

# A COMPARISON OF THE FIDELITY BETWEEN VARIOUS CORES FABRICATED WITH CAD/CAM SYSTEMS

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## INTRODUCTION

As the increase of the demand for esthetic dental restorations, all-ceramic crowns became a general choice of prosthesis. Since Land<sup>1</sup> first introduced the porcelain jacket crown using white gold foil in 1886, various all-ceramic restorations have been established and developed to obtain satisfactory clinical results. In early 1980s, the CAD/CAM (computer-assisted design/computer-assisted manufacturing) system was first brought into the dental field. Since then, various CAD/CAM systems for fabrication of the all-ceramic restorations were developed and used in dental clinic.

Dental CAD/CAM systems use scanning, design and machining process to custom-shape copings from industrially pre-fabricated ceramic blocks. The methods of scanning are categorized into direct method using an intraoral camera, and indirect method using a made stone model. The indirect method is classified by its sensing method: the non-contact type using a probe and the contact type using a laser scanner or a camera.<sup>2</sup> Among various CAD/CAM systems, Procera<sup>3</sup> system accepts contact type, and Lava and Cerec inLab<sup>4</sup> systems accept non-contact type.

The marginal fidelity of prosthesis is an important factor of the successful prosthodontic treatment. In the case of subgingival or ill-fitted margin, it is possible to cause

hypersensitivity, dental caries, plaque accumulation, and gingivitis as well as periodontitis and alveolar bone loss which bring the loss of teeth. When the marginal gap is large, the surface of cement is exposed which induces dissolution of the cement by saliva.<sup>5-10</sup> It is important to improve the fidelity of restorations and to reduce the thickness of cement film since the marginal leakage is influenced by them.<sup>8</sup>

In the study on the fidelity of metal ceramic crowns and restorations fabricated with CAD/CAM system, Yeo *et al.*<sup>11</sup> reported that mean gap dimensions and standard deviations at the marginal opening for the incisor crowns were  $87 \pm 34 \mu\text{m}$  for metal ceramic crown,  $83 \pm 33 \mu\text{m}$  for Celay In-Ceram,  $112 \pm 55 \mu\text{m}$  for conventional In-Ceram, and  $46 \pm 16 \mu\text{m}$  for IPS Empress 2 layering technique. In the study of marginal adaptation and microleakage of Procera AllCeram crowns with four cements, Albert and El-Mowafy<sup>3</sup> reported that Procera AllCeram copings had a significantly larger mean marginal gap ( $54 \mu\text{m}$ ) compared to metal ceramic ( $29 \mu\text{m}$ ). In the study of clinical fit of all-ceramic three-unit fixed partial dentures, generated with three different CAD/CAM systems, Reich *et al.*<sup>4</sup> reported that the medians of marginal gaps were  $75 \mu\text{m}$  for Digident CAD/CAM system,  $65 \mu\text{m}$  for Cerec inLab system and Lava system, and  $54 \mu\text{m}$  for the conventional FPDs. They also concluded the accuracy of CAD/CAM generated three-unit FPDs is satisfactory for clinical use.

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The fabrication of prostheses fabricated with various CAD/CAM systems using high-strength ceramic material is available currently and the accuracy of fit of crown-copings fabricated with CAD/CAM systems is similar to, or exceeds that produced using the conventional casting technique.<sup>8</sup> However, data on such prostheses were often limited and under-studied.

This study compared and analyzed the fidelity between the conventional metal cast core and the cores fabricated with Procera (Nobel Biocare, Gothenburg, Sweden) which uses the contact scanning system, and Lava (3M ESPE, Seefeld, Germany) and Cerec inLab (Sirona Dental System GmbH, Bensheim, Germany) which use the non-contact scanning system.

## MATERIALS AND METHODS

A resin model tooth of mandibular right second molar (AG 3, Frasco, Germany) was prepared by 2566 milling bur (Edenta AG, Switzerland) and milling machine (PFG-100, Cendres & Metaux SA., Switzerland) (Fig. 1). A prepared tooth had rounded shoulder margin of 1.0 mm diameter, 3.0 mm axial height, and 12° convergence angle. All angles and apexes were rounded.

The impression of prepared resin model tooth was taken by additional polymerization impression material (Aquasil Ultra LV & XLV, Densply Caulk, Milford, DE, USA). Self-polymerizing acrylic resin (GC Pattern Resin, GC Corp, Tokyo, Japan) was flown into the impression body to make a pattern for fabrication of the metal master model. The acrylic pattern was invested and casted by the alloy (Rexillum-3, Jeneric/Pentron Incorp., Wallingford, USA) to fabricate a metal master model (Fig. 2). The metal master model was used to measure the fidelity of cores.

Additional polymerization impression material (Aquasil Ultra LV & XLV, Densply Caulk, Milford, DE, USA) was used to take 40 impression of metal master model. 40 duplicated model dies were made using die stone (Fujirock EP, GC, Japan).

Using duplicated model dies, 40 cores (10 cores per group) were fabricated; 10 metal cast cores, 10 Procera cores, 10 Lava cores, and 10 Cerec inLab cores were fabricated. The metal cast cores were fabricated by private dental lab technicians (Gaujung Dental Laboratory, Daegu)

(Fig. 3). The Procera core fabrication was requested to a private dental lab (Myungmun Dental Laboratory, Daegu). 10 duplicated model dies were scanned (Procera Scanner Model 50; Jemtab Systems, Akers, Sweden) and the data were sent to the manufacturer (Procera Sandvik AB; Nobel Biocare AB). 10 Al<sub>2</sub>O<sub>3</sub> cores with a thickness of 0.6 mm were fabricated by the manufacturer. The Lava core fabrication was requested to Lava milling center. 10 duplicated model dies were scanned (Scan Scanner, 3M ESPE, Germany) followed by designing process. The block (ZrO<sub>2</sub> specimen, 3M ESPE, Germany) went through milling process (Lava Form Milling Unit, 3M ESPE, Germany) and sintering process (Lava Therm Furnace, 3M ESPE, Germany) to fabricate 10 Lava cores. The Cerec inLab core fabrication was requested to the private dental lab (Yoon, Won-Sang Dental Laboratory, Seoul). 10 duplicated model dies were scanned (inEos scanner, Sirona Dental System GmbH, Germany) followed by designing process. The block (IPS e.max ZirCAD, Ivoclar Vivadent AG., Liechtenstein) went through milling process (Cerec inLab unit, Sirona Dental System GmbH, Germany) and sintering process (Sintramat high-temperature furnace, Ivoclar Vivadent AG., Liechtenstein) to fabricate 10 Cerec inLab cores (Fig. 4).

Fabricated cores were categorized into 4 groups, 10 each. Metal cast cores were called group 1 as control group. Procera cores, Lava cores and Cerec inLab cores were called group 2, group 3 and group 4 as experimental group.

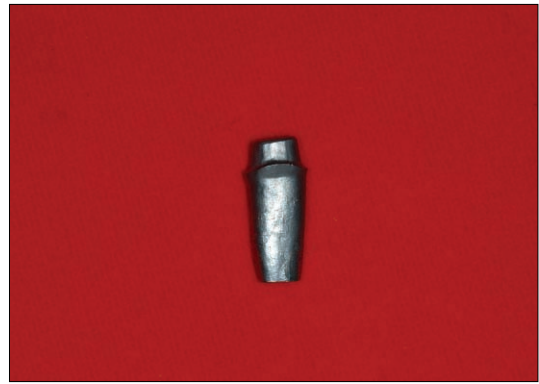
To seat a core on metal master model, a special type of device was designed (Fig. 5). A core was seated on metal master model using Torque controller (TorqControl; anthogyr, Sallanches, France) applying 10 Ncm torque to the top screw of the device (Fig. 6).

The absolute marginal discrepancy was measured using measuring microscope (MM-40, Nikon, Japan) and digital counter (SC-212, Nikon, Japan) (Fig. 7) at ×100 magnification (Fig. 8). The absolute marginal discrepancy of one core was measured at randomly chosen 50 points along the margin. The value was determined by the mean of two measurements at a same point and the mean value of measurements at 50 points was defined as the absolute marginal discrepancy.

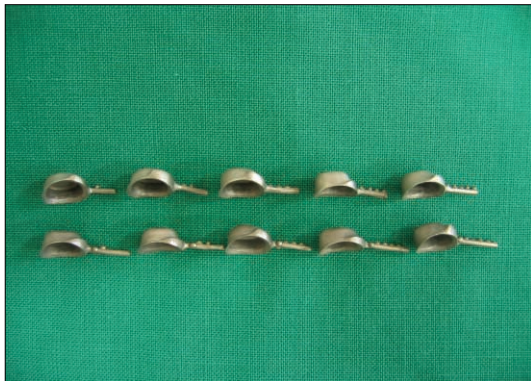
The internal gap was measured by surface area of metal master model via Non-contact type contour measuring



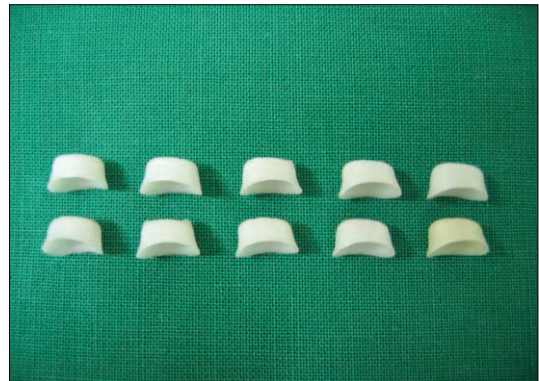
**Fig. 1.** Preparation of resin tooth by using milling machine.



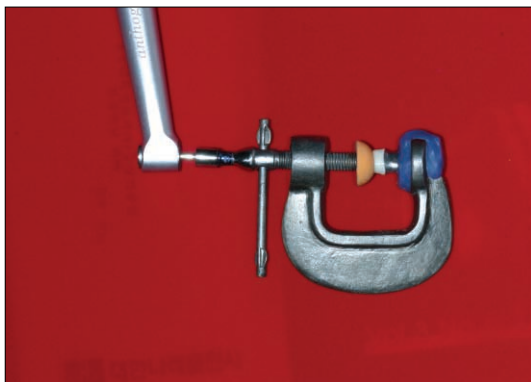
**Fig. 2.** Metal master model.



**Fig. 3.** Metal cast cores.



**Fig. 4.** Cerec inLab cores.



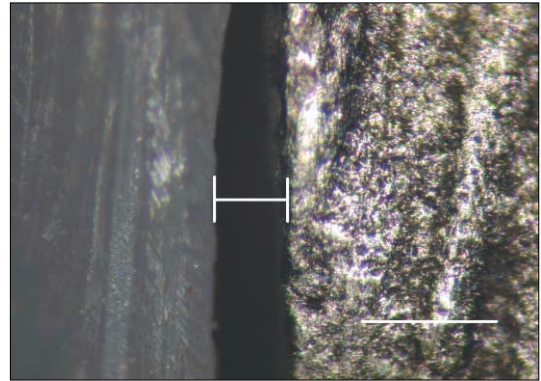
**Fig. 5.** Loading device with torque controller.



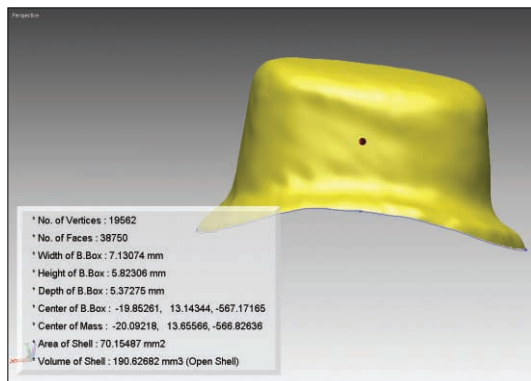
**Fig. 6.** 10Ncm setting of torque controller.



**Fig. 7.** Measuring microscope and digital counter.



**Fig. 8.** Absolute marginal discrepancy of Cerec inLab core (original magnification  $\times 100$ , white bar represents  $100 \mu\text{m}$ ).



**Fig. 9.** Surface area measured using non-contact type contour measuring device.



**Fig. 10.** Electron scale.

device (VIVID 910, Konica Minolta, Tokyo, Japan), as well as weight and density of silicone paste. Non-contact type contour measuring device was used to measure the surface area of metal master model (Fig. 9). The surface area was  $70.15487 \text{ mm}^2$ . To calculate the density, silicone paste (Fusion Wash Type; GC., Tokyo, Japan) was filled in ring which have a hole with diameter of 1 cm and height of 0.3 cm. The weight and the volume were measured. Density = mass/volume =  $0.4118 \text{ g}/0.2355 \text{ cm}^3 = 1.75 \text{ g/cm}^3$ . The

weight of silicone paste was measured by electron scale (AP210S; Ohaus Corp., Pine Brook, NJ, USA) (Fig. 10). The electron scale was regulated at zero degree with metal master model and a core. Then, silicone paste was added into a core and the core was seated on metal master model by finger-pressure. Before the completion of polymerization, over-filled paste was removed and the weight was measured on electron scale. The internal gap of a core was calculated by the following equation.

Thickness (internal gap) = weight/(density  $\times$  area)

The means and standard deviations per group were calculated and statistical inferences among the groups were analyzed using one-way ANOVA test and Tukey's HSD test at 0.05 level of significance.

## RESULTS

The fidelity of metal cast core showed the smallest gaps, followed by Lava core, Cerec inLab core and Procera core (Table I, IV). When comparing the absolute marginal discrepancies, 3 core groups showed significant differences with the metal cast core group as well as among themselves ( $P < 0.05$ ) (Table II, III). When comparing the internal gaps, 3 core groups showed significant differences with the metal cast core group. Also, there were significant differences between Procera cores and Lava cores, and between Procera cores and Cerec inLab cores ( $P < 0.05$ ). However, there was no significant difference between Lava cores and Cerec inLab cores (Table V, VI).

## DISCUSSION

The crown fidelity is defined variously among researchers. Holmes *et al.*<sup>10</sup> defined various types of measurements between the casting surface and the tooth to clarify each term. The angular combination of the marginal gap and the extension error (overextension or underextension) was called the absolute marginal discrepancy. This study accepted the concept of the absolute marginal discrepancy to measure the fidelity of cores.

The clinically acceptable range of the crown fidelity is not yet clearly indicated. Sorensen *et al.*<sup>5</sup> reported that small defects less than or equal to 50  $\mu\text{m}$  were associated with significantly less bone loss than defects exceeding this value, and the prostheses fabricated under a conventional casting method were showed the marginal adaptation below 50  $\mu\text{m}$  when the laboratory condition was optimal.<sup>2,6-8</sup> However, as a matter of fact, it is difficult to obtain the marginal adaptation around 50  $\mu\text{m}$ . Hung *et al.*<sup>12</sup> reported that the practical range for clinical acceptability of fit seems to be approximately 50 to 75  $\mu\text{m}$ . McLean and von

**Table I.** Mean and standard deviation (SD) of absolute marginal discrepancies in each of 4 core groups (unit:  $\mu\text{m}$ )

	Group 1	Group 2	Group 3	Group 4
1	30.8	68.9	40.5	47.1
2	31.1	77.9	41.0	47.9
3	36.5	69.6	37.4	66.6
4	31.5	69.1	42.7	68.0
5	30.1	86.1	30.6	54.4
6	36.3	61.6	43.3	64.2
7	33.0	71.4	39.0	46.8
8	26.8	79.1	42.2	61.2
9	30.1	66.9	52.2	48.7
10	39.1	71.6	39.2	48.5
Mean	32.5	72.2	40.8	55.3
SD	3.7	7.0	5.4	8.7

**Table II.** Results of one-way ANOVA test for absolute marginal discrepancy

	Sum of squares	DF	Mean square	F	P
Between groups	9116.985	3	3038.995	72.106	.000
Within groups	1517.27	36	42.146		
Total	10634.255	39			

**Table III. ( i ).** Results of Tukey' s HSD test for absolute marginal discrepancy

( I ) groups	( J ) groups	Mean difference (I-J, $\mu$ m)	P value
1	2	-39.69000*	.000
1	3	-8.28000*	.034
1	4	-22.81000*	.000
2	3	31.41000*	.000
2	4	16.88000*	.000
3	4	-14.53000*	.000

\* Mean difference is significant at the 0.05 level.

**Table III. ( ii ).** Statistical comparisons between groups in absolute marginal discrepancy

Group	1	2	3	4
1	-			
2	*	-		
3	*	*	-	
4	*	*	*	-

\* denotes pair of groups significantly different at the 0.05 level.

**Table IV.** Mean and standard deviation (SD) of internal gaps in each of 4 core groups(unit:  $\mu$ m)

	Group 1	Group 2	Group 3	Group 4
1	31.8	70.0	40.7	44.8
2	42.4	74.1	50.5	45.6
3	38.3	83.1	46.4	54.6
4	32.6	71.7	39.9	47.2
5	32.6	66.8	42.4	50.5
6	44.8	68.4	44.8	63.5
7	32.6	65.2	35.8	54.6
8	39.1	71.7	61.9	57.8
9	43.2	75.8	50.5	45.6
10	46.4	66.8	46.4	53.8
Mean	38.4	71.4	45.9	51.8
SD	5.7	5.3	7.3	6.2

**Table V.** Results of one-way ANOVA test for internal gap

	Sum of squares	DF	Mean Square	F	P
Between groups	5971.287	3	1990.429	52.571	.000
Within groups	1363.021	36	37.862		
Total	7334.308	39			

**Table VI. ( i ).** Results of Tukey' s HSD test for internal gap

( I ) groups	( J ) groups	Mean difference (I-J, $\mu\text{m}$ )	P value
1	2	-32.98000*	.000
1	3	-7.55000*	.045
1	4	-13.42000*	.000
2	3	25.43000*	.000
2	4	19.56000*	.000
3	4	-5.87000	.162

\* Mean difference is significant at the 0.05 level.

**Table VI. ( ii ).** Statistical comparisons between groups in internal gap

Group	1	2	3	4
1	-			
2	*	-		
3	*	*	-	
4	*	*	NS	-

\* denotes pair of groups significantly different at the 0.05 level.

NS : not significant

Fraunhofer<sup>13</sup> reported that for a good long-term prognosis, the clinically acceptable marginal gap for a crown is within the range of 120  $\mu\text{m}$ . According to numerous studies on the crown fidelity of cast crowns and crowns fabricated with CAD/CAM system, the value of 120  $\mu\text{m}$  was the clinically acceptable marginal gap.<sup>3,8,14</sup>

According to study results on the crown fidelity of cast crowns, metal margin showed mean marginal opening of 27.5  $\mu\text{m}$ <sup>15</sup>, noble alloy crown showed marginal opening of 25  $\mu\text{m}$ <sup>16</sup>, PFM crowns showed marginal opening of 45-87  $\mu\text{m}$ <sup>11-15</sup>, and metal-ceramic copings showed mean marginal gap of 29  $\mu\text{m}$ .<sup>3</sup>

There were many studies on the fidelity of crowns fabricated with CAD/CAM system. May *et al.*<sup>8</sup> reported that mean gap dimensions for marginal openings, internal adaptation, and precision of fit for Procera AllCeram crowns were below 70  $\mu\text{m}$ . Boening *et al.*<sup>17</sup> reported that medians of mean marginal gap widths of Procera AllCeram crowns were between 80 and 95  $\mu\text{m}$  in anterior teeth and between 90 and 145  $\mu\text{m}$  in posterior teeth. Karlsson<sup>18</sup> reported that the marginal discrepancy of Procera titanium crowns was approximately 60  $\mu\text{m}$  *in vitro* and 70  $\mu\text{m}$  *in vivo*,

with a range of 3-205  $\mu\text{m}$ . Denissen *et al.*<sup>19</sup> reported that the marginal gap of Procera cores on the stone dies was  $68 \pm 53$   $\mu\text{m}$  and it was a favorable measurement value for a clinically acceptable, strong all-ceramic onlay. Quintas *et al.*<sup>20</sup> reported that the mean values of vertical marginal discrepancy of procera copings were 25  $\mu\text{m}$  before cementation and 44  $\mu\text{m}$  after cementation. Hertlein *et al.*<sup>21</sup> investigated the marginal fit of the Lava AllCeramic System for anterior and posterior teeth with a chamfered preparation margin. Under a stereomicroscope, the marginal gap was  $38 \pm 20$   $\mu\text{m}$  and the absolute marginal discrepancy was  $72 \pm 36$   $\mu\text{m}$ . In the study on clinical fit of all-ceramic three-unit fixed partial dentures, generated with three different CAD/CAM systems, Reich *et al.*<sup>4</sup> reported that the medians of marginal gaps were 65  $\mu\text{m}$  for Lava system and 65  $\mu\text{m}$  for Cerec inLab system. Bindle and Mormann<sup>22</sup> evaluated the marginal and internal fit of all-ceramic CAD/CAM crown copings with chamfer margin. In the case of Lava system, the marginal gap was  $43 \pm 23$   $\mu\text{m}$ , internal mesiodistal gap width was  $82 \pm 49$   $\mu\text{m}$ , and internal mid-orobuccal gap width was  $114 \pm 58$   $\mu\text{m}$ .

In this study, the absolute marginal discrepancies of metal cast cores, Procera cores, Lava cores and Cerec inLab cores

were  $32.5 \pm 3.7 \mu\text{m}$ ,  $72.2 \pm 7.0 \mu\text{m}$ ,  $40.8 \pm 5.4 \mu\text{m}$  and  $55.3 \pm 8.7 \mu\text{m}$  respectively. The internal gaps were  $38.4 \pm 5.7 \mu\text{m}$ ,  $71.4 \pm 5.3 \mu\text{m}$ ,  $45.9 \pm 7.3 \mu\text{m}$  and  $51.8 \pm 6.2 \mu\text{m}$  respectively. Even though there were general differences in measuring locations, conditions and definition of the crown fidelity, this study showed satisfactory values within the experimental condition based on previous studies. The tested restorations had clinically acceptable fidelity.

The fidelity of restorations is influenced by various factors. In general, tooth preparation, impression body, accuracy of master model, restoration material, processing method, marginal contour and location, type of cement, convergence of axial wall, and luting space have influence on the fidelity of restorations. Also, in the case of CAD/CAM system, scanning, software design, milling process and shrinkage effect after sintering additionally influences the fidelity.

To obtain the optimal results, several considerations were taken on the experimental design. First, the prepared tooth used in this study had 1.0 mm wide rounded shoulder margin, 3.0 mm axial height and  $12^\circ$  convergence angle. This design and numerical values are based on data of previous studies. Lin *et al.*<sup>23</sup> evaluated the marginal and internal adaptation of Procera copings using different tooth preparations. Mean external marginal openings were  $64 \mu\text{m}$  for chamfer finish line,  $51 \mu\text{m}$  for 0.8 mm rounded shoulder, and  $68 \mu\text{m}$  for 0.5 mm rounded shoulder. They also reported that the variations in the vertical height of inter-proximal finish lines did not significantly affect marginal opening. In general, less than  $12^\circ$  convergence angle is suggested for the favorable crown retention. However, Nakamura *et al.*<sup>2</sup> reported that it seems appropriate to use the standard  $12^\circ$  total convergence angle specified by the Cerec system.

Second, because the core mainly determines the overall fit of a veneered crown, in this study, the fit of cores was measured without veneering.<sup>20,22,24,25</sup>

Third, in this study, the amount of torque applied to the upper screw to seat a thin ceramic core on metal master model was restricted to 10 Ncm, because in an unpublished pilot study most of the ceramic copings were fractured above this limit.<sup>20</sup>

Forth, Groten *et al.*<sup>26</sup> reported that approximately 50 measurements are required for clinically relevant information about gap size regardless of gap definition or

cementation condition. Therefore, based on above data the absolute marginal discrepancy of a core was measured at randomly chosen 50 points along the margin.

Fifth, there was a study result that the type of cement influences the marginal adaptation.<sup>3</sup> In this study, the absolute marginal discrepancy was measured without permanent cementation to eliminate the influence of cement on the marginal adaptation.

However, the laboratory testing cannot exactly reproduce the clinical condition. Therefore, the results should be viewed carefully and there are a few limitations in this study. First, in this study, the fidelity of cores was measured without permanent cementation of the core and it could potentially affect the marginal adaptation. To reproduce the clinical condition, Jorgensen<sup>27</sup> suggested that any study aimed at determining the marginal adaptation of a crown system requires cementation of the crowns. In the study of the marginal adaptation before and after the permanent cementation, the marginal discrepancy had been increased<sup>12,20</sup> significantly<sup>24</sup> after cementation.

Second, due to the limitations of the microscopic imaging, only measurements of absolute marginal discrepancy in vertical dimension could be made. However, the evaluation of vertical discrepancy was chosen as potentially more clinically significant, since this discrepancy affects the exposure of luting agent and the horizontal discrepancy affects cleanability and plaque retention.<sup>28</sup>

Third, Sorensen<sup>9</sup> introduced a standardized method for determination of crown margin fidelity: direct view, cross-sectional view, impression technique, and explorer and visual view. This study used direct view to evaluate the absolute marginal discrepancy. The direct view method is convenient, easy, and rapid because the crown is retrievable, unlike the cementation, embedment, and sectioning method, which causes destruction of the crown. However, it is difficult to determine the repeatable measuring point of reference with a rounded margin, and to assess over-contouring of crown margin. Although clinically prepared crown margin seems to be sharp, it is showed rounded under microscope. In this study, it was difficult to determine measuring points of rounded margin and over-contoured margin and also it could affect the results.

Forth, luting space of specimens was not consistent in this



study. There was a study reporting that the crown fidelity was different according to various cementation spaces.<sup>2</sup> If all cores involved in this study had same luting spaces, the data could have been different. However, this study focused on processing accuracy of cores fabricated with different CAD/CAM systems using same master model. Since each CAD/CAM system accepts different luting spaces as its optimal fabrication condition, inconsistency of the luting spaces did not affect the purpose of this study much.

Nevertheless several limitations mentioned above, all values on the fidelity of cores fabricated with CAD/CAM system were within clinically acceptable range. Especially Lava cores showed the fidelity of below 50  $\mu\text{m}$  and it means that the fidelity of core fabricated with CAD/CAM system is now very close to fidelity of core produced using conventional casting technique.

To obtain more reliable research data on the fidelity of cores fabricated with CAD/CAM system, further evaluation of prostheses in the intraoral condition and more studies considered various factors are needed.

## CONCLUSIONS

The results were as follows.

1. The absolute marginal discrepancies were  $32.5 \pm 3.7 \mu\text{m}$  for metal cast core,  $72.2 \pm 7.0 \mu\text{m}$  for Procera core,  $40.8 \pm 5.4 \mu\text{m}$  for Lava core, and  $55.3 \pm 8.7 \mu\text{m}$  for Cerec inLab core. The internal gaps were  $38.4 \pm 5.7 \mu\text{m}$  for metal cast core,  $71.4 \pm 5.3 \mu\text{m}$  for Procera core,  $45.9 \pm 7.3 \mu\text{m}$  for Lava core, and  $51.8 \pm 6.2 \mu\text{m}$  for Cerec inLab core. The fidelity of metal cast core showed the smallest gaps, followed by Lava core, Cerec inLab core and Procera core.
2. When comparing the absolute marginal discrepancies, 3 core groups showed significant differences with the metal cast core group as well as among themselves ( $P < 0.05$ ).
3. When comparing the internal gaps, 3 core groups showed significant differences with the metal cast core group. Also, there were significant differences between Procera cores and Lava cores, and between Procera cores and Cerec inLab cores ( $P < 0.05$ ). However, there was no significant difference between Lava cores and Cerec inLab cores.

4. The fidelities of 4 core groups were all within the clinically acceptable range (120  $\mu\text{m}$ ).

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## A COMPARISON OF THE FIDELITY BETWEEN VARIOUS CORES FABRICATED WITH CAD/CAM SYSTEMS

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**STATEMENT OF PROBLEM:** Recently, various all-ceramic crowns fabricated with CAD/CAM systems have come into wide use in dental clinic. However, there are only few domestic studies on CAD/CAM restorations. **PURPOSE:** Purpose of this study was to compare the fidelity (absolute marginal discrepancy and internal gap) between various cores fabricated with different CAD/CAM systems (Procera system, Lava system, Cerec inLab system) and conventional metal cast core. **MATERIALS AND METHODS:** 10 cores per each system were fabricated. The absolute marginal discrepancies were measured using measuring microscope and digital counter. The internal gaps were calculated using a silicone paste. The results were statistically analyzed using the one-way ANOVA test and Tukey's HSD test. **RESULTS:** Within the limits of this study the results were as follows. 1. The absolute marginal discrepancies were  $32.5 \pm 3.7 \mu\text{m}$  for metal cast core,  $72.2 \pm 7.0 \mu\text{m}$  for Procera core,  $40.8 \pm 5.4 \mu\text{m}$  for Lava core, and  $55.3 \pm 8.7 \mu\text{m}$  for Cerec inLab core. The internal gaps were  $38.4 \pm 5.7 \mu\text{m}$  for metal cast core,  $71.4 \pm 5.3 \mu\text{m}$  for Procera core,  $45.9 \pm 7.3 \mu\text{m}$  for Lava core, and  $51.8 \pm 6.2 \mu\text{m}$  for Cerec inLab core. 2. The fidelity of metal cast core showed the smallest gaps, followed by Lava core, Cerec inLab core, and Procera core. **CONCLUSION:** The fidelities of 4 core groups were all within the clinically acceptable range ( $120 \mu\text{m}$ ).

**KEY WORDS:** All-ceramic crown, CAD/CAM system, Absolute marginal discrepancy, Internal gap

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