 | 24.28 | 67 | 110.199 | -55.751 | 6.7035 | 125.0 | 122.70 | 2.30 |
| 30 | 96.172 | -48.451 | 6.8735 | 102.0 | 103.30 | -1.30 | 68 | 110.199 | -55.744 | 6.8325 | 115.0 | 126.00 | -11.00 |
| 31 | 96.172 | -48.546 | 6.7760 | 110.5 | 97.82 | 12.68 | 69 | 110.199 | -55.595 | 6.1140 | 104.0 | 114.10 | -10.10 |
| 32 | 96.172 | -48.576 | 6.7825 | 100.0 | 96.96 | 3.04 | 70 | 110.199 | -55.627 | 5.8160 | 105.0 | 105.90 | -0.90 |
| 33 | 96.172 | -48.583 | 6.6985 | 103.0 | 94.75 | 8.25 | 71 | 108.183 | -54.195 | 6.6310 | 142.0 | 134.90 | 7.10 |
| 34 | 96.172 | -48.591 | 6.6295 | 92.0 | 92.83 | -0.83 | 72 ^a | 108.183 | -54.248 | 5.4455 | 136.0 | 105.00 | 31.00 |
| 35 | 94.156 | -47.026 | 6.6290 | 105.0 | 107.00 | -2.00 | 73 | 110.199 | -55.817 | 7.2325 | 120.5 | 133.00 | -12.50 |
| 36 | 114.230 | -58.721 | 7.2330 | 117.6 | 112.30 | 5.30 | 74 | 98.188 | -50.131 | 7.3270 | 101.0 | 96.00 | 5.00 |
| 37 | 114.230 | -58.717 | 7.2305 | 118.9 | 112.40 | 6.50 | 75 | 114.230 | -58.726 | 7.3000 | 109.8 | 113.80 | -4.00 |
| 38 | 114.230 | -58.710 | 7.1150 | 118.5 | 109.90 | 8.60 | | | | | | | |

M_w is the molecular weight, E_T is the total energy, η is the chemical hardness, BP_{Obs} is the observed boiling point in centigrade and BP_{Pred} is the predicted boiling point with the help of the PM3 method. ^adata points are not included in deriving regression equation. Residual is the difference between observed and predicted boiling point.

best fitted equation for the prediction of boiling point (BP_{Pred}) is equation-12 and the predicted values are reported under Table 3. The statistical quality for this model is better than AM1 model. The correlation coefficient r² value is 0.910, and the cross validation coefficient r_{cv}² value is 0.904. In this model the outlier compounds are 11, 29 and 72. The descriptor values of these compounds are not included in deriving regression equation. The Plot of experimental vs. predicted boiling point values for this model is given in Figure 2.

$$\text{B. P. PM3} = 19.3459 M_w + 33.9725 E_T + 23.6533 \eta - 273.751 \\ r_{cv}^2 = 0.904 \quad r^2 = 0.910, \text{SE} = 7.5, \text{Degree of freedom} = 0.89 \\ (12)$$

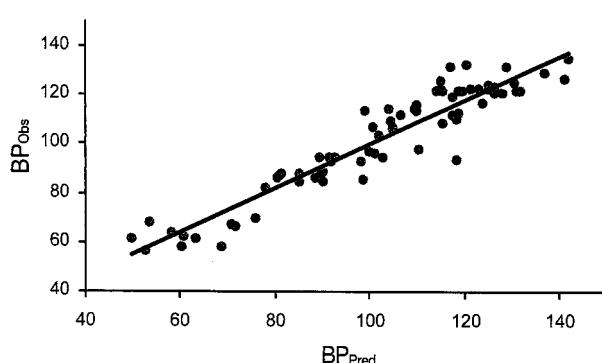


Figure 2. The trend of observed and predicted boiling points using PM3 based model

The third QSPR model has been made with the help of PM5 based results. The various equations for boiling point prediction have been generated by employing different descriptors based on PM5 calculations. The best-fitted equation for this class is equation-12. The predicted boiling points from equation-13 are given under Table 4. The results are reliable as is clear from correlation coefficient r^2 , which is 0.911, and the cross validation coefficient r_{cv}^2 , which is 0.905. In this model also three compounds 11, 13 and 29 are outliers and the descriptor values of these compounds are not included in deriving regression equation. The statistical quality of this method is similar like PM3 method. The Plot of experimental vs. predicted boiling point values for this model is given in Figure 3.

Table 4. The PM5 based global descriptors and observed & predicted boiling points

| No. | M_w | E_T | η | BP _{Obs} | BP _{Pred} | Residual | No. | M_w | E_T | η | BP _{Obs} | BP _{Pred} | Residual |
|-----------------|---------|---------|--------|-------------------|--------------------|----------|-----|---------|---------|--------|-------------------|--------------------|----------|
| 1 | 86.177 | -44.353 | 6.8280 | 68.70 | 56.32 | 12.38 | 39 | 114.230 | -58.659 | 6.8320 | 109.40 | 113.40 | -4.00 |
| 2 | 86.177 | -44.356 | 6.8920 | 60.30 | 58.04 | 2.26 | 40 | 114.230 | -58.670 | 6.8060 | 106.80 | 112.30 | -5.50 |
| 3 | 86.177 | -44.362 | 7.0270 | 49.70 | 61.63 | -11.93 | 41 | 114.230 | -58.654 | 6.7605 | 115.60 | 111.60 | 4.00 |
| 4 | 84.161 | -42.810 | 6.6900 | 58.30 | 65.46 | -7.16 | 42 | 114.230 | -58.666 | 6.8585 | 99.20 | 113.90 | -14.70 |
| 5 | 84.161 | -42.819 | 6.5510 | 63.00 | 61.24 | 1.76 | 43 | 114.230 | -58.659 | 6.7460 | 118.20 | 111.00 | 7.20 |
| 6 | 84.161 | -42.664 | 6.2110 | 52.60 | 56.78 | -4.18 | 44 | 112.214 | -57.114 | 6.6285 | 128.00 | 120.80 | 7.20 |
| 7 | 84.161 | -42.890 | 6.8085 | 70.70 | 66.14 | 4.56 | 45 | 112.214 | -57.117 | 6.6040 | 117.70 | 120.00 | -2.30 |
| 8 | 84.161 | -42.899 | 6.8915 | 53.60 | 68.17 | -14.57 | 46 | 112.214 | -57.128 | 6.4895 | 124.00 | 116.40 | 7.60 |
| 9 | 84.161 | -42.925 | 6.8590 | 71.80 | 66.41 | 5.39 | 47 | 112.214 | -57.118 | 6.6810 | 115.50 | 122.10 | -6.60 |
| 10 | 82.145 | -41.254 | 6.3640 | 76.00 | 69.70 | 6.30 | 48 | 112.214 | -57.130 | 6.4945 | 110.00 | 116.50 | -6.50 |
| 11 ^a | 82.145 | -41.256 | 5.8535 | 83.00 | 55.25 | 27.75 | 49 | 112.214 | -57.154 | 6.2545 | 104.50 | 108.90 | -4.40 |
| 12 | 82.145 | -41.333 | 6.2005 | 60.50 | 62.47 | -1.97 | 50 | 112.214 | -57.167 | 6.2270 | 100.50 | 107.70 | -7.20 |
| 13 ^a | 100.203 | -51.507 | 6.7865 | 98.50 | 83.61 | 14.89 | 51 | 112.214 | -57.200 | 6.7345 | 123.00 | 120.90 | 2.10 |
| 14 | 100.203 | -51.510 | 6.8225 | 90.00 | 84.54 | 5.46 | 52 | 112.214 | -57.205 | 6.7125 | 119.00 | 120.10 | -1.10 |
| 15 | 100.203 | -51.512 | 6.8810 | 80.50 | 86.10 | -5.60 | 53 | 112.214 | -57.233 | 6.7815 | 131.00 | 121.10 | 9.90 |
| 16 | 100.203 | -51.511 | 6.8830 | 89.80 | 86.20 | 3.60 | 54 | 112.214 | -57.235 | 6.7885 | 126.40 | 121.30 | 5.10 |
| 17 | 100.203 | -51.514 | 6.8625 | 80.90 | 85.51 | -4.61 | 55 | 112.214 | -57.238 | 6.8055 | 115.00 | 121.60 | -6.60 |
| 18 | 98.188 | -49.960 | 6.6460 | 98.00 | 92.81 | 5.19 | 56 | 112.214 | -57.238 | 6.7890 | 121.50 | 121.20 | 0.30 |
| 19 | 98.188 | -49.973 | 6.5550 | 90.00 | 89.81 | 0.19 | 57 | 112.214 | -57.241 | 6.7860 | 114.00 | 121.00 | -7.00 |
| 20 | 98.188 | -49.975 | 6.5080 | 84.90 | 88.42 | -3.52 | 58 | 112.214 | -57.247 | 6.7475 | 131.80 | 119.70 | 12.10 |
| 21 | 98.188 | -49.972 | 6.4805 | 88.60 | 87.75 | 0.85 | 59 | 112.214 | -57.253 | 6.7720 | 126.60 | 120.20 | 6.40 |
| 22 | 98.188 | -49.975 | 6.5340 | 81.50 | 89.14 | -7.64 | 60 | 112.214 | -57.248 | 6.7305 | 119.50 | 119.20 | 0.30 |
| 23 | 98.188 | -49.988 | 6.3860 | 85.20 | 84.55 | 0.65 | 61 | 110.199 | -55.567 | 6.5080 | 129.00 | 130.50 | -1.50 |
| 24 | 98.188 | -50.000 | 6.3165 | 78.00 | 82.20 | -4.20 | 62 | 110.199 | -55.771 | 6.7065 | 137.00 | 129.40 | 7.60 |
| 25 | 98.188 | -50.047 | 6.7620 | 92.70 | 93.18 | -0.48 | 63 | 110.199 | -55.702 | 6.5540 | 141.00 | 127.30 | 13.70 |
| 26 | 98.188 | -50.051 | 6.7650 | 89.50 | 93.13 | -3.63 | 64 | 110.199 | -55.772 | 6.7575 | 125.00 | 130.70 | -5.70 |
| 27 | 98.188 | -50.082 | 6.8145 | 91.30 | 93.51 | -2.21 | 65 | 110.199 | -55.687 | 6.3685 | 130.50 | 122.60 | 7.90 |
| 28 | 98.188 | -50.082 | 6.8285 | 95.60 | 93.91 | 1.69 | 66 | 110.199 | -55.783 | 6.7595 | 117.00 | 130.40 | -13.40 |
| 29 ^a | 98.188 | -50.083 | 6.8380 | 118.40 | 94.14 | 24.26 | 67 | 110.199 | -55.714 | 6.4110 | 125.00 | 122.90 | 2.10 |
| 30 | 96.172 | -48.412 | 6.5305 | 102.00 | 102.70 | -0.70 | 68 | 110.199 | -55.689 | 6.5605 | 115.00 | 128.00 | -13.00 |
| 31 | 96.172 | -48.527 | 6.4030 | 110.50 | 95.32 | 15.18 | 69 | 110.199 | -55.538 | 5.9395 | 104.00 | 115.50 | -11.50 |
| 32 | 96.172 | -48.534 | 6.5255 | 100.00 | 98.55 | 1.45 | 70 | 110.199 | -55.580 | 5.5905 | 105.00 | 104.20 | 0.80 |
| 33 | 96.172 | -48.544 | 6.4395 | 103.00 | 95.79 | 7.21 | 71 | 108.183 | -54.171 | 6.3855 | 142.00 | 135.20 | 6.80 |
| 34 | 96.172 | -48.550 | 6.3660 | 92.00 | 93.52 | -1.52 | 72 | 108.183 | -54.204 | 6.4970 | 136.00 | 137.20 | -1.20 |
| 35 | 94.156 | -46.985 | 6.3545 | 105.00 | 106.90 | -1.90 | 73 | 110.199 | -55.774 | 6.7835 | 120.50 | 131.40 | -10.90 |
| 36 | 114.230 | -58.664 | 6.7780 | 117.60 | 111.70 | 5.90 | 74 | 98.188 | -50.093 | 6.8020 | 101.00 | 92.77 | 8.23 |
| 37 | 114.230 | -58.663 | 6.7825 | 118.90 | 111.90 | 7.00 | 75 | 114.230 | -58.666 | 6.8455 | 109.80 | 113.60 | -3.80 |
| 38 | 114.230 | -58.655 | 6.7705 | 118.50 | 111.80 | 6.70 | | | | | | | |

M_w is the molecular weight, E_T is the total energy, η is the chemical hardness, BP_{Obs} is the observed boiling point in centigrade and BP_{Pred} is the predicted boiling point with the help of the PM5 method. ^adata points are not included in deriving regression equation. Residual is the difference between observed and predicted boiling point.

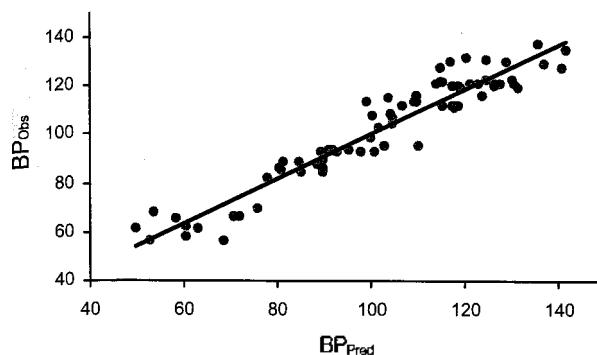


Figure 3. The trend of observed and predicted boiling points using PM5 based model

$$\text{B. P. PM5} = 18.9745 M_w + 33.2244 E_T + 28.1835 \eta - 297.672$$

$$r_{cv}^2 = 0.905, r^2 = 0.911, \text{SE} = 7.09, \text{Degree of freedom} = 0.90$$

$$(13)$$

The fourth QSPR model has been developed on the basis of descriptor values derived from DFT calculation using the B88-PW91 method with the DZVP basis set. In this model we have generated various equations by employing descriptors as independent variables and the best fitted equation is equation-14. The predicted boiling point (BP_{Pred}) from equation-14 is reported in Table-5. The correlation coefficient r^2 is 0.941, and the cross validation coefficient r_{cv}^2 is 0.938. Here compounds 11, 29 and 63 are outliers and the descriptor values of these compounds are not included in deriving

Table 5. The DFT based global descriptors and observed & predicted boiling points

| No. | Mw | E _T | η | BP _{Obs} | BP _{Pred} | Residual | No. | Mw | E _T | η | BP _{Obs} | BP _{Pred} | Residual |
|-----------------|---------|----------------|--------|-------------------|--------------------|----------|-----------------|---------|----------------|--------|-------------------|--------------------|----------|
| 1 | 86.177 | -237.076 | 4.6055 | 68.70 | 64.89 | 3.81 | 39 | 114.23 | -315.692 | 4.3280 | 109.40 | 113.22 | -3.82 |
| 2 | 86.177 | -237.074 | 4.5170 | 60.30 | 62.22 | -1.92 | 40 | 114.23 | -315.697 | 4.2850 | 106.80 | 111.94 | -5.14 |
| 3 | 86.177 | -237.073 | 4.3380 | 49.70 | 56.84 | -7.14 | 41 | 114.23 | -315.688 | 4.3570 | 115.60 | 114.07 | 1.53 |
| 4 | 84.161 | -235.832 | 4.0740 | 58.30 | 60.64 | -2.34 | 42 | 114.23 | -315.693 | 4.2145 | 99.20 | 109.81 | -10.61 |
| 5 | 84.161 | -235.835 | 4.0725 | 63.00 | 60.61 | 2.39 | 43 | 114.23 | -315.686 | 4.1730 | 118.20 | 108.54 | 9.66 |
| 6 | 84.161 | -235.838 | 3.9240 | 52.60 | 56.16 | -3.56 | 44 | 112.214 | -314.458 | 4.1645 | 128.00 | 120.06 | 7.94 |
| 7 | 84.161 | -235.836 | 4.2505 | 70.70 | 65.96 | 4.74 | 45 | 112.214 | -314.453 | 4.0275 | 117.70 | 115.92 | 1.78 |
| 8 | 84.161 | -235.838 | 4.1530 | 53.60 | 63.04 | -9.44 | 46 | 112.214 | -314.461 | 4.0760 | 124.00 | 117.41 | 6.59 |
| 9 | 84.161 | -235.865 | 4.4700 | 71.80 | 72.66 | -0.86 | 47 | 112.214 | -314.454 | 4.1225 | 115.50 | 118.78 | -3.28 |
| 10 | 82.145 | -234.593 | 3.8230 | 76.00 | 64.84 | 11.16 | 48 | 112.214 | -314.458 | 3.9145 | 110.00 | 112.55 | -2.55 |
| 11 ^a | 82.145 | -234.535 | 3.5455 | 83.00 | 56.29 | 26.71 | 49 | 112.214 | -314.458 | 3.7210 | 104.50 | 106.73 | -2.23 |
| 12 | 82.145 | -234.599 | 3.8545 | 60.50 | 65.81 | -5.31 | 50 | 112.214 | -314.459 | 3.6580 | 100.50 | 104.84 | -4.34 |
| 13 | 100.203 | -276.387 | 4.5380 | 98.50 | 91.20 | 7.30 | 51 | 112.214 | -314.458 | 4.1740 | 123.00 | 120.34 | 2.66 |
| 14 | 100.203 | -276.386 | 4.4550 | 90.00 | 88.71 | 1.29 | 52 | 112.214 | -314.462 | 4.2120 | 119.00 | 121.50 | -2.50 |
| 15 | 100.203 | -276.385 | 4.3675 | 80.50 | 86.07 | -5.57 | 53 | 112.214 | -314.488 | 4.3885 | 131.00 | 126.90 | 4.10 |
| 16 | 100.203 | -276.382 | 4.3040 | 89.80 | 84.16 | 5.64 | 54 | 112.214 | -314.487 | 4.3735 | 126.40 | 126.44 | -0.04 |
| 17 | 100.203 | -276.381 | 4.2320 | 80.90 | 81.99 | -1.09 | 55 | 112.214 | -314.491 | 4.3535 | 115.00 | 125.86 | -10.86 |
| 18 | 98.188 | -275.146 | 4.1900 | 98.00 | 92.48 | 5.52 | 56 | 112.214 | -314.485 | 4.1925 | 121.50 | 121.00 | 0.50 |
| 19 | 98.188 | -275.146 | 4.0770 | 90.00 | 89.08 | 0.92 | 57 | 112.214 | -314.487 | 4.1260 | 114.00 | 119.01 | -5.01 |
| 20 | 98.188 | -275.146 | 3.9665 | 84.90 | 85.76 | -0.86 | 58 | 112.214 | -314.496 | 4.2635 | 131.80 | 123.17 | 8.63 |
| 21 | 98.188 | -275.142 | 3.9460 | 88.60 | 85.13 | 3.47 | 59 | 112.214 | -314.494 | 4.1130 | 126.60 | 118.64 | 7.96 |
| 22 | 98.188 | -275.142 | 3.8965 | 81.50 | 83.65 | -2.15 | 60 | 112.214 | -314.496 | 4.2835 | 119.50 | 123.77 | -4.27 |
| 23 | 98.188 | -275.148 | 3.8450 | 85.20 | 82.12 | 3.08 | 61 | 110.199 | -313.217 | 4.1015 | 129.00 | 129.90 | -0.90 |
| 24 | 98.188 | -275.149 | 3.8575 | 78.00 | 82.50 | -4.50 | 62 | 110.199 | -313.270 | 4.2935 | 137.00 | 135.85 | 1.15 |
| 25 | 98.188 | -275.148 | 4.1795 | 92.70 | 92.17 | 0.53 | 63 ^a | 110.199 | -313.246 | 3.8520 | 141.00 | 122.50 | 18.50 |
| 26 | 98.188 | -275.150 | 4.1150 | 89.50 | 90.24 | -0.74 | 64 | 110.199 | -313.273 | 4.0800 | 125.00 | 129.45 | -4.45 |
| 27 | 98.188 | -275.178 | 4.3790 | 91.30 | 98.27 | -6.97 | 65 | 110.199 | -313.223 | 3.9635 | 130.50 | 125.77 | 4.73 |
| 28 | 98.188 | -275.178 | 4.3660 | 95.60 | 97.88 | -2.28 | 66 | 110.199 | -313.278 | 4.0610 | 117.00 | 128.90 | -11.90 |
| 29 ^a | 98.188 | -275.173 | 4.3060 | 118.40 | 96.06 | 22.34 | 67 | 110.199 | -313.250 | 3.7600 | 125.00 | 119.75 | 5.25 |
| 30 | 96.172 | -273.904 | 4.0795 | 102.00 | 100.89 | 1.11 | 68 | 110.199 | -313.248 | 3.8835 | 115.00 | 123.46 | -8.46 |
| 31 | 96.172 | -273.911 | 4.0190 | 110.50 | 99.09 | 11.41 | 69 | 110.199 | -313.196 | 3.2065 | 104.00 | 102.93 | 1.07 |
| 32 | 96.172 | -273.941 | 3.9860 | 100.00 | 98.21 | 1.79 | 70 | 110.199 | -313.212 | 3.4045 | 105.00 | 108.94 | -3.94 |
| 33 | 96.172 | -273.943 | 4.0245 | 103.00 | 99.37 | 3.63 | 71 | 108.183 | -312.010 | 3.6715 | 142.00 | 128.83 | 13.17 |
| 34 | 96.172 | -273.944 | 3.8825 | 92.00 | 95.11 | -3.11 | 72 | 108.183 | -312.032 | 3.9500 | 136.00 | 137.28 | -1.28 |
| 35 | 94.156 | -272.703 | 4.0490 | 105.00 | 111.84 | -6.84 | 73 | 110.199 | -313.274 | 4.0925 | 120.50 | 129.83 | -9.33 |
| 36 | 114.23 | -315.698 | 4.4135 | 117.60 | 115.81 | 1.79 | 74 | 98.188 | -275.185 | 4.2925 | 101.00 | 95.70 | 5.30 |
| 37 | 114.23 | -315.696 | 4.3810 | 118.90 | 114.82 | 4.08 | 75 | 114.23 | -315.690 | 4.2075 | 109.80 | 109.59 | 0.21 |
| 38 | 114.23 | -315.692 | 4.3820 | 118.50 | 114.84 | 3.66 | | | | | | | |

M_w is the molecular weight, E_T is the total energy, η is the chemical hardness, BP_{Obs} is the observed boiling point in centigrade and BP_{Pred} is the predicted boiling point with the help of the DFT method. ^adata points are not included in deriving regression equation. Residual is the difference between observed and predicted boiling point.

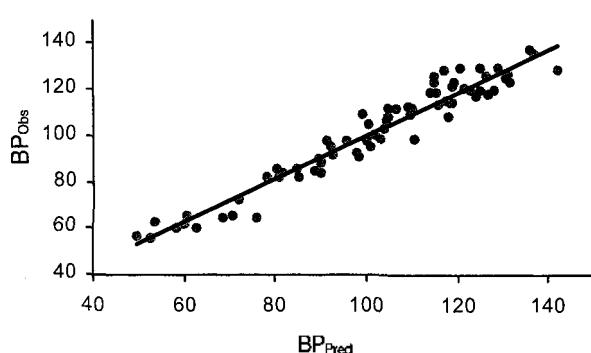


Figure 4. The trend of observed and predicted boiling points using DFT based model

regression equation. The Plot of experimental vs. predicted boiling point values for this model is given in Figure 4.

$$\text{B.P.DFT} = -8.02625 \text{M}_w - 3.58485 \text{E}_T + 30.045 \eta - 231.69$$

$$r_{cv}^2 = 0.938, r^2 = 0.941, \text{SE} = 5.6, \text{Degree of freedom} = 0.93$$

$$(14)$$

The above discussion indicates that the DFT method is the more reliable than semiempirical methods for the prediction of boiling point of alkanes which is in accordance with our expectations. Although the statistical quality of DFT method is very good but the absolute values of the predicted boiling point is a bit different. To improve the absolute values of the boiling point as well as the statistical quality we have calcu-

Table 6. The DFT based local & global descriptors and observed & predicted boiling points

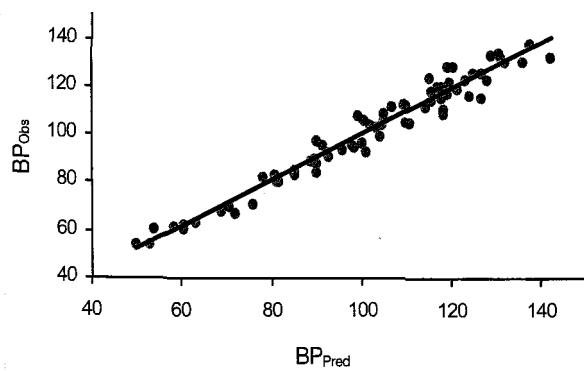
| No. | Site | E_n^{\ddagger} | Mw | Et | η | BP _{Obs} | BP _{Pred} | Residual |
|-----------------|------|------------------|---------|----------|--------|-------------------|--------------------|----------|
| 1 | 6 | 160.8562 | 86.177 | -237.076 | 4.6055 | 68.70 | 68.24 | 0.46 |
| 2 | 1 | 174.0529 | 86.177 | -237.074 | 4.5170 | 60.30 | 60.40 | -0.10 |
| 3 | 6 | 177.2726 | 86.177 | -237.073 | 4.3380 | 49.70 | 54.40 | -4.70 |
| 4 | 2 | 168.8818 | 84.161 | -235.832 | 4.0740 | 58.30 | 62.05 | -3.75 |
| 5 | 4 | 164.9671 | 84.161 | -235.835 | 4.0725 | 63.00 | 63.67 | -0.67 |
| 6 | 3 | 178.1847 | 84.161 | -235.838 | 3.9240 | 52.60 | 54.28 | -1.68 |
| 7 | 6 | 159.8139 | 84.161 | -235.836 | 4.2505 | 70.70 | 70.45 | 0.25 |
| 8 | 5 | 177.3055 | 84.161 | -235.838 | 4.1530 | 53.60 | 60.58 | -6.98 |
| 9 | 6 | 181.4787 | 84.161 | -235.865 | 4.4700 | 71.80 | 67.12 | 4.68 |
| 10 | 5 | 157.5123 | 82.145 | -234.593 | 3.8230 | 76.00 | 71.30 | 4.70 |
| 11 ^a | 3 | 144.8478 | 82.145 | -234.535 | 3.5455 | 83.00 | 69.24 | 13.77 |
| 12 | 6 | 180.2796 | 82.145 | -234.599 | 3.8545 | 60.50 | 62.56 | -2.06 |
| 13 | 7 | 162.8379 | 100.203 | -276.387 | 4.5380 | 98.50 | 94.21 | 4.29 |
| 14 | 1 | 172.9725 | 100.203 | -276.386 | 4.4550 | 90.00 | 87.79 | 2.21 |
| 15 | 5 | 179.4718 | 100.203 | -276.385 | 4.3675 | 80.50 | 82.79 | -2.29 |
| 16 | 6 | 173.0481 | 100.203 | -276.382 | 4.3040 | 89.80 | 83.84 | 5.96 |
| 17 | 5 | 175.7504 | 100.203 | -276.381 | 4.2320 | 80.90 | 80.83 | 0.07 |
| 18 | 1 | 164.0661 | 98.188 | -275.146 | 4.1900 | 98.00 | 95.63 | 2.37 |
| 19 | 4 | 152.6404 | 98.188 | -275.146 | 4.0770 | 90.00 | 97.51 | -7.51 |
| 20 | 7 | 175.7985 | 98.188 | -275.146 | 3.9665 | 84.90 | 84.91 | -0.01 |
| 21 | 2 | 165.0029 | 98.188 | -275.142 | 3.9460 | 88.60 | 88.90 | -0.30 |
| 22 | 5 | 181.0449 | 98.188 | -275.142 | 3.8965 | 81.50 | 80.87 | 0.63 |
| 23 | 2 | 172.1470 | 98.188 | -275.148 | 3.8450 | 85.20 | 83.30 | 1.90 |
| 24 | 5 | 174.8789 | 98.188 | -275.149 | 3.8575 | 78.00 | 82.48 | -4.48 |
| 25 | 7 | 175.2970 | 98.188 | -275.148 | 4.1795 | 92.70 | 90.64 | 2.06 |
| 26 | 7 | 172.4479 | 98.188 | -275.150 | 4.1150 | 89.50 | 90.17 | -0.67 |
| 27 | 6 | 175.7110 | 98.188 | -275.178 | 4.3790 | 91.30 | 95.74 | -4.44 |
| 28 | 6 | 180.2740 | 98.188 | -275.178 | 4.3660 | 95.60 | 93.48 | 2.12 |
| 29 | 4 | 135.1205 | 98.188 | -275.173 | 4.3060 | 118.40 | 110.90 | 7.51 |
| 30 | 6 | 162.8398 | 96.172 | -273.904 | 4.0795 | 102.00 | 104.24 | -2.24 |
| 31 | 5 | 157.9727 | 96.172 | -273.911 | 4.0190 | 110.50 | 104.74 | 5.76 |
| 32 | 6 | 175.0174 | 96.172 | -273.941 | 3.9860 | 100.00 | 96.82 | 3.18 |
| 33 | 7 | 162.8846 | 96.172 | -273.943 | 4.0245 | 103.00 | 102.93 | 0.07 |
| 34 | 6 | 177.8814 | 96.172 | -273.944 | 3.8825 | 92.00 | 92.95 | -0.95 |
| 35 | 6 | 177.0343 | 94.156 | -272.703 | 4.0490 | 105.00 | 108.57 | -3.57 |
| 36 | 8 | 172.6029 | 114.230 | -315.698 | 4.4135 | 117.60 | 115.41 | 2.19 |
| 37 | 1 | 165.9926 | 114.230 | -315.696 | 4.3810 | 118.90 | 117.34 | 1.56 |
| 38 | 8 | 161.3686 | 114.230 | -315.692 | 4.3820 | 118.50 | 119.30 | -0.80 |

E_n^{\ddagger} is the highest Klopman atomic softness value, M_w is the molecular weight, E_T is the total energy, η is the chemical hardness, BP_{Obs} is the observed boiling point in centigrade and BP_{Pred} is the predicted boiling point from the DFT_{Local} (DFT_{Local} is the addition of E_n^{\ddagger} values in DFT model) method.

^aData points are not included in deriving regression equation. Residual is the difference between observed and predicted boiling point.

Table 6. Continued

| No. | Site | E_n^\ddagger | Mw | E_T | η | BP _{Obs} | BP _{Pred} | Residual |
|-----------------|------|----------------|---------|----------|--------|-------------------|--------------------|----------|
| 39 | 3 | 173.6211 | 114.230 | -315.692 | 4.3280 | 109.40 | 112.75 | -3.35 |
| 40 | 7 | 174.3305 | 114.230 | -315.697 | 4.2850 | 106.80 | 111.36 | -4.56 |
| 41 | 6 | 170.7109 | 114.230 | -315.688 | 4.3570 | 115.60 | 114.71 | 0.89 |
| 42 | 1 | 178.5331 | 114.230 | -315.693 | 4.2145 | 99.20 | 107.75 | -8.55 |
| 43 | 6 | 173.7142 | 114.230 | -315.686 | 4.1730 | 118.20 | 108.68 | 9.52 |
| 44 | 1 | 165.7014 | 112.214 | -314.458 | 4.1645 | 128.00 | 122.83 | 5.17 |
| 45 | 7 | 163.3517 | 112.214 | -314.453 | 4.0275 | 117.70 | 120.25 | -2.55 |
| 46 | 2 | 175.3007 | 112.214 | -314.461 | 4.0760 | 124.00 | 116.51 | 7.49 |
| 47 | 2 | 175.3899 | 112.214 | -314.454 | 4.1225 | 115.50 | 117.65 | -2.15 |
| 48 | 7 | 175.1585 | 112.214 | -314.458 | 3.9145 | 110.00 | 112.38 | -2.38 |
| 49 | 8 | 184.3572 | 112.214 | -314.458 | 3.7210 | 104.50 | 103.50 | 1.00 |
| 50 | 6 | 174.5292 | 112.214 | -314.459 | 3.6580 | 100.50 | 106.00 | -5.50 |
| 51 | 8 | 167.4685 | 112.214 | -314.458 | 4.1740 | 123.00 | 122.33 | 0.67 |
| 52 | 6 | 155.4407 | 112.214 | -314.462 | 4.2120 | 119.00 | 128.39 | -9.38 |
| 53 | 6 | 156.5930 | 112.214 | -314.488 | 4.3885 | 131.00 | 132.56 | -1.56 |
| 54 | 7 | 171.5713 | 112.214 | -314.487 | 4.3735 | 126.40 | 125.87 | 0.53 |
| 55 | 7 | 175.7776 | 112.214 | -314.491 | 4.3535 | 115.00 | 123.60 | -8.60 |
| 56 | 6 | 175.7491 | 112.214 | -314.485 | 4.1925 | 121.50 | 119.42 | 2.08 |
| 57 | 6 | 190.1808 | 112.214 | -314.487 | 4.1260 | 114.00 | 111.64 | 2.36 |
| 58 | 8 | 155.3382 | 112.214 | -314.496 | 4.2635 | 131.80 | 129.88 | 1.92 |
| 59 | 7 | 180.6932 | 112.214 | -314.494 | 4.1130 | 126.60 | 115.31 | 11.29 |
| 60 | 8 | 176.4311 | 112.214 | -314.496 | 4.2835 | 119.50 | 121.53 | -2.03 |
| 61 | 8 | 164.1046 | 110.199 | -313.217 | 4.1015 | 129.00 | 132.82 | -3.82 |
| 62 | 8 | 164.4965 | 110.199 | -313.270 | 4.2935 | 137.00 | 137.81 | -0.81 |
| 63 ^a | 8 | 190.0903 | 110.199 | -313.246 | 3.8520 | 141.00 | 115.53 | 25.47 |
| 64 | 7 | 179.6043 | 110.199 | -313.273 | 4.0800 | 125.00 | 125.93 | -0.93 |
| 65 | 7 | 153.7925 | 110.199 | -313.223 | 3.9635 | 130.50 | 133.60 | -3.10 |
| 66 | 7 | 192.7253 | 110.199 | -313.278 | 4.0610 | 117.00 | 119.94 | -2.94 |
| 67 ^a | 8 | 193.0943 | 110.199 | -313.250 | 3.7600 | 125.00 | 111.90 | 13.11 |
| 68 | 7 | 171.7252 | 110.199 | -313.248 | 3.8835 | 115.00 | 124.07 | -9.07 |
| 69 | 5 | 187.9669 | 110.199 | -313.196 | 3.2065 | 104.00 | 99.53 | 4.47 |
| 70 | 7 | 184.6418 | 110.199 | -313.212 | 3.4045 | 105.00 | 106.11 | -1.11 |
| 71 | 8 | 164.8661 | 108.183 | -312.010 | 3.6715 | 142.00 | 132.43 | 9.57 |
| 72 | 7 | 187.8743 | 108.183 | -312.032 | 3.9500 | 136.00 | 130.05 | 5.95 |
| 73 | 8 | 174.7390 | 110.199 | -313.274 | 4.0925 | 120.50 | 128.31 | -7.81 |
| 74 | 7 | 176.9594 | 98.188 | -275.185 | 4.2925 | 101.00 | 92.99 | 8.01 |
| 75 | 1 | 183.8653 | 114.230 | -315.690 | 4.2075 | 109.80 | 105.32 | 4.49 |

Figure 5. The trend of observed and predicted boiling points using DFT_{Local} based model

lated Klopman atomic softness values at all the atoms of all the alkanes and selected the highest E_n^\ddagger value. The MLR analysis with this highest E_n^\ddagger values in combination with the descriptors of DFT model (molecular weight, total energy and chemical hardness) provides most valuable QSPR model for the prediction of boiling point of alkanes. We called this model DFT_{Local} model. The regression equation for this model is equation-15 and the predicted values are given in Table-6. In this model the correlation coefficient r^2 is 0.959 and the cross validation coefficient r_{cv}^2 is 0.954. Here compounds 11, 63 and 67 are outliers and the descriptor values of these compounds are not included in deriving regression equation. The Plot of experimental vs. predicted boiling point values for this model is given in Figure 5.

$$\begin{aligned} \text{B. P. DFT}_{\text{Local}} = & -0.420475 E_n^{\ddagger} - 7.53796 M_w - 3.41562 E_T \\ & + 25.8986 \eta - 143.56 \\ r_{cv}^2 = 0.954, r^2 = 0.959, \text{SE} = 4.7, \text{Degree of freedom} = 0.96 \end{aligned} \quad (15)$$

The correlation coefficient (r^2), cross validation coefficient (r_{cv}^2) and standard error (SE) values for all the models are as follows.

| Method | r^2 | r_{cv}^2 | SE |
|----------------------|-------|------------|-----|
| AM1 | 0.891 | 0.885 | 7.9 |
| PM3 | 0.910 | 0.904 | 7.5 |
| PM5 | 0.911 | 0.905 | 7.1 |
| DFT | 0.941 | 0.938 | 5.6 |
| DFT _{Local} | 0.959 | 0.954 | 4.7 |

Conclusion

In this contribution the calculation of semiempirical and DFT based descriptors is carried out and the regression models have been generated for the determination of boiling point of a series of alkanes. The comparison of all the models indicates that the DFT model is more reliable than others and has high predictive power. The addition of Klopman atomic softness in DFT model improves the result of the model and makes it more reliable and important for the prediction of the boiling point of alkanes.

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