

## Vortex Filament Equation and Non-linear Schrödinger Equation in $S^3$

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ABSTRACT. In 1906, da Rios, a student of Levi-Civita, wrote a master's thesis modeling the motion of a vortex in a viscous fluid by the motion of a curve propagating in  $R^3$ , in the direction of its binormal with a speed equal to its curvature. Much later, in 1971 Hasimoto showed the equivalence of this system with the non-linear Schrödinger equation (NLS)

$$q_t = i(q_{ss} + \frac{1}{2}|q|^2q).$$

In this paper, we use the same idea as Terng used in her lecture notes but different technique to extend the above relation to the case of  $S^3$ , and obtained an analogous equation that

$$q_t = i[q_{ss} + (\frac{1}{2}|q|^2 + 1)q].$$

### 1. Introduction

The material of this section was taken from [2] with a minor modification.

#### 1.1. A special orthogonal frame field on $S^3$

$S^3$  is the unit sphere in  $R^4$  i.e.,

$$(1.1) \quad S^3 = \{x \in R^4 \mid |x| = 1\}.$$

For any  $x, y \in S^3$ , the distance  $d(x, y)$  between  $x$  and  $y$  is defined by

$$(1.2) \quad \cos d(x, y) = x \cdot y,$$

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where  $x \cdot y$  is the inner product of  $x$  and  $y$ . For any constant  $a, a \in (0, 1)$ , there exists  $A \in O(4)$  such that

$$(1.3) \quad d(x, Ax) = a \quad \forall x \in S^3.$$

For example we may take

$$(1.4) \quad A = \begin{pmatrix} a & -b & -c & -d \\ b & a & -d & c \\ c & d & a & -b \\ d & -c & b & a \end{pmatrix} \text{ or } A = \begin{pmatrix} a & b & c & d \\ -b & a & -d & c \\ -c & d & a & -b \\ -d & -c & b & a \end{pmatrix},$$

and  $a^2 + b^2 + c^2 + d^2 = 1$ .

We can also regard  $S^3$  as a set of all the unit quaternions and regard  $R^4$  as a non-commutative division algebra. Its unit element is  $1=(1,0,0,0)$ , and its generators are  $i = (0, 1, 0, 0)$ ,  $j = (0, 0, 1, 0)$ ,  $k = (0, 0, 0, 1)$ , where  $i, j, k$  satisfy

$$(1.5) \quad \begin{cases} i \cdot j = k = -j \cdot i \\ j \cdot k = i = -k \cdot j \\ k \cdot i = j = -i \cdot k \\ i^2 = j^2 = k^2 = -1. \end{cases}$$

Define the module of a quaternion  $x = x_1 1 + x_2 i + x_3 j + x_4 k \in R^4$  by

$$(1.6) \quad |x|^2 = \sum_{i=1}^4 x_i^2,$$

and the product of two quaternions has the property:

$$(1.7) \quad |x \cdot y| = |x| \cdot |y|,$$

for any  $x, y \in R^4$ . So the set of all the unit quaternions i.e  $S^3$  is a non-commutative Lie group. The two matrices in (1.4) just correspond to the left and right translation of  $a1 + bi + cj + dk \in S^3$ . That is to say, for  $g = a1 + bi + cj + dk \in S^3$  we have

$$Lg, Rg : S^3 \rightarrow S^3$$

$$(1.8) \quad Lg(x) = g \cdot x; \quad Rg(x) = x \cdot g; \quad \text{for } x \in S^3.$$

The mapping

$$(1.9) \quad a1 + bi + cj + dk \mapsto \begin{pmatrix} a & -b & -c & -d \\ b & a & -d & c \\ c & d & a & -b \\ d & -c & b & a \end{pmatrix},$$

gives an isomorphism from  $S^3$  to a subgroup of  $O(4)$  corresponding to the left translation which is determined by the element in  $S^3$ . It will be convenient to regard  $S^3$  as this subgroup for computation.

In the following we'll find the tangent space of  $S^3$  at the unit element. It is spanned by  $x_1 = (0, 1, 0, 0), x_2 = (0, 0, 1, 0), x_3 = (0, 0, 0, 1)$ . Notice that  $x_1$  is the tangent vector of the curve  $c(t) = (\cos t, \sin t, 0, 0) \in S^3$  at  $1=(1,0,0,0)$ . Since

$$(1.10) \quad c(t) = \cos t \cdot 1 + \sin t \cdot i = \begin{pmatrix} \cos t & -\sin t & 0 & 0 \\ \sin t & \cos t & 0 & 0 \\ 0 & 0 & \cos t & -\sin t \\ 0 & 0 & \sin t & \cos t \end{pmatrix},$$

so we can regard  $x_1$  as

$$(1.11) \quad \frac{d}{dt}c(t)|_{t=0} = \begin{pmatrix} 0 & -1 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 \\ 0 & 0 & 1 & 0 \end{pmatrix} \in O(4),$$

similarly regard  $x_2, x_3$  as

$$(1.12) \quad \begin{pmatrix} 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 1 \\ 1 & 0 & 0 & 0 \\ 0 & -1 & 0 & 0 \end{pmatrix} \quad \begin{pmatrix} 0 & 0 & 0 & -1 \\ 0 & 0 & -1 & 0 \\ 0 & 1 & 0 & 0 \\ 1 & 0 & 0 & 0 \end{pmatrix}$$

respectively. It's easy to verify that

$$(1.13) \quad [x_1, x_2] = 2x_3, [x_2, x_3] = 2x_1, [x_3, x_1] = 2x_2.$$

If we ignore the first component of  $x_i, i = 1, 2, 3$ , and regard it as the vector of  $R^3$  then

$$(1.14) \quad \begin{cases} x_1 \times x_2 = x_3 \\ x_2 \times x_3 = x_1 \\ x_3 \times x_1 = x_2 \end{cases},$$

or use the usual inner product and orientation in  $S^3$ , we can also define the above relation.

Let  $\tilde{x}_i$  be the vector field which is obtained by the left translation of  $x_i$  similarly we have

$$(1.15) \quad \begin{cases} \tilde{x}_1 \times \tilde{x}_2 = \tilde{x}_3 \\ \tilde{x}_2 \times \tilde{x}_3 = \tilde{x}_1 \\ \tilde{x}_3 \times \tilde{x}_1 = \tilde{x}_2 \end{cases}.$$

The cross product "×" in the tangent space at each point in  $S^3$  is defined by ordinary inner product and orientation.

### 1.2. The Frenet frame of curves on $S^3$

In this section we want to build the Frenet frame of curves in  $S^3$ . The theory of curves in  $S^3$  has a special treatment. In other words we can use left invariant vector field  $\tilde{x}_i$  to express all the tangent vector fields on  $S^3$ .

Let  $c : [0, l] \rightarrow S^3$  be a curve and parametrized by its arc length. Its tangent vector is

$$(1.16) \quad \frac{d}{ds}c(s) = t(s),$$

as  $c(s) \in S^3$ , then

$$(1.17) \quad c(s) \cdot c(s) = 1.$$

Differentiating both sides of (1.17), we get

$$(1.18) \quad \frac{d}{ds}c(s) \cdot c(s) = 0.$$

So  $t(s) = \frac{d}{ds}c(s)$  is the tangent vector field on  $S^3$  along  $c(s)$ , it can be expressed as

$$(1.19) \quad t(s) = \sum_{i=1}^3 f_i(s)\tilde{x}_i(c(s)),$$

where  $f_i(s)$  are some smooth functions on  $c(s)$ . As  $c(s)$  is parametrized by its arc length, so

$$(1.20) \quad \sum_{i=1}^3 f_i^2(s) = 1.$$

Differentiating both sides of (1.20), we get

$$(1.21) \quad \sum_{i=1}^3 f_i(s)f_i'(s) = 0.$$

Let  $\nabla'$  denotes covariant differentiation on  $S^3$ . Any vector fields along  $c(s)$  can be expressed as

$$(1.22) \quad \sum_{i=1}^3 h_i(s)\tilde{x}_i(c(s)).$$

Then

$$\begin{aligned}
 (1.23) \quad & \frac{\nabla'}{ds} \left\{ \sum_{i=1}^3 h_i(s) \tilde{x}_i(c(s)) \right\} \\
 &= \sum_{i=1}^3 h'_i(s) \tilde{x}_i(c(s)) + \sum_{i=1}^3 h_i(s) \frac{\nabla'}{ds} \tilde{x}_i(c(s)) \\
 &= \sum_{i=1}^3 h'_i(s) \tilde{x}_i(c(s)) + \sum_{i=1}^3 h_i(s) \sum_{j=1}^3 f_j(s) \nabla_{\tilde{x}_j}^{\tilde{x}_i}(c(s)) \\
 &= \sum_{i=1}^3 h'_i(s) \tilde{x}_i(c(s)) + \frac{1}{2} \sum_{i=1}^3 \sum_{j=1}^3 h_i(s) f_j(s) [\tilde{x}_j, \tilde{x}_i](c(s)) \\
 &= \sum_{i=1}^3 h'_i(s) \tilde{x}_i(c(s)) + \det \begin{pmatrix} \tilde{x}_1 & \tilde{x}_2 & \tilde{x}_3 \\ f_1 & f_2 & f_3 \\ h_1 & h_2 & h_3 \end{pmatrix}.
 \end{aligned}$$

In particular

$$(1.24) \quad \frac{\nabla'}{ds} t(s) = \sum_{i=1}^3 f'_i(s) \tilde{x}_i(c(s)).$$

Define curvature function of curve  $c(s)$  by

$$(1.25) \quad k = \left| \frac{\nabla'}{ds} t(s) \right| = \left( \sum_{i=1}^3 f_i'^2(s) \right)^{\frac{1}{2}}.$$

Assume that  $k \neq 0$  then the normal vector field along  $c(s)$  is defined by

$$(1.26) \quad n = \frac{1}{k} \frac{\nabla'}{ds} t(s) = \frac{1}{k} \sum_{i=1}^3 f'_i(s) \tilde{x}_i(c(s)).$$

Then  $n$  is a unit vector of the tangent space of  $S^3$  at  $c(s)$ , and  $n$  is perpendicular to  $t$ .

Binormal vector field along  $c(s)$  is given by:

$$(1.27) \quad b = t \times n = \frac{1}{k} \det \begin{pmatrix} \tilde{x}_1 & \tilde{x}_2 & \tilde{x}_3 \\ f_1 & f_2 & f_3 \\ f'_1 & f'_2 & f'_3 \end{pmatrix} \equiv \frac{1}{k} \sum_{i=1}^3 g_i(s) \tilde{x}_i(c(s)).$$

So  $b$  is still a unit vector of the tangent space of  $S^3$  at  $c(s)$ , and  $b$  is perpendicular to both  $t$  and  $n$ . By (1.26), (1.24) can be written as

$$(1.28) \quad \frac{\nabla'}{ds} t(s) = kn.$$

Let

$$(1.29) \quad \tau = \frac{\nabla'}{ds} n(s) \cdot b(s),$$

the function  $\tau$  is called the torsion of the curve  $c(s)$ . By direct computation we get

$$(1.30) \quad \frac{\nabla'}{ds} n(s) = -kt(s) + \tau b(s),$$

$$(1.31) \quad \frac{\nabla'}{ds} b(s) = -\tau n(s).$$

So along the curve  $c(s)$  there is an orthogonal frame field  $\{c(s); t(s), n(s), b(s)\}$  which is called Frenet frame of curves on  $S^3$ . (1.28), (1.30), (1.31) are called Frenet formula. We rewrite it in the matrix form

$$(1.32) \quad \frac{\nabla'}{ds} \begin{pmatrix} t \\ n \\ b \end{pmatrix} = \begin{pmatrix} 0 & k & 0 \\ -k & 0 & \tau \\ 0 & -\tau & 0 \end{pmatrix} \begin{pmatrix} t \\ n \\ b \end{pmatrix}.$$

### 1.3. The parallel frame of curves on $S^3$

We want to change the Frenet frame  $(t, n, b)^T$  to  $(e_1, e_2, e_3)^T$  so that the 2,3-th entry of the coefficient matrix of  $\frac{\nabla'}{ds}(e_1, e_2, e_3)^T$  is zero. To do this, we follow the method as described in [1]. Rotate the Frenet frame  $(n, b)$  by an angle  $\beta(s)$  satisfy that

$$(1.33) \quad \beta'(s) = -\tau(s),$$

then

$$(1.34) \quad \frac{\nabla'}{ds} e_2 \cdot e_3 = 0.$$

So that we get the new o.n frame  $(e_1, e_2, e_3)^T$ , and it satisfies

$$(1.35) \quad \frac{\nabla'}{ds} \begin{pmatrix} e_1 \\ e_2 \\ e_3 \end{pmatrix} = \begin{pmatrix} 0 & k_1 & k_2 \\ -k_1 & 0 & 0 \\ -k_2 & 0 & 0 \end{pmatrix} \begin{pmatrix} e_1 \\ e_2 \\ e_3 \end{pmatrix},$$

where

$$(1.36) \quad \begin{cases} k_1 = k \cos \beta(s) \\ k_2 = -k \sin \beta(s) \end{cases}.$$

The o.n frame  $(e_1, e_2, e_3)^T$  is called parallel frame along  $c(s)$ . The function  $k_1(s), k_2(s)$  are called the principal curvatures along  $e_2, e_3$  respectively. However,

the choice of parallel frame is not unique, because we can replace  $\beta(s)$  by  $\beta(s)$  plus a constant  $\beta_0$ , get another o.n frame  $(e_1, v_2, v_3)^T$ . It is again parallel, but the principal curvature  $k_1, k_2$  along  $v_2, v_3$  are satisfies

$$(1.37) \quad \frac{\nabla'}{ds} e_1 = k_1 e_2 + k_2 e_3 = \tilde{k}_1 v_2 + \tilde{k}_2 v_3.$$

**2. Vortex filament equation and the NLS in  $S^3$**

In 1906, da.Rios, a graduate student of Levi-Civita, wrote a master degree thesis, in which he modeled the movement of a thin vortex in a vicious fluid by the motion of a curve propagating in  $R^3$  in the direction of its binormal with a speed equal to its curvature according to

$$(2.1) \quad \gamma_t = \gamma_s \times \gamma_{ss}.$$

This is called the vortex filament equation or smoke ring equation, and it can be regarded as a dynamical system on the space of curves in  $R^3$ . Much later, in 1971, Hasimoto showed the equivalence of this system with the NLS

$$(2.2) \quad q_t = i(q_{ss} + \frac{1}{2}|q|^2 q).$$

In this section we'll build the vortex filament equation in  $S^3$  similar to that as in  $R^3$ , and study the relationship between vortex filament equation and the NLS in  $S^3$ . For any  $\gamma(s, t)$  belongs to  $S^3$ ,  $\gamma(s, t)$  is a surface in  $S^3$  so

$$(2.3) \quad \gamma(s, t) \cdot \gamma(s, t) = 1.$$

Differentiating both sides of (2.3) with respect to  $s$  and  $t$  respectively

$$(2.4) \quad \begin{cases} \gamma_s(s, t) \cdot \gamma(s, t) = 0 \\ \gamma_t(s, t) \cdot \gamma(s, t) = 0. \end{cases}$$

So both  $\gamma_s(s, t)$  and  $\gamma_t(s, t)$  are the vectors of the tangent space of  $S^3$  at  $\gamma(s, t)$ .

We can use left invariant vector fields  $\tilde{x}_i$  to express all the tangent vector fields on  $S^3$ , let

$$(2.5) \quad \gamma_s(s, t) = \sum_{i=1}^3 f_i(s, t) \tilde{x}_i(s, t),$$

then similar to (1.24),

$$(2.6) \quad \frac{\nabla'}{ds} \gamma_s(s, t) = \sum_{i=1}^3 \frac{d}{ds} f_i(s, t) \tilde{x}_i(\gamma(s, t)).$$

So  $\gamma_s(s, t) \times \frac{\nabla'}{ds} \gamma_s(s, t)$  is still a vector of tangent space of  $S^3$  at  $\gamma(s, t)$ . If  $\gamma(s, t)$  satisfy

$$(2.7) \quad \gamma_t(s, t) = \gamma_s(s, t) \times \frac{\nabla'}{ds} \gamma_s(s, t),$$

we call  $\gamma(s, t)$  is the vortex filament surface in  $S^3$ . (2.7) is called the vortex filament equation on  $S^3$ .

Equation (2.7) has the property:

**Proposition.** *If  $\gamma_s(s, t)$  is a solution of (2.7) and  $|\gamma_s(s, 0)| = 1$  for all  $s$ , then  $|\gamma_s(s, t)| = 1$  for all  $(s, t)$ . In other words if  $\gamma(\cdot, 0)$  is parametrized by arc length then so is  $\gamma(\cdot, t)$  for all  $t$ .*

*Proof.* It suffices to prove that

$$(2.8) \quad \frac{d}{dt} \langle \gamma_s(s, t), \gamma_s(s, t) \rangle = 0$$

Remark:  $\langle \cdot, \cdot \rangle$  is the inner product in  $S^3$ . To see (2.8), we compute directly to get:

$$(2.9) \quad \begin{aligned} \frac{1}{2} \frac{d}{dt} \langle \gamma_s(s, t), \gamma_s(s, t) \rangle &= \left\langle \frac{\nabla'}{dt} \gamma_s, \gamma_s \right\rangle \\ &= \left\langle \frac{d}{dt} \gamma_s - a \gamma, \gamma_s \right\rangle = \left\langle \frac{d}{dt} \gamma_s, \gamma_s \right\rangle \\ &= \left\langle \frac{d}{ds} \gamma_t, \gamma_s \right\rangle = \left\langle \frac{d}{ds} \left( \gamma_s \times \frac{\nabla'}{ds} \gamma_s \right), \gamma_s \right\rangle \\ &= \left\langle \frac{d}{ds} \gamma_s \times \frac{\nabla'}{ds} \gamma_s + \gamma_s \times \frac{d}{ds} \left( \frac{\nabla'}{ds} \gamma_s \right), \gamma_s \right\rangle = \left\langle \frac{d}{ds} \gamma_s \times \frac{\nabla'}{ds} \gamma_s, \gamma_s \right\rangle \\ &= \left( \gamma_s, \frac{d}{ds} \gamma_s, \frac{\nabla'}{ds} \gamma_s \right) = \left( \frac{d}{ds} \gamma_s, \frac{\nabla'}{ds} \gamma_s, \gamma_s \right) \\ &= \left( \frac{\nabla'}{ds} \gamma_s + b \gamma, \frac{\nabla'}{ds} \gamma_s, \gamma_s \right) = \left( \frac{\nabla'}{ds} \gamma_s, \frac{\nabla'}{ds} \gamma_s, \gamma_s \right) \\ &= 0. \end{aligned}$$

Both  $a$  and  $b$  are some functions on  $\gamma(s, t)$ . So for a solution  $\gamma(s, t)$  of (2.7), we may assume that  $\gamma(\cdot, t)$  is parametrized by arc length for all  $t$ .

Next we will explain the geometric meaning of the evolution equation on the space of curves in  $S^3$ . Let  $(t, n, b)(\cdot, t)$  denote the Frenet frame of the curve  $\gamma(\cdot, t)$ . Since  $\gamma_s = t$ , and  $\frac{\nabla'}{ds} \gamma_s = \frac{\nabla'}{ds} t = kn$  then the curve flow (2.7) becomes:

$$(2.10) \quad \gamma_t = kt \times n = kb.$$

In other words, the curve flow (2.7) moves in the direction of binormal with curvature as its speed in  $S^3$ . In the following, we write equation (2.7) in terms of parallel frame  $(e_1, e_2, e_3)^T$ . Recall that if we rotate the Frenet frame  $(n, b)$  by an angle  $\beta(s, t)$  satisfy

$$(2.11) \quad \frac{d}{ds} \beta(s, t) = -\tau(s, t),$$



then

$$(2.12) \quad b = \sin \beta e_2 + \cos \beta e_3.$$

Hence

$$(2.13) \quad \gamma_t = kb = k(\sin \beta e_2 + \cos \beta e_3) = -k_2 e_2 + k_1 e_3.$$

In fact vortex filament equation (2.7) and NLS

$$q_t = i[q_{ss} + (\frac{1}{2}|q|^2 + 1)q]$$

shown the same motion equation. We will give the demonstration below.

Suppose  $\gamma(s, t)$  is a solution of (2.7), choose a parallel frame  $(e_1, e_2, e_3)^T(\cdot, t)$  for each curve  $\gamma(\cdot, t)$ . Let  $k_1(\cdot, t)$  and  $k_2(\cdot, t)$  denote the principal curvature of  $\gamma(\cdot, t)$  along  $e_2(\cdot, t), e_3(\cdot, t)$  respectively. Then we get

$$(2.14) \quad \frac{\nabla'}{ds} \begin{pmatrix} e_1 \\ e_2 \\ e_3 \end{pmatrix} = \begin{pmatrix} 0 & k_1 & k_2 \\ -k_1 & 0 & 0 \\ -k_2 & 0 & 0 \end{pmatrix} \begin{pmatrix} e_1 \\ e_2 \\ e_3 \end{pmatrix}.$$

We want to compute  $\frac{\nabla'}{dt}(e_1, e_2, e_3)^T$ , so we first compute  $\frac{\nabla'}{dt}e_1(\cdot, t)$ ,

$$(2.15) \quad \begin{aligned} \frac{\nabla'}{dt}e_1 &= \frac{\nabla'}{dt}t = \frac{\nabla'}{dt}\gamma_s = \frac{\nabla'}{ds}\gamma_t \\ &= \frac{\nabla'}{ds}(-k_2 e_2 + k_1 e_3) \\ &= -(k_2)_s e_2 + (-k_2) \frac{\nabla'}{ds}e_2 + (k_1)_s e_3 + k_1 \frac{\nabla'}{ds}e_3 \\ &= -(k_2)_s e_2 + (k_1)_s e_3 + (-k_2)(-k_1 e_1) + k_1(-k_2 e_1) \\ &= -(k_2)_s e_2 + (k_1)_s e_3. \end{aligned}$$

Since  $e_i(s, t)$  are orthogonal, there exists a function  $u(s, t)$  so that

$$(2.16) \quad \frac{\nabla'}{dt} \begin{pmatrix} e_1 \\ e_2 \\ e_3 \end{pmatrix} = \begin{pmatrix} 0 & -(k_2)_s & (k_1)_s \\ (k_2)_s & 0 & u \\ -(k_1)_s & -u & 0 \end{pmatrix} \begin{pmatrix} e_1 \\ e_2 \\ e_3 \end{pmatrix}.$$

Now, how to compute the function  $u(s, t)$  is the key step. If we can find  $u(s, t)$ , then we can get the coefficient matrix of  $\frac{\nabla'}{dt}(e_1, e_2, e_3)^T$ . Before computing  $u(s, t)$  we give some preparative knowledge.

(1): Since

$$(2.17) \quad \begin{aligned} \frac{\nabla'}{ds} \frac{\nabla'}{dt} - \frac{\nabla'}{dt} \frac{\nabla'}{ds} &= \nabla_{\frac{\partial}{\partial s}} \nabla_{\frac{\partial}{\partial t}} - \nabla_{\frac{\partial}{\partial t}} \nabla_{\frac{\partial}{\partial s}} - \nabla_{[\frac{\partial}{\partial s}, \frac{\partial}{\partial t}]} + \nabla_{[\frac{\partial}{\partial s}, \frac{\partial}{\partial t}]} \\ &= R(\frac{\partial}{\partial s}, \frac{\partial}{\partial t}) + \nabla_{[\frac{\partial}{\partial s}, \frac{\partial}{\partial t}]}, \end{aligned}$$

where  $\nabla_{[\frac{\partial}{\partial s}, \frac{\partial}{\partial t}]} = 0$ , so

$$(2.18) \quad \frac{\nabla' \nabla'}{dt ds} = \frac{\nabla' \nabla'}{ds dt} - R\left(\frac{\partial}{\partial s}, \frac{\partial}{\partial t}\right).$$

$R\left(\frac{\partial}{\partial s}, \frac{\partial}{\partial t}\right)$  is the curvature operator of  $S^3$ .

(2): Let  $M$  be a Riemann manifold of constant curvature  $K$ , for any  $X, Y, Z, W \in T_p M$  we have

$$(2.19) \quad R(X, Y, Z, W) = \langle R(X, Y)Z, W \rangle = -K(\langle X, Z \rangle \langle Y, W \rangle - \langle X, W \rangle \langle Y, Z \rangle).$$

This can refer to [3]. Since  $S^3$  is a space of constant curvature, and the sectional curvature  $K=1$ . So

$$(2.20) \quad \begin{aligned} & \langle R\left(\frac{\partial}{\partial s}, \frac{\partial}{\partial t}\right)e_2, e_3 \rangle \\ &= \langle R(e_1, -k_2 e_2 + k_1 e_3)e_2, e_3 \rangle \\ &= (-1)(\langle e_1, e_2 \rangle \langle -k_2 e_2 + k_1 e_3, e_3 \rangle - \langle e_1, e_3 \rangle \langle -k_2 e_2 + k_1 e_3, e_2 \rangle) \\ &= 0 \end{aligned}$$

similarly

$$(2.21) \quad \langle R\left(\frac{\partial}{\partial s}, \frac{\partial}{\partial t}\right)e_1, e_2 \rangle = k_2,$$

$$(2.22) \quad \langle R\left(\frac{\partial}{\partial s}, \frac{\partial}{\partial t}\right)e_1, e_3 \rangle = -k_1$$

by (2.18), (2.20), (2.21), (2.22) we get

$$(2.23) \quad \left\langle \frac{\nabla' \nabla'}{dt ds} e_2, e_3 \right\rangle = \left\langle \frac{\nabla' \nabla'}{ds dt} e_2, e_3 \right\rangle,$$

$$(2.24) \quad \left\langle \frac{\nabla' \nabla'}{dt ds} e_1, e_2 \right\rangle = \left\langle \frac{\nabla' \nabla'}{ds dt} e_1, e_2 \right\rangle - k_2,$$

$$(2.25) \quad \left\langle \frac{\nabla' \nabla'}{dt ds} e_1, e_3 \right\rangle = \left\langle \frac{\nabla' \nabla'}{ds dt} e_1, e_3 \right\rangle + k_1.$$

In the following we begin to compute  $u(s, t)$ ,

$$(2.26) \quad \begin{aligned} \left\langle \frac{\nabla'}{dt} \left( \frac{\nabla'}{ds} e_2 \right), e_3 \right\rangle &= \left\langle \frac{\nabla'}{dt} (-k_1 e_1), e_3 \right\rangle \\ &= \left\langle -(k_1)_t e_1 - k_1 \frac{\nabla'}{dt} e_1, e_3 \right\rangle \\ &= \left\langle -k_1 (-(k_2)_s e_2 + (k_1)_s e_3), e_3 \right\rangle \\ &= -k_1 (k_1)_s \end{aligned}$$

similarly

$$(2.27) \quad \left\langle \frac{\nabla'}{ds} \left( \frac{\nabla'}{dt} e_2 \right), e_3 \right\rangle = (k_2)_s k_2 + u_s,$$

by (2.23)

$$(2.28) \quad -k_1(k_1)_s = (k_2)_s k_2 + u_s.$$

So

$$(2.29) \quad u = -\frac{1}{2}(k_1^2 + k_2^2) + c(t),$$

for some smooth function  $c(t)$ . Remember that for each fixed  $t$ , we can rotate  $(e_2, e_3)(\cdot, t)$  by a constant angle  $\theta(t)$  to another parallel normal frame  $(v_2, v_3)(\cdot, t)$  of  $\gamma(\cdot, t)$ . If we choose  $\theta(t)$  so that  $\theta'(t) = -c(t)$ , then the new parallel frame satisfies

$$(2.30) \quad \frac{\nabla'}{dt} \begin{pmatrix} e_1 \\ v_2 \\ v_3 \end{pmatrix} = \begin{pmatrix} 0 & -(\tilde{k}_2)_s & (\tilde{k}_1)_s \\ (\tilde{k}_2)_s & 0 & -\frac{\tilde{k}_1^2 + \tilde{k}_2^2}{2} \\ -(\tilde{k}_1)_s & \frac{\tilde{k}_1^2 + \tilde{k}_2^2}{2} & 0 \end{pmatrix} \begin{pmatrix} e_1 \\ v_2 \\ v_3 \end{pmatrix}.$$

So we have proved the first part of the following theorem:

**Theorem.** *Suppose  $\gamma(s, t)$  is a solution of the vortex filament equation (2.7) and  $|\gamma(s, 0)| = 1$  for all  $s$ . Then*

- (1) *there exists a parallel normal frame  $(e_1, e_2, e_3)^T(\cdot, t)$  for each curve  $\gamma(\cdot, t)$  so that*

$$(2.31) \quad \frac{\nabla'}{ds} \begin{pmatrix} e_1 \\ e_2 \\ e_3 \end{pmatrix} = \begin{pmatrix} 0 & k_1 & k_2 \\ -k_1 & 0 & 0 \\ -k_2 & 0 & 0 \end{pmatrix} \begin{pmatrix} e_1 \\ e_2 \\ e_3 \end{pmatrix},$$

$$(2.32) \quad \frac{\nabla'}{dt} \begin{pmatrix} e_1 \\ e_2 \\ e_3 \end{pmatrix} = \begin{pmatrix} 0 & -(k_2)_s & (k_1)_s \\ (k_2)_s & 0 & -\frac{k_1^2 + k_2^2}{2} \\ -(k_1)_s & \frac{k_1^2 + k_2^2}{2} & 0 \end{pmatrix} \begin{pmatrix} e_1 \\ e_2 \\ e_3 \end{pmatrix},$$

where  $k_1(\cdot, t)$  and  $k_2(\cdot, t)$  are the principal curvatures of  $\gamma(\cdot, t)$  along  $e_2(\cdot, t)$  and  $e_3(\cdot, t)$  respectively.

- (2)  $q = k_1 + ik_2$  is a solution of the NLS

$$q_t = i[q_{ss} + \left(\frac{1}{2}|q|^2 + 1\right)q].$$

*Proof.* We have proved (1). For (2), we use (2.31),(2.32) to compute the evolution of  $(k_1)_t$  and  $(k_2)_t$ .

$$\begin{aligned}
 (2.33) \quad (k_1)_t &= \frac{\nabla'}{dt} k_1 = \frac{\nabla'}{dt} \left\langle \frac{\nabla'}{ds} e_1, e_2 \right\rangle \\
 &= \left\langle \frac{\nabla'}{dt} \frac{\nabla'}{ds} e_1, e_2 \right\rangle + \left\langle \frac{\nabla'}{ds} e_1, \frac{\nabla'}{dt} e_2 \right\rangle \\
 &= \left\langle \frac{\nabla'}{ds} \frac{\nabla'}{dt} e_1, e_2 \right\rangle - k_2 + \langle k_1 e_2 + k_2 e_3, (k_2)_s e_1 - \frac{k_1^2 + k_2^2}{2} e_3 \rangle \\
 &= \left\langle \frac{\nabla'}{ds} (- (k_2)_s e_2 + (k_1)_s e_3), e_2 \right\rangle - k_2 - k_2 \frac{k_1^2 + k_2^2}{2} \\
 &= - (k_2)_{ss} - k_2 - k_2 \frac{k_1^2 + k_2^2}{2}
 \end{aligned}$$

similarly

$$(2.34) \quad (k_2)_t = (k_1)_{ss} + k_1 + k_1 \frac{k_1^2 + k_2^2}{2}.$$

Therefore

$$\begin{aligned}
 (2.35) \quad q_t &= (k_1)_t + i(k_2)_t \\
 &= - (k_2)_{ss} - k_2 - k_2 \frac{k_1^2 + k_2^2}{2} + i(k_1)_{ss} + ik_1 + ik_1 \frac{k_1^2 + k_2^2}{2} \\
 &= i[q_{ss} + (\frac{1}{2}|q|^2 + 1)q].
 \end{aligned}$$

□

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