

Comparison of shaping ability between various hybrid instrumentation methods with ProTaper

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ABSTRACT

The purpose of this study was to compare and evaluate the shaping abilities of various hybrid instrumentation method using constant tapered file systems with ProTaper® S1 and the difference between experts and inexperienced clinicians in use of NiTi file.

Three hybrid methods used in this study were composed of ProTaper® S1 and K-Flexofile® (group S), ProTaper® S1 and HeroShaper® (group H), and ProTaper® S1 and ProFile® (group P), respectively. The ProTaper®-alone method (group C) was introduced as a control group.

After canal preparation, the lapse of time was recorded. The images of pre- and post-operative canal were scanned and superimposed. Amounts of instrumented canal widths and centering ratio were measured at apical 1, 2 and 3 mm levels and statistical analysis was performed.

In this study, both of the group C and S took more time to prepare canals than other groups. Inexperienced operators required more time for the entire preparation with the groups C and H than the experienced ($p < 0.05$). And the centering ratio of group P were preferable to ProTaper®-alone method or the hybrid technique using stainless steel files. As such, within experienced operators, group H also showed better results in addition to the group P.

Under these condition, the hybrid methods of each the ProFile® system and HeroShaper® with ProTaper® are recommendable comparative to ProTaper®-alone method. According to the results, the hybrid instrumentation method is a more appropriate method of canal preparation than single file system for narrow or curved canals. (J Kor Acad Cons Dent 31(1):11-19, 2006)

Key words: Hybrid method, Inexperienced, Experienced, ProTaper, ProFile, HeroShaper

- Received 2005.8.23., revised 2005.10.11., accepted 2005.10.27. -

I. Introduction

Root canal instruments manufactured from nickel titanium (NiTi) alloy have been developed in an attempt to overcome the limitations imposed by stainless steel alloys¹⁾. NiTi instruments have two to three times higher elastic flexibility and a superior resistance to torsional fracture, compared with similar sized conventional stainless steel

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※ This work was supported by Pusan National University Research Grant, 2004.

instruments¹⁻⁵).

A number of NiTi rotary systems have been introduced in the market. Most of these systems are typical files generally with a constant tapered shaft design, while they have their own rake angles and radial lands⁶⁻¹⁰. On the other hand, the recently developed ProTaper system (Dentsply Maillefer, Ballaigues, Switzerland) is unique among these NiTi rotary instruments in that it has a progressively changing tapered shaft design^{9,10}. And the feature of cross-section of ProTaper - convex triangular - is claimed to reduce the contact area between the file and dentin and to make excellent cutting efficiency¹⁰. However, the great taper of ProTaper finishing files (F1, F2 and F3) makes a thicker and stiffer instrument especially at the apical portion, when compared to other files with the same apical size. This may attribute not only to the decreased operation time but also to the increased total canal width and deviation value⁹⁻¹¹. Several studies showed that ProTaper system produced more aberrations, deformation and straightening of the canal¹²⁻¹⁴. And then, some researchers suggested that a Ni-Ti file of less taper or U-file design -e.g. ProFile (Dentsply Maillefer, Ballaigues, Switzerland)- should be better for refining of the apical portion of small curved canals because of its greater elasticity¹⁵⁻¹⁷.

Judging from these various views, the complex design of ProTaper system capacitates efficient shaping of the coronal aspects of the canal and the relocation of canal orifices, resulting in a straight-line access^{10,15,16}. Therefore, the ProTaper with other file systems can be used in combination to emphasize the advantages of each system. This hybrid concept is to combine instruments of different file systems and use different instrumentation techniques suitable for individual clinical situations, thus the clinicians can achieve the best biomechanical cleaning and shaping results more easily and simply^{16,17}.

The purposes of this study are to compare and evaluate the shaping abilities of various hybrid instrumentation methods, using constant tapered file systems with ProTaper S1, and to compare

the differences between experts and inexperienced clinicians in use of NiTi instruments.

II. Materials and Methods

Twenty dentists were divided into two groups depending on the experience in using NiTi file systems - the first group (N) has no practical experience with NiTi file systems but prepared root canal with manual stainless steel files for more than 5 years. The second operator group (E) was composed of endodontists of over 5 years and has experience with rotary NiTi files over 2 years.

The each groups of operators prepared 80 simulated curved root canals in resin blocks (Endo Training Bloc; Dentsply Maillefer, Ballaigues, Switzerland). And each operator of the groups prepared two simulated root canals with four instrumentation methods respectively. The instrumentation methods are as following.

Method C: Control group - ProTaper system (S1, S2, F1 and F2).

Method S: ProTaper S1 and K-Flexofile (Dentsply Maillefer, Ballaigues, Switzerland) apically.

Method H: ProTaper S1 and HeroShaper (Micro-mega, Besancon, France) apically.

Method P: ProTaper S1 and ProFile apically.

1. Simulated root canals

The simulated root canal blocks used in this study had the working length of approximately 16 mm and about 40° curvature angle. Aqueous methylene blue dye was injected into the canal to enhance the contrast of the pre-instrumentation image. These resin blocks were scanned in a reproducible position with a scanner (Scanjet C8510A, Hewlett-Packard, California, USA), and then the data were stored in a personal computer.

2. Instrumentation

All of the rotary NiTi files used in this study were operated by an electric motor (Tecnika, ATR, Pistola, Italy) set at 300 r.p.m. and torque

Table 1. The instrumentation procedures

Method C	Hybrid methods [S], [H], [P]
	Patency check with #10 K-file followed by #15 K-file
	S1 to flare coronal until the depth of #15 K-file
	Working length measuring
	S1 to working length
S2 to working length	{#20 K-file},{HeroShaper .04/20},{ProFile .04/20}
F1 to working length	to working length
F2 to working length	{#25 K-file},{HeroShaper .04/25},{ProFile .04/25}
	to working length
	Apical gauging with #25 K-file

of 30 (Tecnika motor setting value) in a 16 : 1 reduction handpiece. The stainless steel K-Flexofile was operated by hand with balanced force technique. The instrumented sequence of each experimental group is summarized in Table 1.

During the procedures, canals were verified the patency with #10 K-file, then irrigated and lubricated with RC-prep (Stone Pharmaceuticals, Philadelphia, USA) repeatedly after instrumentation. All files used in this study were new.

3. Image taking

After the root canal preparation was completed, enlarged canals were filled with Vitapex (Neo Dental Chemical Products co., LTD, Tokyo, Japan). The resin blocks were scanned again in the reproducible position as previously described. The scanned images were assessed on a 15-inch TFT-LCD monitor (SyncMaster CX1565N, Samsung, Suwon, Korea) using Adobe Photoshop ver.7.0 (Adobe, San Jose, California, USA). The pre- and post-instrumented canal images were superimposed on one another and these superimposed images were inspected at a magnification of 141 times.

4. Evaluation

4-1. Aberration

Assessments were made according to the various types of canal aberrations such as apical zip, elbow and ledge.

4-2. Preparation time

Each operator recorded the time lapse of canal preparation including time for irrigation, changing instruments and recapitulation.

4-3. Assessment of canal preparation: Instrumented canal width and centering ratio

Measurements were made horizontally at three levels (1, 2 and 3 mm) from apical foramen (Figure 1). Instrumented canal widths were measured linearly from the pre-instrumented point to the post-instrumented wall inward and outward at each level. The amount of deviation was measured and centering ratio was calculated to evaluate the movement of root canal center after preparation^{18,19}. The ratio was computed using the following method: the absolute value of deviation divided by the whole width of the post-instrumented canal (Figure 2).

5. Statistical analysis

Statistical analysis of the collected data was performed with SPSS version 10.0 (SPSS Inc., Chicago, IL, USA). Statistical analysis of the four experimental groups was performed with ANOVA and Duncan's multiple range tests for post-hoc comparison. Independent t-test was done for comparative analysis between operators. Differences revealed in the data were designated as significant at $p < 0.05$.

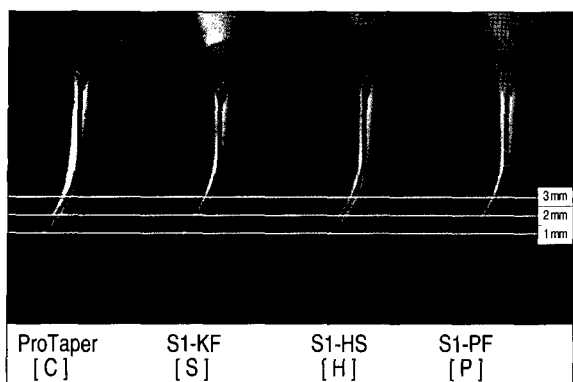


Figure 1. Representative superimposed images after instrumentation by method; the three horizontal lines mean the measured levels of 1 mm, 2 mm and 3 mm from apical end.

III. Results

1. Aberrations

The resin blocks instrumented with group S had more ledges than the other groups (Table 2). The experienced group made no aberrations with any methods.

2. Preparation time

The time needed for completion with each method is presented in Table 3. Both the group C and S took more time to prepare canals than the other groups irrespective of the experience of operators. The inexperienced operators required more time for the entire preparation with the group C and H methods than the experienced ($p < 0.05$).

3. Instrumented canal width and centering ratio

The instrumented canal widths after preparation were diminished in the order of groups C, S, H and P at all levels, regardless of operators ($p < 0.05$), except at 1 mm in the experienced where showed no significant differences between C and S groups and between S and H groups (Table 4).

The centering ratio is a measure of the ability of

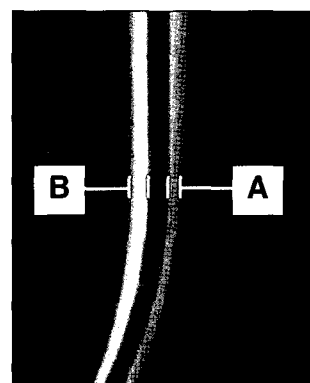


Figure 2. Instrumented canal width and deviation; Deviation: A-B.
A, outward instrumented width
B, inward instrumented width

Table 2. Incidence of canal aberrations by groups

Group	C		S		H		P	
	N	E	N	E	N	E	N	E
Ledge	0	0	7	0	1	0	0	0
Obstruction	1	0	1	0	0	0	0	0
Total	1	0	8	0	1	0	0	0

N: Inexperienced operators in Ni-Ti instrumentation
E: Experienced operators in Ni-Ti instrumentation

the instrument to stay centered in the canal^{18,19}. In inexperienced operators, at 1 and 2 mm, group P was distinctive from group H ($p < 0.05$). Group P had the smallest centering ratio of all the groups ($p < 0.05$). Group H had significantly larger centering ratios compared with group P ($p < 0.05$), and had no significant differences with group C ($p > 0.05$). Comparable with group C, however, group S had a better centering ability at 2 mm, but a larger ratio at 1 mm ($p < 0.05$) and no significant differences with group C.

Within the experienced operators, there were no significant differences between group P and group H except at 2 mm, and both groups had smaller centering ratios than group C ($p < 0.05$). Group S had no significant differences with group C at 1 mm levels and the largest ratio than the other hybrid methods (Figure 3 - 4 and Table 5).

Table 3. The lapse of time (seconds) per group (Mean ± SD)

Operator	Group C*	Group S	Group H*	Group P
Inexperienced	523 ± 154 ^{A†}	307 ± 93 ^{B†}	219 ± 53 ^{C†}	199 ± 71 ^{C†}
Experienced	269 ± 101 ^{A†}	240 ± 120 ^{A†}	166 ± 34 ^{B†}	164 ± 56 ^{B†}

* show a significant difference between operator groups (p < 0.05).

† Different superscripts indicate significant differences between the methods (p < 0.05).

Table 4. Instrumented canal width (µm) after root canal preparation (Mean ± SD)

Level	Operator	C	S	H	P
1 mm	N	489.5 ± 16 ^{D*}	396.0 ± 82 ^C	311.5 ± 91 ^B	185.5 ± 57 ^A
	E	485.5 ± 15 ^C	414.5 ± 15 ^{bc}	361.0 ± 22 ^b	254.5 ± 33 ^a
2 mm	N	416.0 ± 62 ^D	350.5 ± 10 ^C	274.0 ± 44 ^B	179.5 ± 52 ^A
	E	413.5 ± 53 ^d	331.5 ± 10 ^c	282.5 ± 39 ^b	224.0 ± 32 ^a
3 mm	N	413.0 ± 57 ^D	349.0 ± 12 ^C	272.0 ± 50 ^B	194.0 ± 47 ^A
	E	441.5 ± 53 ^d	345.5 ± 82 ^c	281.0 ± 32 ^b	234.5 ± 25 ^a

* Different superscripts indicate significant differences between the methods (p < 0.05).

N, Inexperienced operators in Ni-Ti instrumentation

E, Experienced operators in Ni-Ti instrumentation

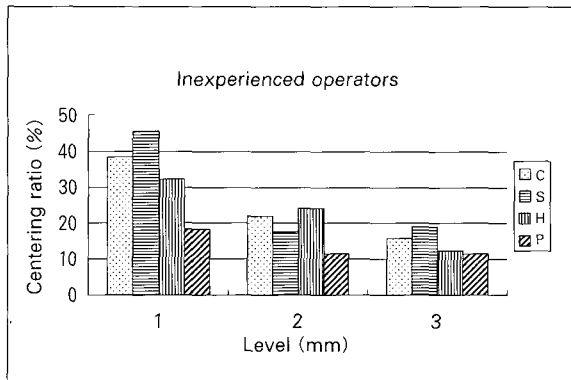


Figure 3. Mean differences of centering ratio between 4 methods in inexperienced operators.

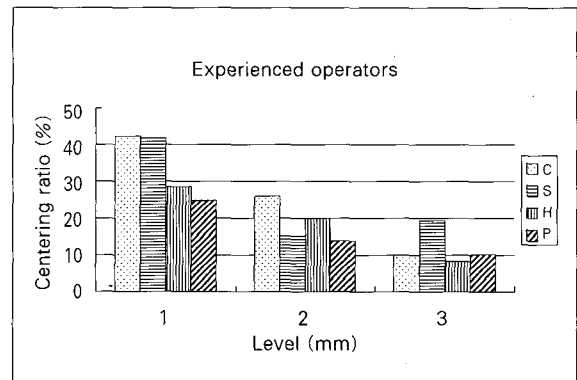


Figure 4. Mean differences of centering ratio between 4 methods in experienced operators.

Table 5. The significant differences between groups in centering ratio

Level	Operator	C	S	H	P
1 mm	N	BC*	C	B	A
	E	b	b	a	a
2 mm	N	B	AB	B	A
	E	c	ab	b	a
3 mm	N	No significant differences			
	E	a	b	a	a

* Different letters indicate significant differences between the methods (p < 0.05).

N, Inexperienced operators in Ni-Ti instrumentation

E, Experienced operators in Ni-Ti instrumentation

IV. Discussion

Clinically, it is true that there is no one perfect system of NiTi rotary instruments for all cases of root canal preparation. Each system has its own strong points and shortcomings, and particular rules for its operation. Likewise, ProTaper has many reports regarding its usefulness, especially in the initial phase of shaping (coronal and mid-root portion)^{10,15,16}. Despite its several merits, however, some studies showed that the ProTaper instruments produced more aberration, deformation and straightening of the canal especially at the apical portion, due to their thicker and stiffer finishing files (F1, F2 and F3)^{12,14}. Because of these concerns about procedural errors, some studies recommended that the use of passive or manual NiTi files should be better for the final phase of shaping of curved canals as a hybrid technique^{15,17}. It leads to the concept of hybrid instrumentation that can combine the best features of different systems for safe, quick, and predictable results¹⁶.

In this study, the hybrid instrumentation methods, combining ProTaper S1 and other instruments, were tested to compare the shaping ability. ProTaper S1 was used for the performance of body shaping and apical pre-enlargement, and the respective subsequent system of K-Flexofile, HeroShaper and ProFile was operated for the shaping and refining of the apical portion.

Conventional stainless steel files have higher deviations and more procedural errors than NiTi rotary files²⁻⁶. Up to now, however, stainless steel files are widely used and familiar with dentists using the traditional hand instrumentation techniques, and Szep *et al.*²⁰ reported that they produced a less occurrence in fracture of files than the NiTi collection. In this study, K-Flexofile was used as the representative of traditional stainless steel files, which is more flexible than the other stainless steel files. HeroShaper and ProFile are active and passive rotary NiTi instruments respectively and generally well acknowledged to the clinician.

One of the main problems inherent in the rotary preparation by clinicians is the risk of instrument fracture²¹. In this test, however, there was no fracture of instruments but the aberrations that might lead to fracture and hinder ideal canal preparation were distinctively noted in group S (ProTaper S1 and K-Flexofile) by inexperienced operator. Despite the notice, no statistical conclusions could be made by reason of the small number of occurrence.

In order to evaluate canal shaping ability, the time lapse for preparation, instrumented canal width, and centering ratio were measured and calculated^{18-22,23}.

Group C, as the control group, took more time and showed the largest cutting ability and higher apical deviation than other hybrid methods. It is consistent with some other studies in this points¹¹⁻¹⁴. Group S, compared with group C, took less instrumentation time in inexperienced operators and had no differences with experienced operators, in contrast to other reports¹²⁻¹⁴. It was probably that the operators without experience in rotary files had taken extreme care about active cutting tendency of ProTaper, to follow the recommendation from manufacturer. Another possibility is that they were already familiar to the traditional K-file. Group H and group P took less instrumentation time significantly than the other groups in both operators. Despite the research that the rake angle affects the shaping time²⁴, interestingly, group H did not have significant differences with group P. The result was interpreted that the time lapse was reduced significantly by the use of ProTaper S1 for pre-flaring of coronal two-thirds. Tip diameter of S1 corresponds to ISO size #17, and this made it easy to get not only coronal flaring but also apical pre-enlargement with the progressive greater taper.

Group S showed that the instrumented widths were smaller than group C at all measured levels. But, both of two groups showed poor centering ability than other two hybrid method. Especially, at 3 mm level, the group S had significantly larger width than other method in both operator groups. It was probable that the elasticity of K-file

became problematic as the F series of ProTaper, thereby group S showed some aberrations also, especially in the severely curved canal²⁻⁴⁾.

Group P showed the smallest instrumented width at all measured levels. Meanwhile, group P had the tendency of better centering ability than the other groups at all levels.

On the other hand, in group H, the canals were enlarged to larger width than group P, but were less than groups C and S. In addition, it was noticed that group H had similar centering ratios with group P at 3 mm in both operator groups. Particularly, at the 1 mm level (the terminal point of the curvature), group H had larger centering ratio than group P in inexperienced operators, but both groups yielded the similar centering with the experienced operators. The differences observed between groups P and H may be explained by the geometric design of ProFile and HeroShaper and by the difference in experiences of operators. With regards to the instrument design, Powell *et al.*²⁵⁾ has reported that the tip design of the instrument affects the shape of canals and the levels of deviation.

Canal shaping is disposed to transport the prepared canal away from the original axis. To prevent this problem, Griffiths *et al.*²⁶⁾ recommended that clinicians need to restrict the use of larger and stiffer instruments in the deeper portion of curved canal. In addition, various preparation techniques have been proposed to minimize this phenomenon. One of the effective methods is to pre-flare the coronal segment, and it is perhaps because of the fact that pre-flaring means that the file tip works on a minor contact surface^{16,19)}.

In present study, it was largely attributable to the use of ProTaper S1 that helped prepare a sufficiently wide and smooth-walled glide path in the coronal aspect of the curvature of the canal.

Among these hybrid methods, group P and group H showed good centering, less straightening, transportations and aberrations, in addition to the time-saving properties. These results generally corresponded with the distinguishing char-

acteristics of each file system^{6-15,27-30)}. Under this condition, hybrid methods showed better results than ProTaper-alone method, except for group S. Group S, when compared with group C, did not have any advantages in this study. Stainless steel files, however, may be preferable in smaller canals, because these instruments are able to negotiate constrictions and obstructions without bending⁵⁾. Therefore, clinicians have to make a choice over the instruments and methods suitable for each and individual case.

According to the present results, we can suggest the hybrid instrumentation is a more appropriate method in canal preparation than single file system especially for narrow or curved canals. Under the condition of this study the group P, pre-flaring with ProTaper S1 and apical enlargement with ProFile, can be recommended for overall efficiency. Group H, pre-flaring with ProTaper S1 and apical enlargement with HeroShaper, was preferred for experienced operators in addition to group P, as group H showed more cutting efficacy and centering ratios not significantly different from group P.

For use of this method in clinic, it is necessary to understand where in the canal each instrument performs its cutting action and apprehend when and how to use each instrument to its best ability.

V. Conclusion

According to the present results, we can suggest that hybrid instrumentation is more appropriate canal preparation method than single file systems for narrow or curved canals.

In this study, the centering ratio of group P was preferable to ProTaper-alone method or the hybrid method using stainless steel files. As such, within experienced operators, group H showed better results in addition to the group P. Under these conditions, hybrid methods of the ProFile and HeroShaper system with ProTaper are recommendable comparative to ProTaper-alone method.

References

1. Walia H, Brantley WA, Gerstein H. An initial investigation of the bending and torsional properties of Nitinol root canal files. *J Endod* 14(7):346-351, 1988.
2. Schafer E, Schulz-Bongert U, Tulus G. Comparison of hand stainless steel and nickel titanium rotary instrumentation: a clinical study. *J Endod* 30(6):432-435, 2004.
3. Chen JL, Messer HH. A comparison of stainless steel hand and rotary nickel-titanium instrumentation using a silicone impression technique. *Aust Dent J* 47(1):12-20, 2002.
4. Garip Y, Gunday M. The use of computed tomography when comparing nickel-titanium and stainless steel files during preparation of simulated curved canals. *Int Endod J* 34(6):452-457, 2001.
5. Glosson CR, Haller RH, Dove SB, Delrio CE. A comparison of root canal preparation using NiTi hand, NiTi engine driven and K-Flex endodontic instruments. *J Endod* 21:146-151, 1995.
6. Schafer E. Shaping ability of Hero 642 rotary nickel-titanium instruments and stainless steel hand K-Flexofiles in simulated curved root canals. *Oral Surg Oral Med Oral Pathol Oral Radiol Endod* 92(2):215-220, 2001.
7. Park H. A comparison of Greater Taper files, Profiles and stainless steel files to shape curved root canals. *Oral Surg Oral Med Oral Pathol Oral Radiol Endod* 91(6):715-718, 2001.
8. Ankrum MT, Hartwell GR, Truitt JE. K3 Endo, ProTaper, and ProFile systems: breakage and distortion in severely curved roots of molars. *J Endod* 30(4):234-237, 2004.
9. Bergmans L, Van Cleynenbreugel J, Beullens M, Wevers M, Van Meerbeek B, Lambrechts P. Progressive versus constant tapered shaft design using NiTi rotary instruments. *Int Endod J* 36(4):288-295, 2003.
10. Clauder T, Baumann MA. ProTaper NT system. *Dent Clin North Am* 48(1):87-111, 2004.
11. Peters OA, Peters CI, Barbakow F. ProTaper rotary root canal preparation: effects of canal anatomy on final shape analysed by micro CT. *Int Endod J* 36(1):86-92, 2003.
12. Calberson FL, Deroose CA, Hommez GM, De Moor RJ. Shaping ability of ProTaper nickel-titanium files in simulated resin root canals. *Int Endod J* 37(9):613-623, 2004.
13. Yun HH, Kim SK. A comparison of the shaping abilities of 4 nickel-titanium rotary instruments in simulated root canals. *Oral Surg Oral Med Oral Pathol Oral Radiol Endod* 95(2):228-233, 2003.
14. Schafer E, Vlassis M. Comparative investigation of two rotary nickel-titanium instruments: ProTaper versus RaCe. Part 1. Shaping ability in simulated curved canals. *Int Endod J* 37(4):229-238, 2004.
15. Berutti E, Chiandussi G, Gaviglio I, Ibba A. Comparative analysis of torsional and bending stresses in two mathematical models of nickel-titanium rotary instruments: ProTaper versus ProFile. *J Endod* 29(1):15-19, 2003.
16. Walsch H. The hybrid concept of nickel-titanium rotary instrumentation. *Dent Clin North Am* 48:183-202, 2004.
17. Park SH, Cho KM, Kim JW. The Efficiency of the Ni-Ti Rotary files in Curved Simulated Canals Shaped by Novice Operators. *J Kor Acad Cons Dent* 28(2):146-155, 2003.
18. Calhoun G, Montgomery S. The effects of four instrumentation techniques on root canal shape. *J Endod* 14(6):273-277, 1988.
19. Kosa DA, Marshall G, Baumgartner JC. An analysis of canal centering using mechanical instrumentation techniques. *J Endod* 25(6):441-445, 1999.
20. Szep S, Gerhardt T, Leitzbach C, Luder W, Heidemann D. Preparation of severely curved simulated root canals using engine-driven rotary and conventional hand instruments. *Clin Oral Investig* 5(1):17-25, 2001.
21. Peters OA. Current Challenges and Concepts in the Preparation of Root Canal Systems: A Review. *J Endod* 30(8):559-567, 2004.
22. Hata G, Uemura M, Kato AS, Imura N, Novo NF, Toda T. A comparison of shaping ability using ProFile, GT file, and Flex-R endodontic instruments in simulated canals. *J Endod* 28(4):316-321, 2002.
23. Kim HC, Park JK, Hur B. Relative efficacy of three Ni-Ti file systems used by undergraduates. *J Kor Acad Cons Dent* 30(1):38-48, 2005.
24. Park WK, Lee HJ, Hur B. Shaping ability of nickel-titanium rotary files. *J Kor Acad Cons Dent* 29(1):44-50, 2004.
25. Powell SE, Simon JHS, Maze B. A comparison of the effect of modified and nonmodified instrument tips on apical canal configuration. *J Endod* 12:293-300, 1986.
26. Griffiths IT, Bryant ST, Dummer PM. Canal shapes produced sequentially during instrumentation with Quantec LX rotary nickel-titanium instruments: a study in simulated canals. *Int Endod J* 33:346-354, 2000.
27. Iqbal MK, Firic S, Tulcan J, Karabucak B, Kim S. Comparison of apical transportation between ProFile and ProTaper NiTi rotary instruments. *Int Endod J* 37(6):359-364, 2004.
28. Garala M, Kuttler S, Hardigan P, Steiner-Carmi R, Dorn S. A Comparison of the minimum canal wall thickness remaining following preparation using two nickel-titanium rotary systems. *Int Endod J* 36:636-642, 2003.
29. Gonza lez-Rodr'guez MP, Ferrer-Luque CM. A comparison of Profile, Hero 642, and K3 instrumentation systems in teeth using digital imaging analysis. *Oral Surg Oral Med Oral Pathol Oral Radiol Endod* 97(1):112-115, 2004.
30. Thompson SA, Dummer PMH. Shaping ability of Hero642 rotary nickel-titanium instruments in simulated root canals: Part 1. *Int Endod J* 33:248-254, 2000.

국문초록

ProTaper를 사용한 다양한 hybrid instrumentation methods의 근관성형 효율 비교

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이 연구의 목적은 ProTaper® S1과 3가지 종류의 파일을 각각 같이 사용하는 혼합법의 근관성형 효율을 비교해 보는 것이다.

5년 이상의 임상경력을 가진 치과의사 20명이 Ni-Ti 파일 경험자군과 비경험자군으로 나뉘어, ProTaper®만을 사용한 C군과 ProTaper® S1과 함께 세 종류의 파일 시스템- ProFile® (P군), HeroShaper® (H군), K-Flexofile® (S군)-을 혼합 적용하여, 각각의 방법으로 레진 근관을 성형하였다. 성형 전후 이미지를 중첩 시켜 근관형태 이상을 조사하고, 근단공부터 1, 2, 3 mm 위치에서 근관 폭경의 변화량, 중심 변위율을 산출, 비교하여 다음의 결과를 얻었다.

C군과 S군 모두 다른 실험군에 비해 성형시간이 많이 소요되었다. 경험자군에 비해 비경험자군에서는 C군과 H군에서 더 많은 시간이 소요되었다. P군의 중심변위율은 ProTaper®만을 사용한 C군이나 SS 파일을 사용한 S군보다 양호하였다. 마찬가지로, 경험자군의 경우에는 P군에 추가하여 H군도 더 나은 결과를 보였다 ($p < 0.05$).

이 실험 조건하에, ProFile®과 HeroShaper®를 사용한 혼합법이 ProTaper®만을 사용한 성형방법보다 더욱 추천된다.

주요어: 혼합법, 비경험자, 경험자, ProTaper, ProFile, HeroShaper