# Influence of Thickness on the Degree of Cure of Composite Resin Core Material

# Pyoung-Cheol Kwon<sup>1</sup>, Jeong-Won Park<sup>2\*</sup>

<sup>1</sup>Department of Conservative Dentistry, School of Dentistry, Kyungpook National University <sup>2</sup>Department of Conservative Dentistry, College of Dentistry, Yonsei University

### **ABSTRACT**

The purpose of this study was to investigate the influence of thickness on the degree of cure of dual-cured composite core.

2, 4, 6, 8 mm thickness Luxacore Dual and Luxacore Self (DMG Inc, Hamburg, Germany) core composites were cured by bulk or incremental filling with halogen curing unit or self-cure mode. The specimens were stored at 37°C for 24 hours and the Knoop's hardness of top and bottom surfaces were measured.

The statistical analysis was performed using ANOVA and Tukey's test at p = 0.05 significance level.

In self cure mode, polymerization is not affected by the thickness. In Luxacore dual, polymerization of the bottom surface was effective in 2, 4 and 6 (incremental) mm specimens. However the 6 (bulk) and 8 (bulk, incremental) mm filling groups showed lower bottom/top hardness ratio (p  $\langle$  0.05). Within the limitation of this experiment, incremental filling is better than bulk filling in case of over 4 mm depth, and bulk filling should be avoided. [J Kor Acad Cons Dent 31(5):352-358, 2006]

Key words: Dual cure resin core, Microhardness, Polymerization

Received 2006.4.6., revised 2006.7.28., accepted 2006.8.24.

# I. INTRODUCTION

Composite resin restoratives have been widely applied in clinical dentistry and replaced amalgam since their introduction<sup>1)</sup>. As a core material, the use of composite is more common nowadays. Composite cores can be classified in three groups by their curing mode. Self-cured type is conve-

nient to build up the core and reduces the chairtime, while it takes a long time to have hardness enough to prepare crown. Light-cured type has advantages to maximize working time and minimize setting time, however, there is a possibility of incomplete polymerization in deep cavities. Recently, dual-cured type that combines the advantages of self-cured and light-cured composites has been introduced and their use has been increased.

Many clinicians used dual-cured type composite core materials in a bulk filling technique. But one of the limitations of these materials is that a hard-top surface is not an indication of adequate polymerization throughout the depth of the

Department of Conservative Dentistry
College of Dentistry, Yonsei University
Youngdong Severance Dental Hospital
146-92 Dogok-dong Gangnam-gu, Seoul, 135-720, S.Korea
Tel: 82-2-2019-1350 Fax: 82-2-3463-4052
E-mail: pjw@yumc.yonsei.ac.kr

<sup>\*</sup> Corresponding Author: Jeong-Won Park

restoration in a deep cavity<sup>2-6)</sup>. The effectiveness of polymerization or depth of cure of light-activated composites is vital to ensure optimum physiomechanical properties<sup>1,2,4,7)</sup>. It depends not only the chemistry of the material, but also the filler particle type, size, and quantity<sup>1-3)</sup>. In addition, polymerization is dependent on the effectiveness of the radiation sources, including spectral distribution, intensity, exposure time, and alignment of the light-tip guide<sup>1,2,4)</sup>.

The effectiveness of polymerization may be assessed directly or indirectly 1-4.8). Fourier-transformed infrared spectroscopy or Raman spectroscopy is the most commonly used method directly to measure the degree of conversion of resin or composite<sup>1,2,7)</sup>. However, this method is complex, expensive and time consuming<sup>1-4,8)</sup>. Indirect methods have included scraping, visual and surface hardness<sup>1-4,9)</sup>. DeWald and Ferracane compared four commonly used methods for evaluating depth of cure in light-activated composites<sup>1-3,10)</sup>. They found that visual and scraping methods correlated well, but severely overestimated depth of cure as compared with hardness testing or degree of conversion1-3). Hardness testing appears to be the most popular indirect method for investigating factors that influence effectiveness of polymerization because of the relative simplicity of the method and a good correlation between the results of hardness and infrared spectroscopy experiments<sup>2,3)</sup>.

According to a series of recent researches with dual-cured resin cements, enough polymerization occurs at top surface, but did not necessarily occur at bottom surface when light did not reach bottom<sup>6)</sup>. Also, degree of conversion was different according to cure mode in dual-cured resin cements<sup>6)</sup>. In clinical cases of deep cavities, bulk filling with dual-cured resin doesn't show exactly whether polymerization is completed or not in bottom surface.

Therefore the purpose of this study was to investigate the influence of thickness on the degree of cure when bulk filling was done with dual-cured composite core and whether there was enough polymerization occurred at the deep bottom surface by self cure ability.

## II. MATERIALS AND METHODS

Two composites core materials, Luxacore Dual and Luxacore Self (DMG Inc, Hamburg, Germany) of shade blue were chosen (Table 1).

The composite restoratives under test were placed in Teflon mold 10 mm in diameter and cylindrical cavities 2, 4, 6, 8 mm in depth<sup>4)</sup>. The material placed in the mold cavity was confined between opposing cellulose acetate strips (KerrHawe striproll, Switzerland). A glass slide was placed on the mold and excess material was extruded out by applying pressure. The materials were irradiated from the top surface through the glass slide

Table 1. Components of Luxacore automix dual

Component	%	
Filler		
Barium glass, silan		
Pyrogenic silica, silan		
Total inorganic filler content	₹ 72	
Dental resins	< 26	
Bis-GMA		
Urethane dimethacrylate (UDMA)		
Dodecanediol dimethacrylate (DDDMA)		
Hexanediol dimethacrylate (HDDMA)		
Starter system, additives, pigments	⟨ 2.5	

memod					
Group	Material type	Thickness (mm)	Filling method	Curing method	Curing time
S	Self	2, 4, 6, 8	Bulk	Self	4 min
DS	Dual	2, 4, 6, 8	Bulk	Self	30 min
D2	Dual	2	Bulk	Light	20 sec
D4	Dual	4	Bulk	Light	40 sec
DI6	Dual	6(4 + 2)	Incremental	Light	$40 + 20 \sec$
DI8	Dual	8(4 + 4)	Incremental	Light	$40 + 40 \sec$
DB6	Dual	6	Bulk	Light	60 sec
DB8	Dual	8	Bulk	Light	80 sec

Table 2. Experimental groups followed by the material type, mold thickness, filling method and curing method

as recommended by the manufacturer with a halogen light curing unit (VIP, BISCO Inc, Schaumburg, IL, U. S. A.) at 500 mW/cm².

In Luxacore dual, the curing time was decided by the thickness of composite, e.g., 20 seconds in 2 mm thick group and 40 seconds in 4 mm group. In 6 mm thick specimens, according to manufacturers instruction, lower 4 mm incremental layer was cured for 40 seconds then upper 2 mm was added and cured for 20 seconds more (total 60 sec). In 8 mm thick specimens, lower and upper 4 mm layers were cured for 40 seconds each.

In bulk filling groups, 6 mm thick specimens were cured for 60 seconds and 8 mm specimens for 80 seconds at a time for recognizing the effect of self curing in the deep cavity with diminished light. As a control group of self-cure mode of Luxacore Dual, three of each 2, 4, 6, 8 mm specimens were made and cured in a dark room for 30 minutes. In Luxacore Self groups, they were filled with a bulk placement and cured for 4 minutes before removal.

After cured, the specimens were removed from the mold and stored in the dark water bath at 37 °C for 24 hours and the top and bottom surfaces of each specimen were minimally polished with a #2000 sandpaper<sup>5)</sup>. The specimens were positioned centrally beneath the indentor of a digital microhardness tester (Future-Tech Corp, Tokyo, Japan) to assess Knoop's hardness (KHN) of the top and bottom surfaces. A 25 gf load was applied through the indentor with a dwell time of 10 sec-

onds. Ten specimens were made for each material and cavity-depth combination. For each upper and bottom surface, three readings were taken at three points.

Mean KHN at the top and bottom surfaces represented the hardness of each sample and the hardness ratio (KHN of Bottom/Top) was calculated. The statistical analysis was performed using one-way analysis of variance (ANOVA) and Tukey's test at a p = 0.05 significance level.

## II. RESULTS

The mean KHN of Luxacore self and dual for the different thickness, curing and filling groups was shown in Tables 3, 4 and 5. For Luxacore self and Luxacore dual-self curing mode groups, there was no significant difference in KHN among the different depths at the top & bottom surfaces (Table 3 and 4), and they are analyzed as one groups (S and DS) in Table 5. S and DS groups showed lower hardness value than the other groups at top surface. At the bottom surface, they had lower hardness value than D2, D4, D16, and D18 groups but same with DB6 and higher than DB8.

The hardness ratios of the restoratives at the different cavity depths are shown in Figure. DI8, DB6 and DB8 groups showed ratio lower than 0.8, it means polymerization at the bottom surface is not sufficient.

Table 3. Mean KHN of Luxacore self for different thickness

 $(mean \pm SD)$ 

Thickness	Number	Top	Bottom	Hardness ratio
2	10	$29.4 \pm 2.2$	$28.5 \pm 2.3$	$0.97 \pm 0.02$
4	10	$28.7\pm0.5$	$29.1 \pm 1.9$	$1.01 \pm 0.07$
6	10	$28.5 \pm 1.2$	$27.9 \pm 1.9$	$0.98 \pm 0.04$
8	10	$28.5 \pm 0.7$	$28.3 \pm 1.1$	$0.99 \pm 0.03$

Table 4. Mean KHN of Luxacore dual in self cure mode for different thickness

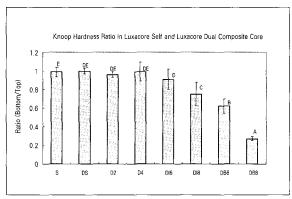
(mean ± SD)

Thickness	Number	Тор	Bottom	Hardness ratio
2	3	$30.5 \pm 0.7$	$29.7 \pm 0.2$	$0.97 \pm 0.03$
4	3	$28.9 \pm 0.3$	$29.5 \pm 1.0$	$1.02 \pm 0.03$
6	3	$29.4 \pm 0.6$	$29.7 \pm 0.9$	$1.01 \pm 0.05$
8	3	$29.0 \pm 0.6$	$29.1 \pm 0.4$	$1.00 \pm 0.01$

Table 5. Mean KHN of Material and Hardness ratio

Groups	Number	$\operatorname{Top}$	Bottom	Ratio
S	40	$28.8 \pm 1.32^{\text{A}}$	$28.4 \pm 1.82^{\text{B}}$	$0.99 \pm 0.05^{\mathrm{E}}$
DS	12	$29.5\pm0.81^{\rm A}$	$29.5 \pm 0.68^{\text{B}}$	$1.00 \pm 0.03^{\text{DE}}$
D2	10	$50.6 \pm 1.11^{\text{B}}$	$48.4 \pm 1.52^{\text{DE}}$	$0.96\pm0.03^{\mathrm{DE}}$
D4	10	$52.5\pm6.41^{\text{BC}}$	$51.9\pm6.02^{\scriptscriptstyle E}$	$0.99\pm0.10^{\text{DE}}$
DI6	10	$49.7 \pm 3.28^{\text{B}}$	$45.0 \pm 5.40^{\text{cd}}$	$0.91 \pm 0.11^{\scriptscriptstyle \mathrm{D}}$
DI8	10	$56.5 \pm 5.66^{\circ}$	$42.3 \pm 6.39^{\circ}$	$0.75 \pm 0.13^{\circ}$
DB6	10	$50.6 \pm 1.17^{\text{B}}$	$31.2 \pm 3.37^{\text{B}}$	$0.62\pm0.08^{\scriptscriptstyle B}$
DB8	10	$51.4 \pm 0.97^{\text{B}}$	$14.0 \pm 0.84^{\text{A}}$	$0.27 \pm 0.02^{A}$

The same superscript at each surface and ratio indicates no significant difference by Tukey's studentized range test (p  $\rangle$  0.05).



**Figure 1.** The Knoop hardness ratios between the top and bottom surface of each experimental groups (p  $\langle 0.05 \rangle$ ). The same superscript over the bar indicates no significant difference by Tukey's studentized range test (p  $\rangle$  0.05).

# IV. DISCUSSION

Bulk placement of composites may be anticipated in deep cavities and the restorations of endodontically treated teeth if composite resin is used as an amalgam substitute<sup>2</sup>. It is, however, difficult for visible light to penetrate thick layers of composites, particularly those with darker shades<sup>2,8</sup>. Filler particles, colorants, and pores scatter visible light and reduce curing efficacy<sup>2</sup>. The effective intensity of light for curing is dependent on the intensity produced by the curing unit, the distance of the light curing tip from the surface of the material, and internal light scattering within the composite<sup>2,3,11</sup>. The manufacturers of

the Luxacore composites claimed that their products were formulated to be placed in bulk increments of 4 mm with a single 40-second visible-light exposure.

Bulk placement of composites may generate higher internal stresses in the material, more loss of marginal integrity and polymerization shrinkage as the volume of composite to be polymerized became larger. The degree to which light-activated composites polymerize is proportional to the amount of light to which they are exposed 1.2.13. At the upper surface of the composites, where no overlying composites interfere with light transmission, it has been found that even a curing source with relatively low intensity can cure the resin matrix to an extent almost equal to that when the high-intensity lights are used 1-3.141.

In the ideal situation, the degree of polymerization of the composite should be the same throughout its depth, and the hardness ratio should be equal to 1:1 or very close to it<sup>1-4)</sup>. That is, if polymerization was effective (i. e., maximum cure of the specimen was achieved) for the depth concerned, the ideal ratio should be 1:1, as the hardness of the bottom surface should be similar to that of the top surface<sup>1,2)</sup>.

As light passes through the bulk of the composite, the light intensity is greatly reduced due to light scattering, thus decreasing the effectiveness of polymerization<sup>1-4,15)</sup>. This scattering of light accounts for the differences in hardness between the top and bottom surfaces of the composites evaluated when specimens were 2 mm deep<sup>1,2,4)</sup>. Following the previous research for the light curing composites, thickness of composites cured at one time should not be greater than 2 mm to provide uniform and maximum polymerization despite manufacturers' claims<sup>2-4)</sup>.

It has been suggested that the top-to-bottom hardness gradient should not exceed 10 - 20% (ie, hardness ratio should be greater than 0.8) for adequately polymerized photo-activated resin composite<sup>1-5,8,16)</sup>. Depth at which a 20% reduction had taken place in maximum hardness was considered as a realistic depth of cure<sup>2,3,17)</sup>. At depths greater than 2 mm, poor polymerization of compos-

ite resulted, for polymerization was very susceptible to changes in light intensity and exposure duration<sup>1-3,8,13)</sup>.

Based on a hardness ratio of 0.8 as a guideline of adequate polymerization of bottom surface, Luxacore self was not affected by the thickness. In Luxacore dual, polymerization was effective in D2, D4 and DI6 specimens but the DI8 group showed just lower than the 0.8 ratio. The results of DB8 were unexpected because the hardness of bottom surface was lower than that of DS group. It could be explained that the initial low intensity light curing accelerated change of the dual cure composite matrix from the gel to postgel phase, thus the free movement of the radical was inhibited [18].

In clinical situation, it is very common to meet the cavity deeper than 4 mm. Following the result of the 6 mm groups, incremental filling group showed much higher hardness ratio than bulk filling group. Even in 8 mm depth, if incremental technique is applied, the bottom of the core can be polymerized close to the ratio 0.8. Within the limitation of this experiment, incremental filling is better than bulk filling in case of over 4 mm depth, and bulk filling should be avoided.

When comparing the Luxacore self and dual, the hardness of Luxacore dual-cured composite was greater than that of Luxacore self-cured type. Even though the hardness did not indicate all mechanical properties of the composite, if the both system used the same matrix and filler, light cure groups might have higher physical properties than self cure groups.

## V. CONCLUSIONS

In this study, we investigated the influence of thickness on the degree of cure of self- and dualcured composite core materials when light and self activated.

In self-cure mode, polymerization is not affected by the thickness both in the Luxacore Self and Dual. In light cure mode, however, when the thickness is over 4 mm, incremental filling is recommended to obtain adequate polymerization of the bottom surface.

## REFERENCES

- Soh MS, Yap AUJ & Siow KS. Effectiveness of composite cure associated with different curing modes of LED lights. Oper Dent 28:371-377, 2003.
- 2. Yap AUJ. Effectiveness of polymerization in composite restoratives claiming bulk placement: impact of cavity depth and exposure time. *Oper Dent* 25:113-120, 2000.
- 3. Soh MS, Yap AUJ & Siow KS. The Effectiveness of cure of LED and halogen curing lights at varying cavity depths. *Oper Dent* 28:707-715, 2003.
- Bala O, Uctasli MB & Tuz MA. Barcoll hardness of different resin-based composites cured by halogen or light emitting diode (LED). Oper Dent 30:69-74, 2005.
- Pilo R & Cardash HS. Post-irradiation polymerization of different anterior and posterior visible light-activated resin composites. *Dent Mater* 8:299-304, 1992.
- Sharp LJ, Yin R, Kang WH & Suh BI. Comparison of curing of resin cements. J Dent Res Abst. # 1847, 2005.
- Asmussen E. Restorative resins: hardness and strength vs quantity of remaining double bonds. Scand J Dent Res 90:484-489, 1982.
- 8. Laiza T Poskus, Elinane Placido & Paulo E Capel Cardoso. Influence of placement techniques on vickers and knoop hardness of class I composite resin restorations. *Dent Mater* 20:726-732, 2004.
- 9. Jandt KD, Mills RW, Blackwell GB & Ashworth SH.

- Depth of cure and compressive strength of dental composites cured with blue light emitting diodes (LEDs). *Dent Mater* 16:41-47, 2000.
- Dewald JP & Ferracane JL. A comparison of four modes of evaluating depth of cure of light-activated composites. J Dent Res 66:727-730, 1987.
- Bayne SC, Heymann HO & Swift EJ Jr. Update on dental composite restorations. J Am Dent Assoc 125: 687-701, 1994.
- 12. Roulet JF. Benefits and disadvantages of tooth-colored alternatives to amalgam. *J Dent* 25:459-473, 1997.
- 13. Rueggeberg FA, Caughman WF & Curtis JW Jr. Effect of light intensity and exposure duration on cure of resin composite. *Oper Dent* 19:26-32, 1994.
- 14. Rueggeberg FA & Jordan DM. Effect of light-tip distance on polymerization of resin composite. Int J Prosthodont 6:364-370, 1993.
- 15. Ruyter IE & ôysaed H. Conversion in different depths of ultraviolet and visible light activated composite materials. *Acta Odontol Scand* 40:179-192, 1982.
- Yearn JA. Factors affecting cure of visible light activated composites. Int Dent J 35:218-225, 1985.
- 17. Watts DC, Amer O & Combe EC. Characteristics of visible light-activated composite systems. Br Dent J 156:209-215, 1984.
- 18. Lovell LG, Newman SM & Bowman CN. The effects of light intensity, temperature, and comonomer composition on the polymerization behavior of dimethacrylate dental resins. J Dent Res 78:1469-1476, 1999.

### 국문초록

# 코어용 레진의 두께가 중합에 미치는 영향

권병철¹·박정원²\*
¹경북대학교 치과대학 치의학과 보존학교실
²연세대학교 치과대학 치의학과 보존학교실

본 연구는 코어용 이중 중합 레진의 중합도에 미치는 두께의 영향과 빛이 감소된 깊은 와동에서 자가 중합에 의한 영향을 조사하고자 하였다. Luxacore Dual과 Luxacore Self (DMG Inc, Hamburg, Germany) 두 종류의 코어용 레진 수복재를 지름 10 ㎜, 두께가 2, 4, 6, 8 ㎜ 의 Teflon mold에 주입하고 자가중합 시키거나 혹은 500 빼/㎝의 광도로 제조자의 지시에 따라 중합 후 37℃ 증류수에 24시간동안 저장하였다. 각 시편의 윗면과 아랫면에서 Knoop's hardness를 측정하였다. 결과는 ANOVA로 통계 분석하였고 Tukey's test로 사후 검정하였다.

Luxacore Self와 Luxacore Dual을 자가중합 시킨 군의 중합도는 두께에 따른 영향을 받지 않았다. Luxacore dual을 광중합한 경우 중합은 2 mm, 4 mm 와 6 (적층충전) m 군에서는 밑면의 효과적인 중합이 일어났으나 8 (적층충전) <math>m 군, 6, 8 (단일충전) m 군은 밑면에서 불완전한 중합을 보였다 (p ( 0.05)). 따라서 이 실험 결과에 의하면 4 mm를 초과하는 경우 단일충전보다 적층충전이 더 좋은 것으로 나타났다.

주요어: 이중중합 레진코어, 미세경도, 중합