UHF 기술을 이용한 온라인 부분방전 모니터링

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On-line Insulation Diagnostic by PD Monitoring Field Practical of UHF Technique for On-line PD Monitoring

吳 鏞*·崔 龍 成[†]·黃 宗 善**·李 炅 燮*** (Yong Oh·Yong-Sung Choi·Jong-Sun Hwang·Kyung-Sup Lee)

Abstract - A field-oriented UHF system for on-line PD monitoring of transformers is designed, which has been installed inside the oil tank of transformer in a substation by two ways: on-line installing mode through the oil-valve and pre-installing mode through the man hole/hand hole cover. This system has successfully captured long intermittent discharge signals that hadn't been detected through conventional techniques, and solved the problem successfully. The results demonstrate that UHF technique has great advantages for on-line PD monitoring of transformers. By adopting the peak detection technique, it becomes easy and effective for the transplantation of the phase-resolved pattern recognition technique from conventional method to UHF method, and then to realize continuous on-line monitoring, source characterization and trending analysis.

Key Words: Power Transformer, On-line Monitoring, Partial Discharge, UHF; Field Test

1. Introduction

As a new partial discharge detecting method, UHF technique has been developed rapidly since 1980s. Because the wave-guide structure of GIS, which is extremely appropriate for the propagation of UHF signals, the application of UHF PD detecting technique on GIS has become great successful, and its on-line sensitivity can reach 1 pC. In the UK, diagnostic couplers are specified for all new GIS, and UHF techniques are used extensively in factory testing, site commissioning and during the service life of the GIS. So far, UHF technique has been applied in the PD detection of many power equipment, such as cable, generator and transformer, etc[1].

The studies of UHF partial discharge detection technique mainly concentrate on the following aspects: sensor design, optimization and calibration [2-6], UHF radiation and propagation mechanism, PD source characterization and fault location[7-8]. In addition, some researchers use UHF method as an anti-interference tool for the conventional technique. Of course, most of the researches are specially developed for GIS, but as a

matter of fact, many of the above techniques can be used to transformers. In 1996, Rutgers firstly explored the feasibility of using UHF technique in transformers[9].

After that, many people made deep researches into this project, and good results is obtained both in laboratory and field practices [10-14]. As for practical use, phase-resolved pattern recognition and trending analysis are the most useful tools for UHF method, just as it is for traditional technique. But because the original UHF signal is very fast, only lasts for the magnitude of nano seconds, it is extremely hard to correlate it with power cycle. At present, people mostly fulfill this function by using the POW mode of the spectrum analyzer, but it's a rather luxury approach and inconvenient at the same time. The peak detection technique is very effective to condition the UHF signal and can accomplish the same function as SA quite easily.

This paper adopts the peak detection technique in the field-oriented UHF on-line PD monitoring system of transformers, then the two practical working instances are introduced in detail, the results indicate the effectiveness of the UHF technique and its superiority over conventional methods.

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2. Experimental

2.1 The configuration of the system

The system includes two main parts: the stationary

교신저자, 正會員: 東新大學校 電氣工學科 教授・工博 E-mail: yschoi67@dsu.ac.kr

^{*} 正 會 員:東新大學校 電氣電子工學科 博士課程

^{**} 正 會 員:全南道立大學 컴퓨터應用電氣科 教授・工博

^{**} 正 會 員:東新大學校 電氣工學科 教授・工博

continuous-working equipment that deals with the UHF peak detection signals, and the movable instrument that analyzes the original UHF signals in time domain as well as frequency domain. The stationary equipment is a self-developed industrial PC system, which is made up of a fast DAQ card and real-time analyzing software. While the movable part is a high quality digital oscilloscope that works in "plug and play" mode. Fig.1 shows the diagram of the system configuration.

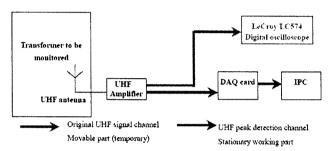


Fig. 1 Block diagram for field UHF PD on-line monitoring system.

2.2 Hardware Components of The System

The hardware components mainly consist of UHF sensor, UWB amplifier with peak detection module, RG142/U cables, high-speed DAQ card, IPC and digital oscilloscope, the bandwidth ranges from 400M~1500M Hz. UHF sensor is a self-compensative Archimedes antenna fed by a 50Ω coaxial cable, which is matched through a 4:1 wide band ferrite-core transformer. Figure 2 shows the SWR property of the UHF sensor. The gain of the amplifier is 40dB with the same working frequency band, and there're two channels output, one is the original UHF signal and the other is the UHF peak detection signal. The function of DAQ card is to sample the UHF peak detection and the reference phase signal with the max sampling rate 20MS/s per channel. The is LeCroy 574A model single-shot sampling rate and 1GHz analog bandwidth, which is used to process the original UHF signal.

2.3 The UHF Peak Detection Technique

Usually in the practices of UHF, the phase information of the PD is obtained by using a SA that is set to POW mode. When considers the cost factors and the convenience reasons, the SA does not suitable to be used as a component of the stationary equipment, so the peak detection technique is adopted to condition the original UHF signals, which not only maintains the phase and magnitude info, but also lower the requirements for the digital sampling rate greatly. By doing this, the cost of the device is reduced to the maximum extent, and the traditional phase–resolved pattern recognition technique can then be transplanted to the UHF method.

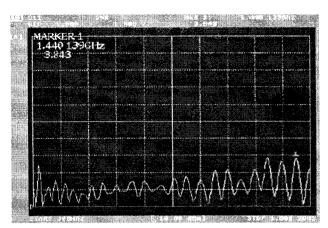


Fig. 2 The SWR attributes of the UHF sensor.

2.4 Main Functions of the System

The two parts of the system work independently. The stationary device will be installed on the equipment during its service life, and its main functions are: continuously monitoring the target, then decide whether there're PD or not; making phase-resolved statistical analysis of the UHF peak detection signals to plot charts, which is to make source characterization; recording important PD parameters and making trending analysis. The stationary part provides reserved port for the movable device to be connected in. A high-speed oscilloscope is used temporarily to make frequency domain analysis of the original UHF signals, which includes making pattern recognition by the UHF spectra and estimate the approximate time-flight information from different sensors, but these kind of work has be done by qualified researchers at present.

2.5 Installing Modes

According to the different installing modes of the sensors, two implementing schema of the system are designed. One way is on-line installation by inserting the sensor into transformer tank through the oil valve, this is the "plug and play" mode; the other way is by pre-installing the sensor onto the manhole or hand hole cover, which must be carry on before the oiling of the transformer, in this way the sensor will be as a part of the cover and will work with the transformer permanently after installation. Special oil-proof design is required for both of these two ways, so as to guarantee the safety service of the transformer; besides, it's necessary to increase the sensitivity of the sensor while installation requirement is satisfied.

3. Results and Discussion

3.1 Anti-interference Measures

The background noises level inside the oil tank is very low (about 25mV), which is about two times lower than

the outer environment (about 50mV). A stable and continual signal was found and recorded by the oscilloscope, see Figure 3. In order to find out its source, several layers of aluminum foil was wrapped onto the apertures at where the flange joints and all the signal lines were screened by a soft spiral iron pipe, which intention is to ensure good screening of the whole measuring system. After convinced that the interferences could be totally removed by the screening, we found that the signal still exists, then the sensor was withdrawn out of the transformer, still the signal existed, so we concluded that the signals are interferences brought about by the switched power of the amplifier.

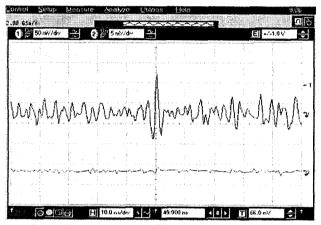


Fig. 3 Typical noise signal from the power system.

During the period of monitoring, three intensive signals were captured by the measuring system. The amplitudes of the signals were about 400mV, which were much higher than that of the background noises (see Figure 4). When each signal was captured, the operations of the transformer tap changer could be excluded definitely. The time intervals between two signals were seven hours approximately. The time domain waveform of the signals indicated that they were much likely to be discharges, but it was kept uncertain whether they were generated inside the transformer oil tank or other electrical equipments' operation coupled into the transformer from the power lines.

3.2 Site Testing Results

In the inspection period of the transformer, two types of sensors are designed and pre-installed permanently onto the oil tank, and all the wires and cables are screened with metal pipe. In the on site PD test before the transformer was put into service, we did experiments with both the UHF system and conventional PD method at the same time, and the current pulse signals and UHF signals were recorded synchronously for comparison studies. During the experiments the maximum UHF

signal was saved and set as the threshold of warning when the transformer was in the normal service state. The power spectrum of the UHF by FFT can be compared with those obtained in the laboratory, so as to get the source type information.

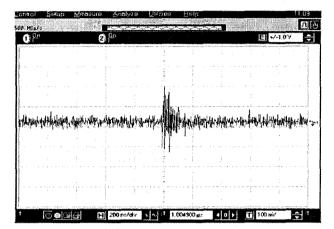


Fig. 4 A typical suspicious discharge signal.

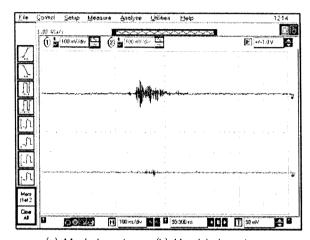
As in the conventional PD test, the procedure is to apply 1.3 times of normal voltage for 30 minutes to each phase one by one. The conventional results are shown in Table 1. The typical UHF PD signals of the R phase are shown in Figure 5. It shows that the background of the manhole antenna is about 30mV, while the PD signal is approximately 150mV. Besides, each time the waveform of the signal almost keeps the same, which indicate that it is a monotype discharge. The case of the hand hole antenna is analogous as the manhole antenna, but the signals are much smaller. Because the signals become steady and low in a few minutes, we conclude that it is gas cavity discharge in oil or corona discharges on small conductor burrs which soon be melted down by the PD energy. The results demonstrate that the sensitivity of the UHF system is high enough to detect very small discharges in transformers.

4. Conclusions

The practical applications in field demonstrate that the UHF technique is very effective for on-line monitoring. By putting the UHF sensor inside the transformer tank, both high sensitivity and anti-interference characteristics can be achieved at the same time, which are the most advantages of UHF over conventional methods. Peak detection technique makes it easier and cheaper for UHF method to import conventional phase-resolved pattern recognition technique and trending analysis, which makes it more practicable for on-line utilization of UHF technique.

Table	1	Apparent	discharges	recorded	with	conventional
		method.				

Apparent charge [pC]	Applied voltage [kV]	R phase	S phase	T phase
Maximum	189	2,000	800	1,200
Steady	189	100	130	110



(a) Manhole antenna(b) Hand hole antennaFig. 5 Typical PD signals from Manhole and hand hole antenna when the R phase is energized.

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References

- [1] Okubo H, Suzuki, "A Frequency component of current pulse waveform in partial discharge measurement", 9th ISH [C] Graz, August 25-29, 1995.
- [2] M.D. Judd, O. Farish, B.F. Hampton, "Broadband couplers for UHF detection of partial discharge in gas-insulated substations", IEE Proc. Sci. Meas. Technol., pp. 237-243, Vol.142, No.3 May 1995.
- [3] M.D. Judd, "Transient calibration of electric field sensors, Science, Measurement and Technology", IEE Proceedings, Volume: 146 Issue: 3, Page(s): 113, 116, May 1999.

- [4] M.D. Judd, O. Farish, "A pulsed GTEM system for UHF sensor calibration", IEEE Trans. Instrumentation and Measurement, Vol. 47, no. 4, pp.875-880, August 1998.
- [5] M.D. Judd, O. Farish, J.S. Pearson, "UHF couplers for gas-insulated substations: a calibration technique, Science, Measurement and Technology", IEE Proceedings, Volume: 144 Issue: 3, Page(s): 117 -122, May 1997.
- [6] M. Knapp, R. Feger, K. Feser, A. Breuer, "Application of the CIGRE-sensitivity verification for UHF PD detection in three-phase GIS, High Voltage Engineering Symposium", 22-27, Conference Publication No. 467, IEE, 1999.
- [7] L. Yang, M.D. Judd, "Propagation characteristics of UHF signals in transformers for locating partial discharge sources", Proc. 13th Int. Symposium on High Voltage Engineering (ISH), Delft, 2003.
- [8] A.R. Convery, M.D. Judd, "Measurement of Propagation characteristics for UHF signals in transformer insulation materials", Proc. 13th Int. Symposium on High Voltage Engineering (ISH), Delft, 2003.
- [9] W.R. Rutgers and Y.H. Fu, "UHF PD-Detection in a power transformer", 10th International Symposium on High Voltage Engineering, pp. 219–222, August 25–29, 1997.
- [10] M.D. Judd, O. Farish, and B.F. Hampton, "The Excitation of UHF signals by partial discharges in GIS", IEEE Trans. Dielect. Elect. Insulation, Vol.3, pp. 213-228, Apr. 1996.
- [11] Judd, M.D., Hampton, B.F., Farish, O., "Modeling partial discharge excitation of UHF signals inwaveguide structures using Green's functions", Science, Measurement and Technology, IEE Proceedings-, Volume: 143 Issue: 1, Page(s): 63 -70, Jan. 1996.
- [12] M.D. Judd, "Using finite difference time domain techniques to model electrical discharge phenomena", Electrical Insulation and Dielectric Phenomena, 2000 Annual Report Conference on, Volume: 2, Page(s): 622 -625 vol.2, Oct. 2000.
- [13] Xu Gaofeng et al, "A Calculational Method of transient electric field excited by partial discharge in gas insulated substation using Dyadic Green Function", Power System Technology, 2002. Proceedings. PowerCon 2002. International Conference on , Volume: 3, Page(s): 1438 -1441, vol.3, Oct. 2002.
- [14] Raja, K., Devaux, F., Lelaidier, S., "Recognition of discharge sources using UHF PD signatures", Electrical Insulation Magazine, IEEE, Volume: 18 Issue: 5, pp. 8 -14, Sept.-Oct. 2002.

저 자 소 개



최 용 성 (崔 龍 成)

1967년 11월 14일생. 1991년 동아대학교 전기공학과 졸업 (학사). 1993년 동 대학원 전기공학과 졸업 (석사). 1998년 동 대학원 전기공학과 졸업 (공박). 1999년~2001년 JAIST Post-Doc.. 2001년~2003년 Osaka Univ. Post-Doc.. 2002년~2005년 원광대학교 연구교수. 2006년~현재 동신대학교 전기공학과 교수. 2006년~현재 전력산업인력양성사업단 기획운영부장.

Tel: 061-330-3204 Fax: 061-330-3103

E-mail: yschoi67@dsu.ac.kr



황 종 선 (黃 宗 善)

1953년 12월 13일생. 1977년 2월 한양교 전기공학과 졸업(공학사). 1979년 동 대학원 졸업(석사). 1995년 전북대학교 전기공학과 졸업(박사). 1987-1998 한국원자력연구원 책임연구원. 1998~현재 전남도립대학 컴퓨터 응용전기과 교수. 2001~현재 한국 직업능력개발원 평가위원. 1999~2002 국제 기능올림픽 국제심사위원 Commercial Wiring Trade. 1998~2002 한국기능올림픽위원회옥내배선 전국대회 심사위원. 1999~2002한국산업단지공단 자문위원.

Tel: 061-380-8621 Fax: 061-380-8466

E-mail: hlepw@hanmail.net



오 용 (吳 鏞)

1964년 8월 2일생. 1987년 전남대학교 졸업 (학사). 1989년 동 대학원 졸업 (석사). 2007년~현재 동신대학교 대 학원 전기공학과 박사과정.

E-mail: hanelc@chol.com



이 경 섭 (李 炅 燮)

1956년 11월 09일생. 1983년 조선대학교 전기공학과 졸업(학사). 1986 동 대학원 전기공학과 졸업(석사). 1991년 동 대학원 전기공학과 졸업(공박). 1988년 ~ 현재 동신대학교 전기공학과 교수. 1994년 ~ 1995년 동경공업대학 객원연구원. 2006년 현재 전력산업인력양성사업단 단장.

Tel: 061-330-3203 Fax: 061-330-3103 E-mail: kslee@dsu.ac.kr