

Effect of Coiling Temperature on the Annealed Texture in Cu/Nb Added Ultra Low Carbon Steels

Yinghua Jiang[†], Young-Koo Park and Oh-Yeon Lee

Division of Advanced Materials Engineering, Chonbuk National University, South Korea

(Received December 5, 2007 : Accepted January 2, 2008)

Abstract The present work was performed to investigate the effect of coiling temperature on the annealed texture in Cu/Nb-added ultra-low-carbon steels. The ultra-low-carbon steels were coiled at 650 and 720°C, respectively. The result showed that the Cu-added ultra-low-carbon steel at a low coiling temperature produced a desirable annealed texture related to good formability. On the other hand, Nb-added ultra-low-carbon steel at a high coiling temperature also produced a desirable texture. This is attributed to the effect of Nb, which retards recrystallization during the coiling process.

Key words microstructure, texture, Cu/Nb added ultra low carbon steel, coiling temperature.

1. Introduction

Recently, the newly developed ultra low carbon steel is expected to be applied in a wide range of automotive parts and applications more excellent formability.¹⁾ The formability is closely related to the texture of the steel ultra low carbon steel sheet. Recently, a lot of attention was focused on the improvement of the final product texture through proper control of the processing parameters: heating temperature, coiling temperature, cold reduction, annealing temperature.²⁾ Among these, this study investigated the effect of coiling temperature on the annealed texture in Cu/Nb added ultra low carbon steels. In this paper, the two annealed ultra low carbon steels were investigated. One was based on Cu and the other was based on Nb. The Nb-added ultra low carbon steel has good formability and non-aging feature 3). However the availability of Nb was restricted by its price and weldability effect. But for Cu-added ultra low carbon steel, C content was controlled in the range of ppm (<30 ppm) itself without the help of the carbide forming elements such as Nb and Ti. The price of Cu is low and Cu-added ultra low carbon steel appears excellent bake hardening behavior and non-aging effect. In the present paper, the annealed texture characteristics were studied in two different ultra low carbon steels after coiling at different temperatures.

2. Experimental procedure

The chemical compositions for the experimental ultra low carbon steels are listed in Table 1. The 30 mm thick slab was hot rolled down to 3.2 mm. Finish rolling was carried out at 920°C followed by coiling at 650 and 720°C. The hot bands were subsequently cold-rolled to 78% and annealed at 800°C for 60sec. The final thickness of the experimental ultra low carbon steel was 0.7 mm. The steel sheets with 10 mm×10 mm×0.7 mm in size were cut in the normal direction (ND). The steel sheets were polished and etched with the nital for optical microscopy. The pole figure {110}, {200}, {211} were measured by Co K α radiation and the orientation distribution function (ODF) is calculated by using the progression extension.

3. Results

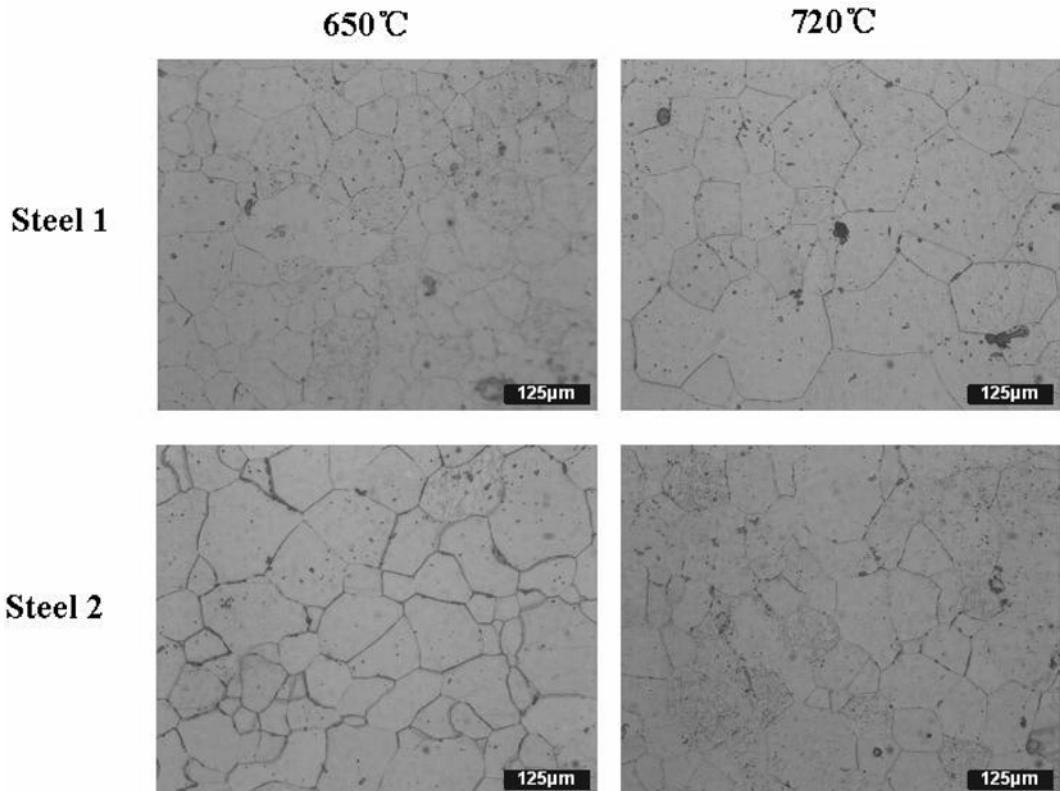
3.1 Microstructure

Fig. 1 shows the annealed microstructures of two different ultra low carbon steels coiled at the temperature of 650 and 720°C. As it can be seen, the microstructures are recrystallized and equiaxed ferrite grains. For the Nb-added ultra low carbon steels, the grain size at high coiling temperature was greater than at low coiling temperature. In the case of Cu-added ultra low carbon steels, the grain size of each sample is almost the same regardless of different coiling temperature.

[†]Corresponding author
E-Mail : yinghua@chonbuk.ac.kr (Y. H. Jiang)

Table 1. Chemical composition of the experimental ULC steels (wt.%)

Steel	C	Mn	P	S	Sol-Al	Nb	Cu	N	Si
1	0.0015	0.5	0.06	0.012	0.035	0.006	-	0.003	0.05
2	0.0015	0.1	0.06	0.012	0.035	-	0.1	0.003	0.05

**Fig. 1.** Optical micrographs of the annealed steels.

3.2 Texture

Fig. 2 shows the corresponding intensity changes of α -fiber ($<110>/\text{RD}$) and γ -fiber ($<111>/\text{ND}$) for the two steels coiled at 650 and 720, respectively. In the Nb-added ultra low carbon steel, on the α -fiber, the intensities were high in vicinity of $\{112\sim223\}<110>$ at the two coiling temperatures. The most intense component $\{223\}<110>$ exhibited an intensity 5-or 7-fold greater than random, respectively. In the γ -fiber, the texture stretched from $\{111\}<110>$ to $\{111\}<112>$, with a strong $\{111\}<112>$ component. The $\{111\}<112>$ component with the intensity 7.5-fold greater than random at high coiling temperature was larger than that at low coiling temperature. It was seen at the coiling temperature of 720°C the two fibers appeared stronger than that at the coiling temperature of 650°C. Especially, the γ -fiber appears strong. In the Cu-added ultra low carbon steel, similarly, on the α -fiber, the intensities were high in vicinity of $\{112\sim223\}<110>$ at

the two coiling temperatures. The most intense component $\{223\}<110>$ exhibited an intensity 5-or 3-fold greater than random. In the γ -fiber, the texture stretched from $\{111\}<110>$ to $\{111\}<112>$ component. At the coiling temperature of 650°C the $\{111\}<110>$ component is identified as a peak orientation, but at the coiling temperature of 720°C the $\{111\}<123>$ component is identified as a peak orientation. The two components exhibited a 5.5-or 4-fold increase over random, respectively. And at the coiling temperature of 650°C the two fibers appeared stronger than that at the coiling temperature of 720°C. On the whole, the Nb-added ultra low carbon steel shows desirable texture at the coiling temperature of 720°C, but the Cu-added ultra low carbon steel shows desirable texture at the coiling temperature of 650°C. Fig. 3 shows the corresponding intensity changes of ε -fiber ($<110>/\text{TD}$) for the two steels coiled at 650 and 720°C, respectively. The ε -fiber of the Nb-added ultra low carbon steel at the

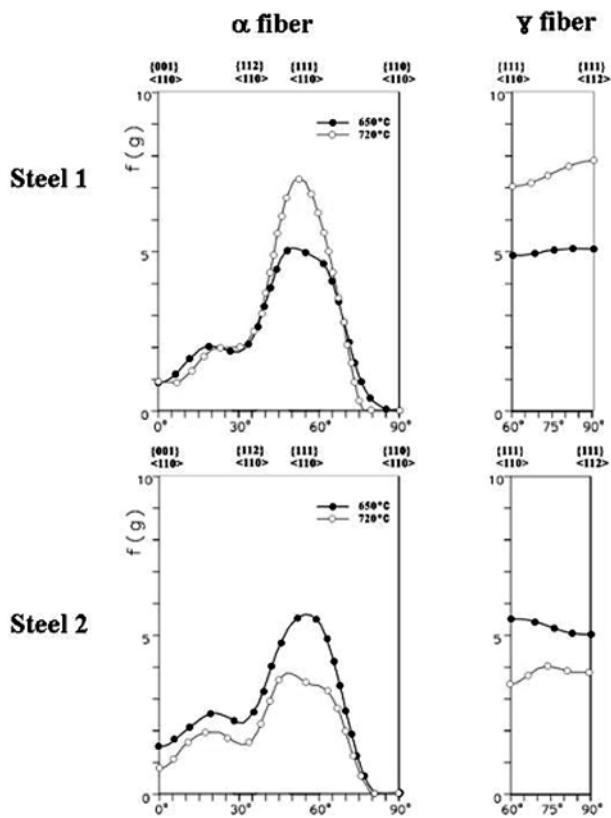


Fig. 2. The α and γ fiber skeleton lines of the annealed steels.

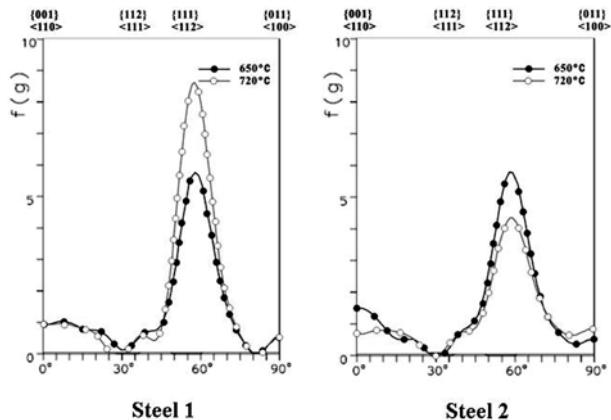


Fig. 3. The ϵ fiber skeleton lines of the annealed steels.

coiling temperature of 720°C is stronger than that at the coiling temperature of 650°C . On the other hand, the ϵ -fiber of the Cu-added ultra low carbon steel at the coiling temperature of 650°C is stronger than that at the coiling temperature of 720°C . In the ϵ -fiber, the maximum intensity is at $\{554\}<225>$ component for two different steels. Especially, the $\{554\}<225>$ intensity of Nb-added ultra low carbon steels at high coiling temperature is stronger than others.

4. Discussions

After coiling at 650 and 720°C , respectively, the microstructures in the Nb- or Cu-added ultra low carbon steels showed recrystallized and equiaxed grains. In the Nb-added ultra low carbon steel, the grain sizes at high coiling temperature of 720°C is larger than that at low coiling temperature of 650°C . The lower the coiling temperature, the lower the content of carbon in the solid solution. This may be connected with the segregation of certain amount of carbon during cooling from the annealing temperature, which is intensified in fine grain steels obtained at a low coiling temperature.⁴⁾ But for Cu-added ultra low carbon steel, the grain sizes are the same, which corresponds the results obtained in.⁵⁾

It is evident from above results that evolution of texture in the high temperature coiling condition is different from that in the low temperature coiling one. In the Nb-added ultra low carbon steel, the α -, γ -and ϵ -fibers are in the ascendant at the high coiling temperature. It is known that Nb, whether in solution or tied in precipitates, suppresses recrystallization processes in ferrite.⁶⁾ So this might cause the increase in recrystallization temperature. The development of texture is dependent on the development of recrystallization. If the recrystallization of ferrite is progressively retarded by the Nb, the development of texture is also retarded. In the Cu-added ultra low carbon steel, the α -, γ -and ϵ -fibers are dominant at the low coiling temperature. In the past, several studies revealed that the high temperature coiling resulted in the formation of fine pre-precipitation of Cu, which caused a deterioration of texture. This just explained the result. It was noted the intensity along the α -fiber peaks at $\{111\}<112>$ in the Nb-added ultra low carbon steel with the coiling temperature of 720°C , but at $\{111\}<110>$ in the Cu-added ultra low carbon steel with the coiling temperature of 650°C . It was known that the $\{111\}<112>$ component is a typical component of annealing texture in steels, and an increase in its intensity indicates that the material has reached a more complete state of recrystallization.⁶⁾ And the increase of $\{111\}<112>$ is related to the increase of the neighboring $\{554\}<225>$ intensity. According to the Fig. 3 the $\{554\}<225>$ component in the γ -fiber appears the strongest in the Nb-added ultra low carbon steel with the coiling temperature of 720°C . The increase of $\{554\}<225>$ is attributed to the solutes effect of Nb.⁷⁾

5. Conclusions

The present study has shown the texture characteristics in two different ultra low carbon steels after coiling at 650 and 720°C, respectively. The α -, γ -and ε -fibers appear similar change trend. The three fibers of the Nb-added ultra low carbon steel is strong at the coiling temperature of 720°C, but that of the Cu-added ultra low carbon steel is strong at the coiling temperature of 650°C. In the γ -fiber of the Nb-added ultra low carbon steel, the most intense component is $\{111\}<112>$ orientation, but for the Cu-added ultra low carbon steel the most intense component is $\{111\}<110>$. These results are closely related to the effect of Nb in the Nb-added ultra low carbon steels.

Acknowledgement

This is a part of the work supported financially by POSCO Technical Research Laboratories.

References

1. K. Tsuzaki, N. R. Ileda and T. Maki, *Scripta Mater.*, **36**, 905 (1997).
2. M. R. Barnett and J. J. Jonas, *ISIJ Inter*, **37**, 706 (1997).
3. R. Mendoza, J. Huante, M. Alanis, C. Gonzalez and J. A. Juarez, *Mater. Sci. Eng.*, **276**, 203 (2000).
4. L. M. Storozheva, R. Bode and K. Hulka, *Met. Sci. Heat Treat.*, **44**(3), 6 (2002).
5. M. Morita, K. Sato and Y. Hosoya, *ISIJ Inter*, **34**, 92 (1994).
6. K. M. Tiitto, C. Jung and P. Wray, *ISIJ Inter*, **44**, 404 (2004).
7. K. Eloot, K. Okuda and K. Sakata, *ISIJ Inter*, **38**, 602 (1998).