

# Electrical Properties of ZPCCT-based Varistor Ceramics

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The microstructure and electrical properties of Zn-Pr-Co-Cr-Tb oxide-based varistors were investigated for different Tb<sub>4</sub>O<sub>7</sub> amounts. As the Tb<sub>4</sub>O<sub>7</sub> amount increased, the average grain size decreased from 7.7 to 4.8 μm and the sintered density increased from 5.73 to 5.84 g/cm<sup>3</sup>. As the Tb<sub>4</sub>O<sub>7</sub> amount increased, the varistor voltage increased from 280.9 to 715.8 V/mm and the nonlinear coefficient increased from 26.4 to 44.4. It is assumed that these varistors can be applied for high power with compact size.

*Keywords* : Microstructure, Tb<sub>4</sub>O<sub>7</sub>, Electrical properties, Varistors

## 1. INTRODUCTION

Zinc oxide doped with several different metal oxides is smart electroceramics showing nonlinear electrical properties, which exhibit abruptly increasing current with increasing voltage. That is, this means the increase of voltage gives rise to the decrease of impedance. This nonlinear of current-voltage properties is because of the presence of a double Schottky barrier (DSB) formed at active grain boundaries containing many trap states. Owing to highly nonlinear properties, these electroceramic devices are used widely in the field of overvoltage protection systems from electronic circuits to electric power systems[1,2]. Zinc oxide nonlinear electroceramics are generally divided into two categories, called Bi<sub>2</sub>O<sub>3</sub>-based and Pr<sub>6</sub>O<sub>11</sub>-based ceramics, in terms of nonlinear-forming oxides (VFO). ZnO-Bi<sub>2</sub>O<sub>3</sub>-based ceramics have been mainly studied in different aspects since ZnO non-ohmic ceramics were discovered. Although ZnO-Bi<sub>2</sub>O<sub>3</sub>-based ceramics show excellent non-ohmic properties, Bi<sub>2</sub>O<sub>3</sub> reacts easily with some or many, but not all, of the metals used in preparing multilayer chip nonlinear ceramics, and it destroys the multilayer structure[3]. And it is reported to have an additional insulating spinel phase, which does not play any role in electrical conduction[3]. Recently, ZnO-Pr<sub>6</sub>O<sub>11</sub>-based ceramics have been studied in order to improve a few drawbacks[3] associated with Bi<sub>2</sub>O<sub>3</sub>[4-14].

Nahm et al. reported that ZnO-Pr<sub>6</sub>O<sub>11</sub>-CoO-Cr<sub>2</sub>O<sub>3</sub>-REO (REO = Er, Y, Dy, La)-based ceramics have highly nonlinear properties[7-14]. To develop the nonlinear electroceramics of high performance, it is very important to comprehend the effects of the additives on nonlinear properties. The objective of this paper is to investigate

the effect of Tb<sub>4</sub>O<sub>7</sub> addition on the microstructure and nonlinear properties of ZPCCT (ZnO-Pr<sub>6</sub>O<sub>11</sub>-CoO-Cr<sub>2</sub>O<sub>3</sub>-Tb<sub>4</sub>O<sub>7</sub>)-based ceramics.

## 2. EXPERIMENTAL PROCEDURE

### 2.1 Sample preparation

Reagent-grade raw materials were prepared for ZnO varistors with composition (98.0-x) mol% ZnO+0.5 mol% Pr<sub>6</sub>O<sub>11</sub>+1.0 mol% CoO+0.5 mol% Cr<sub>2</sub>O<sub>3</sub>+x mol% Tb<sub>4</sub>O<sub>7</sub> (x = 0.0, 0.25, 0.5, 0.75, 1.0). Raw materials were mixed by ball milling with zirconia balls and acetone in a polypropylene bottle for 24 h. The mixture was dried at 120°C for 12 h and calcined in air at 750°C for 2 h. The calcined mixture was pulverized using an agate mortar/pestle and after 2 wt% polyvinyl alcohol (PVA) binder addition, granulated by sieving 200-mesh screen to produce starting powder. The powder was uniaxially pressed into discs of 10 mm in diameter and 2 mm in thickness at a pressure of 800 kg/cm<sup>2</sup>. The discs were covered with raw powder in alumina crucible, sintered at 1330°C for 1 h. The sintered samples were lapped and polished to 1.0 mm thickness. The size of the final samples was about 8 mm in diameter and 1.0 mm in thickness. Silver paste was coated on both faces of samples and ohmic contact of electrodes was formed by heating at 600°C for 10 min. The electrodes were 5 mm in diameter.

### 2.2 Microstructure examination

The either surface of samples was lapped and ground with SiC paper and polished with Al<sub>2</sub>O<sub>3</sub> powders to a mirror-like surface. The polished samples were thermally

etched at 1100 °C for 30 min. The surface microstructure was examined by a scanning electron microscope (SEM, Hitachi S2400, Japan). The average grain size ( $d$ ) was determined by the lineal intercept method as follows:

$$d = \frac{1.56L}{MN} \quad (1)$$

where  $L$  is the random line length on the micrograph,  $M$  is the magnification of the micrograph, and  $N$  is the number of the grain boundaries intercepted by lines[15]. The crystalline phases were identified by an X-ray diffractometry (XRD, Rigaku D/max 2100, Japan) with  $\text{CuK}\alpha$  radiation. The sintered density ( $\rho$ ) of ceramics was measured by the Archimedes method.

### 2.3 Electrical measurement

The V-I characteristics of the varistors were measured using a high voltage source measure unit (Keithley 237). The varistor voltage ( $V_{1\text{mA}}$ ) was measured at a current

density of 1.0 mA/cm<sup>2</sup> and the leakage current ( $I_L$ ) was measured at 0.80  $V_{1\text{mA}}$ . In addition, the nonlinear coefficient ( $\alpha$ ) was determined from the following expression.

$$\alpha = \frac{\log J_2 - \log J_1}{\log E_2 - \log E_1} \quad (2)$$

where  $J_1 = 1.0$  mA/cm<sup>2</sup>,  $J_2 = 10$  mA/cm<sup>2</sup>, and  $E_1$  and  $E_2$  are the electric fields corresponding to  $J_1$  and  $J_2$ , respectively.

## 3. RESULTS AND DISCUSSION

Figure 1 shows the SEM micrographs of ZPCCT-based ceramics for different  $\text{Tb}_4\text{O}_7$  amounts. The microstructure consisted of primary phase ZnO grain (blackish), and secondary phase intergranular layer (whitish), which

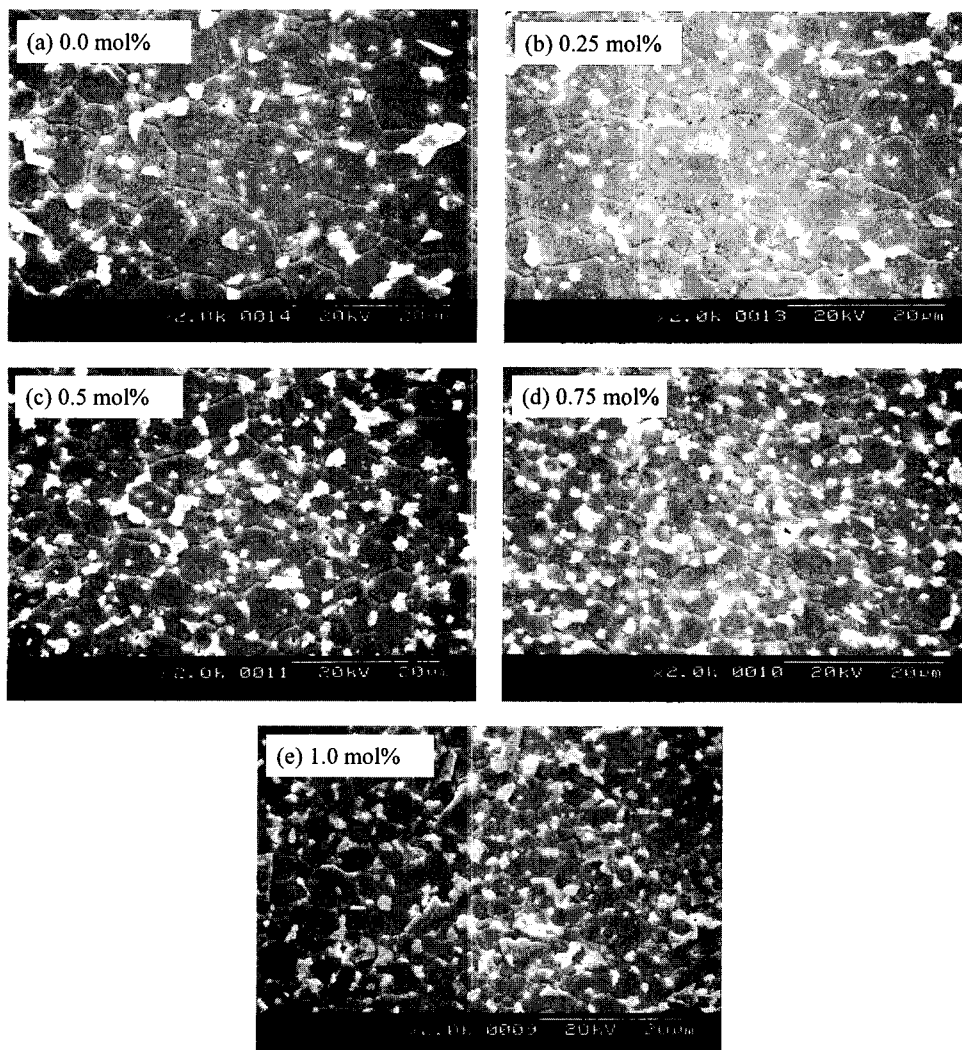


Fig. 1. SEM micrographs of ZPCCT-based varistor ceramics for different  $\text{Tb}_4\text{O}_7$  amounts.

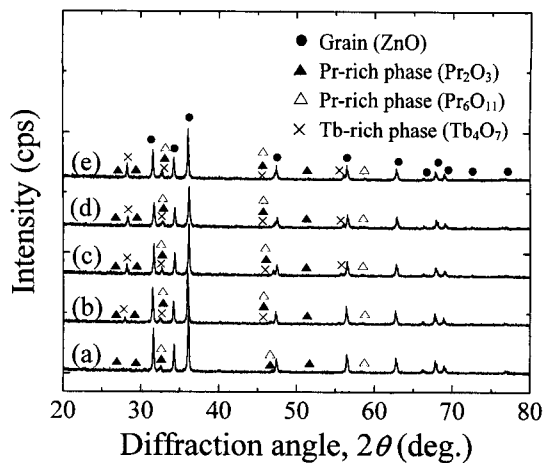


Fig. 2. XRD patterns of ZPCCT-based varistor ceramics for different  $Tb_4O_7$  amounts; (a) 0.0 mol%, (b) 0.25 mol%, (c) 0.5 mol%, (d) 1.0 mol%, and (e) 2.0 mol%.

are Pr- and Tb-rich phases as determined by XRD analysis, as shown in Fig. 2. Fig. 3 shows a distribution of Tb by EDX. No Tb peak into ZnO grain was found within the EDX detection limit. It is assumed that this is attributed to the ionic radius (0.92 Å in Tb) difference for Zn. Added  $Tb_4O_7$  as well as  $Pr_6O_{11}$  was segregated to grain boundaries and nodal points, and Pr- and Tb-oxide were found to coexist in the grain boundaries and the nodal points as if they were a single phase.

Figure 4 shows the average grain size and sintered density of the ZPCCT-based ceramics as a function of  $Tb_4O_7$  amount. The sintered density linearly increased in the range of 5.73 to 5.84 g/cm<sup>3</sup> corresponding to 99.1% to 101.0% of TD (5.78 g/cm<sup>3</sup> in ZnO) with the increase of  $Tb_4O_7$  amount. It shows very high density as much as no porosity through the surface microstructure. Nonlinear electroceramics added with a few rare earth oxides (REO) hardly provide both high sintered density and highly nonlinear[9-12]. Therefore, the high sintered density is very important for high energy capability varistors. The average grain size was greatly linearly decreased from 7.7 to 4.8 μm. Therefore, the densification is found to be enhanced by the addition of  $Tb_4O_7$ . The detailed microstructure parameters are summarized in Table 1.

Figure 5 shows the  $E$ - $J$  characteristics of the ZPCCT-based ceramics for different  $Tb_4O_7$  amounts. The curves show the conduction characteristics divide into two regions: linear region before breakdown field and nonlinear region after breakdown field. The sharper the knee of the curves between the two regions, the better the nonlinear properties. On adding more  $Tb_4O_7$ , the knee gradually becomes more pronounced and the nonlinear properties are enhanced. Therefore, the addition

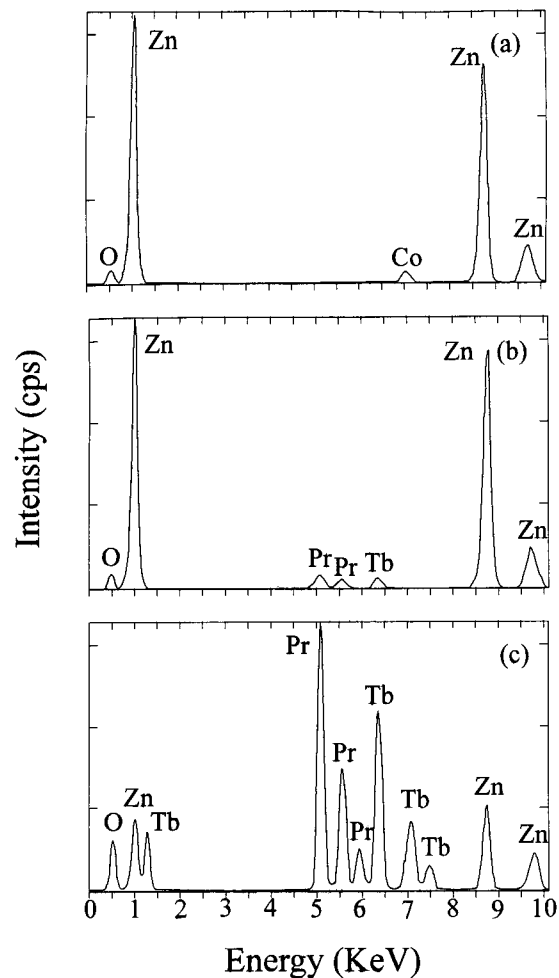


Fig. 3. EDX analysis of ZPCCT-based varistor ceramics for different  $Tb_4O_7$  amounts; (a) ZnO grain, (b) Grain boundary, (c) Intergranular layer.

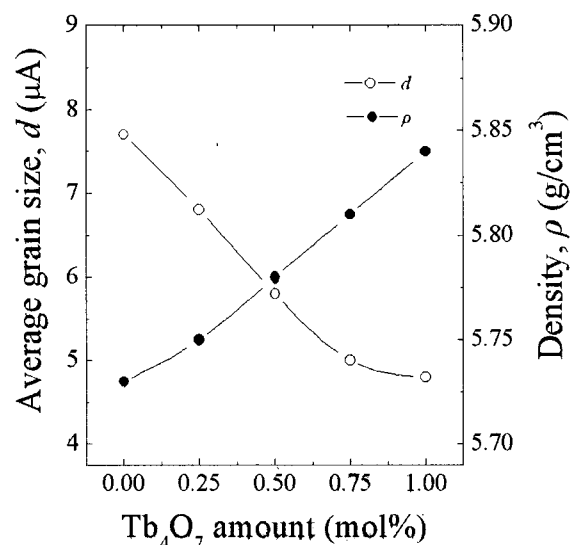


Fig. 4. Average grain size and sintered density as a function of  $Tb_4O_7$  amount.

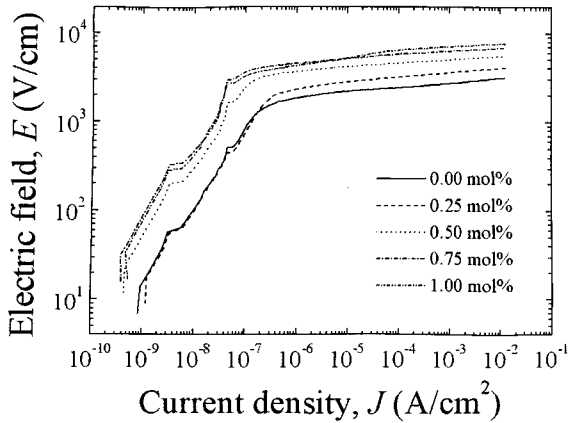


Fig. 5.  $E$ - $J$  characteristics of ZPCCT-based varistors for different  $Tb_4O_7$  amounts.

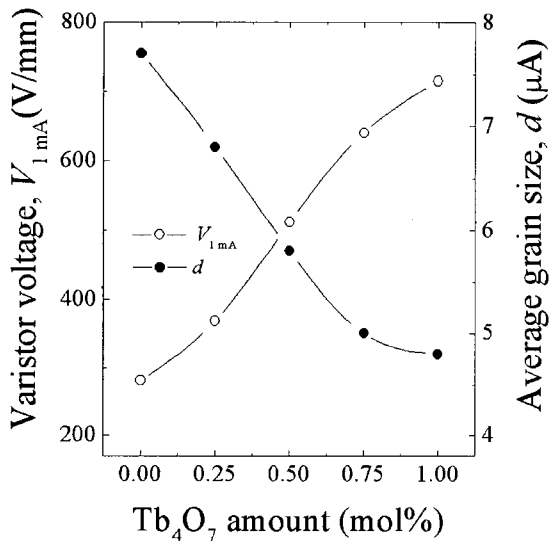


Fig. 6. Varistor voltage and average grain size as a function of  $Tb_4O_7$  amount.

of  $Tb_4O_7$  seems to remarkably enhance nonlinear properties. The varistor voltage ( $V_{1mA}$ ) greatly increased from 280.9 to 715.8 V/mm with the increase of  $Tb_4O_7$  amount. The samples added with  $Tb_4O_7$ , more than 0.5 mol%, provide a very high varistor voltage of 500 to 700 V/mm per unit thickness. This is very important for high voltage nonlinear ceramics with compact size. The increase of  $V_{1mA}$  related to  $Tb_4O_7$  amount can be explained by the increase in the number of grain boundaries owing to the decrease in the average ZnO grain size, as shown in Fig. 6. It can be seen that the relation between varistor voltage and average grain size is totally opposite.

Figure 7 shows the variation of the nonlinear coefficient ( $\alpha$ ) and the leakage current ( $I_L$ ) of the ZPCCT-based ceramics as a function of  $Tb_4O_7$  amount. The  $\alpha$  value of

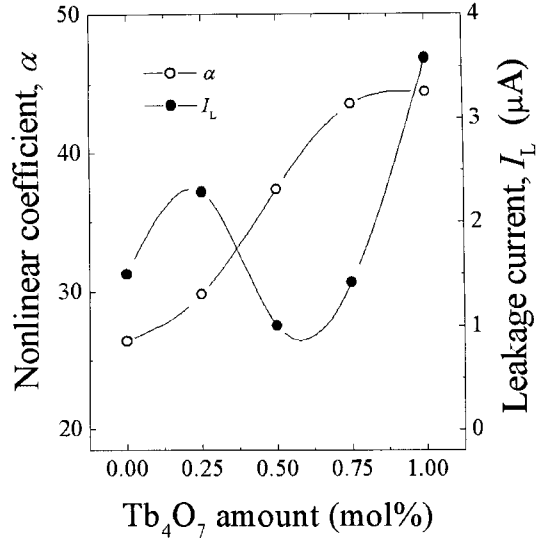


Fig. 7. Nonlinear coefficient and leakage current as a function of  $Tb_4O_7$  amount.

$Tb_4O_7$ -undoped varistors was 26.4 and 0.25 mol%  $Tb_4O_7$ -doped varistors slightly increased up to only 29.8 in  $\alpha$  value. The varistors doped with  $Tb_4O_7$  more than 0.5 mol% linearly increased in the range of 37.4 to 44.4 with the increase of  $Tb_4O_7$  amount. On the other hand, the  $I_L$  value of  $Tb_4O_7$ -undoped varistors was only 1.5  $\mu A$ . When the  $Tb_4O_7$ -amount is small, less than 0.25 mol%, the  $I_L$  value is higher than that of  $Tb_4O_7$ -undoped varistors. As the  $Tb_4O_7$  amount continually increased, the  $I_L$  value decreased. When the  $Tb_4O_7$  amount is more than 0.5 mol%, the  $I_L$  value decreased again. On the whole, the variation tendency of the  $I_L$  value with the increased of  $Tb_4O_7$  amount was very complex unlike  $\alpha$  value. Any way, it was found that the addition of  $Tb_4O_7$  to the quaternary system  $ZnO-Pr_6O_{11}-CoO-Cr_2O_3$  improves the nonlinear properties by increasing the nonlinear coefficient.

#### 4. CONCLUSION

The microstructure and electrical properties of varistors were investigated for different  $Tb_4O_{11}$  amount. The sintered ceramics increased in the range of 5.73-5.84  $g/cm^3$  with the increase of  $Tb_4O_{11}$  amount. The average grain size decreased from 7.7 to 4.8  $\mu m$  with the increase of  $Tb_4O_{11}$  amount. The nonlinear coefficient increased from 26.4 to 44.4 with the increase of  $Tb_4O_{11}$  amount. Conclusively, it is assumed that these varistors can be applied for high power with compact size.

#### ACKNOWLEDGEMENT

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## REFERENCES

- [1] L. M. Levinson and H. R. Philipp, "Zinc oxide varistor-a review", *Amer. Ceram. Soc. Bull.*, Vol. 65, No. 4, p. 639, 1986.
- [2] T. K. Gupta, "Application of zinc oxide varistor", *J. Amer. Ceram. Soc.*, Vol. 73, No. 7, p. 1817, 1990.
- [3] Y. S. Lee and T. Y. Tseng, "Phase identification and electrical properties in ZnO-glass varistors", *J. Amer. Ceram. Soc.*, Vol. 75, No. 6, p. 1636, 1992.
- [4] A. B. Alles and V. L. Burdick, "The effect of liquid-phase sintering on the properties of  $\text{Pr}_6\text{O}_{11}$ -based ZnO varistors", *J. Appl. Phys.*, Vol. 70, No. 11, p. 6883, 1991.
- [5] Alles, A. B., Puskas, R., Callahan, G., and Burdick, V. L., "Compositional effect on the liquid-phase sintering of praseodymium oxides-based ZnO varistors", *J. Am. Ceram. Soc.*, Vol. 76, No. 8, p. 2098, 1993.
- [6] Y.-S. Lee, K.-S. Liao, and T.-Y. Tseng, "Microstructure and crystal phases of praseodymium in zinc oxides varistors", *J. Amer. Ceram. Soc.*, Vol. 79, No. 9, p. 2379, 1996.
- [7] C.-W. Nahm, "The nonlinear properties and stability of ZnO- $\text{Pr}_6\text{O}_{11}$ -CoO- $\text{Cr}_2\text{O}_3$ - $\text{Er}_2\text{O}_3$  ceramic varistors", *Mater. Lett.*, Vol. 47, No. 4, 3 p. 182, 2001.
- [8] C.-W. Nahm and J.-S. Ryu, "Influence of sintering temperature on varistor characteristics of ZPCCE-based ceramics", *Mater. Lett.*, Vol. 53, No. 1-2, p. 110, 2002.
- [9] C.-W. Nahm, "Microstructure and electrical properties of  $\text{Y}_2\text{O}_3$  doped ZnO- $\text{Pr}_6\text{O}_{11}$ -based varistor", *Mater. Lett.*, Vol. 57, No. 7, p. 1317, 2003.
- [10] C.-W. Nahm and B.-C. Shin, "Highly stable electrical properties of ZnO- $\text{Pr}_6\text{O}_{11}$ -CoO- $\text{Cr}_2\text{O}_3$ - $\text{Y}_2\text{O}_3$ -based varistor ceramics", *Mater. Lett.*, Vol. 57, No. 7, p. 1322, 2003.
- [11] C.-W. Nahm, "Microstructure and electrical properties of  $\text{Dy}_2\text{O}_3$ -based ZnO- $\text{Pr}_6\text{O}_{11}$ -based varistor ceramics", *Mater. Lett.*, Vol. 58, No. 17-18, p. 2252, 2004.
- [12] C.-W. Nahm and B.-C. Shin, "Effect of sintering time on electrical characteristics and DC accelerated aging behaviors of Zn-Pr-Co-Cr-Dy oxide-based varistors", *J. Mater. Sci.: Mater. Electron.*, Vol. 16, No. 11-12, p. 725, 2005.
- [13] C.-W. Nahm, "Effect of sintering temperature on microstructure and electrical properties of Zn-Pr-Co-Cr-La oxide-based varistors", *Mater. Lett.*, Vol. 60, No. 28, p. 3394, 2006.
- [14] C.-W. Nahm, "Effect of  $\text{La}_2\text{O}_3$  addition on electrical characteristics of  $\text{Pr}_6\text{O}_{11}$ -based ZnO varistors", *Trans. EEM.*, Vol. 7, No. 3, p. 123, 2006.
- [15] J. C. Wurst and J. A. Nelson, "Lineal intercept technique for measuring grain size in two-phase polycrystalline ceramics", *J. Amer. Ceram. Soc.*, Vol. 55, No. 97-12, p. 109, 1972.