A COMPARATIVE EVALUATION OF THE ESTIMATORS OF THE 2-PARAMETER GENERALIZED PARETO DISTRIBUTION

V. P. Singh¹, M. Ahmad¹ and M. M. Sherif²

¹ Department of Civil and Environmental Engineering, Louisiana State University, Baton Rouge, LA70803-6405, U. S. A

² Department of Civil Engineering, United Arab Emirates University, Al-Ain, UAE

Abstract: Parameters and quantiles of the 2-parameter generalized Pareto distribution were estimated using the methods of regular moments, modified moments, probability weighted moments, linear moments, maximum likelihood, and entropy for Monte Carlo-generated samples. The performance of these seven estimators was statistically compared, with the objective of identifying the most robust estimator. It was found that in general the methods of probability-weighted moments and L-moments performed better than the methods of maximum likelihood estimation, moments and entropy, especially for smaller values of the coefficient of variation and probability of exceedance.

Keywords: Computer simulation, entropy, L-moments, maximum likelihood estimation, probability-weighted moments, regular moments.

1. INTRODUCTION

The generalized Pareto distribution (GPD), first proposed by Pareto in 1897 for the shape parameter < 0, is known as the Pareto type II distribution as well as the Pearson type VI distribution. Since Pickands (1975) introduced the term generalized Pareto (GP) distribution, it has been applied to a number of areas, encompassing socio-economic processes, physical and biological phenomena (Saksena and Johnson, 1984), reliability analysis, and analyses of environmental extremes. Davison and Smith (1990) pointed out that the GP distribution might form

the basis of a broad modeling approach to high-level exceedances. DuMouchel (1983) applied it to estimate the tail thickness, whereas Davison (1984a, 1984b) modeled contamination due to long-range atmospheric transport of radionuclides. Ochoa et al. (1980) found the Pareto distributions to be more suitable for annual peak flow data than the exponential-tailed distributions which are common to hydrologic frequency analysis. Van Montfort and Witter (1985, 1986, 1991) applied the GP distribution to model the peaks over threshold (POT) streamflows and rainfall series, and Smith (1984, 1987) applied it to analyze flood frequencies.

Similarly, Joe (1987) employed it to estimate quantiles of the maximum of N observations. Wang (1991) applied it to develop a POT model for flood peaks with Poisson arrival time, whereas Rosbjerg, et al. (1992) compared the use of the 2-parameter GP and exponential distributions as distribution models for exceedances with the parent distribution being a generalized GP distribution. In an extreme value analysis of the flow of Burbage Brook, Barrett (1992) used the GP distribution to model the POT flood series with Poisson interarrival times. Davison and Smith (1990) presented a comprehensive analysis of the extremes of data by use of the GP distribution for modeling the sizes and occurrences of exceedances over high thresholds.

The cumulative distribution function (CDF) of the 2-parameter GPD (GPD2) of a random variable X can be expressed as

$$F(x) = 1 - (1 - a\frac{x}{b})^{\frac{1}{a}}, a \neq 0$$
 (1)

$$F(x) = 1 - \exp(-\frac{x}{b}), a = 0$$
 (2)

The probability density function (PDF) of the GPD2 can be written as

$$f(x) = \frac{1}{b}(1 - a\frac{x}{b})^{\frac{1}{a}-1}, a \neq 0$$
 (3)

$$f(x) = \frac{1}{b} \exp(-\frac{x}{b}), a = 0$$
 (4)

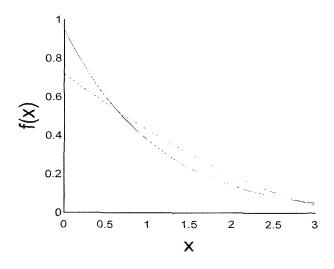
where a is the scale parameter with $-\infty < a < \infty$, b is the shape parameter with b > 0, and the range of x is $0 \le x \le \infty$ for $a \le 0$ and $0 \le x \le b/a$ for a > 0.

The 2-parameter GPD specializes into uni-

form, triangular, exponential and Pareto distributions as special cases. For a > 0, the distribution has a heavy Pareto-type upper tail. The case a = 0 is the exponential distribution. When a > 0 the distribution has an upper end point at b/a. For a = 1/2 and 1 the distribution is triangle and uniform respectively. The shapes of the GPD2 distribution for various values of a and b are illustrated in ures 1a-d.

Methods for estimating the GPD2 parameters, including the regular method of moments (RME), probability-weighted moments (PWM), and the method of maximum likelihood estimation (MLE), were reviewed by Hosking and Wallis (1987). Quandt (1966) used the method of moments (RME), whereas Baxter (1980), and Cook and Mumme (1981) used the method of maximum likelihood estimation (MLE). Van Montfort and Witter (1986) used MLE to fit the GP distribution to represent the Dutch POT rainfall series, and used an empirical correction formula to reduce bias of the scale and shape parameter estimates. Davison and Smith (1990) used MLE, PWM, a graphical method, and the least squares method to estimate the GP distribution parameters. Singh and Guo (1995 a, b, 1997) presented the entropy (ENT)-based parameter estimation method for 2-parameter, 2-parameter generalized Pareto and 3-parameter generalized Pareto distributions. Singh (1998) summarized entropy-based parameter estimation for the Pareto family. Moharram et al. (1993) compared MLE, RME, PWM and least squares method, using Monte Carlo simulation. They found the least squares method to be superior to other methods for shape parameter greater than zero and PWM for shape parameter less than zero.

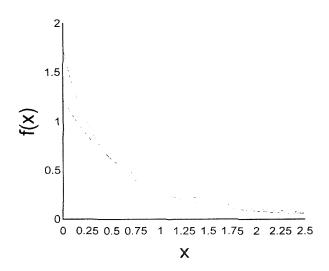
The maximum likelihood estimators exist in large samples provided that a < 1 and are as-



case 3 Figure 1a. Probability density function of the three parameter generalized Pareto distribution for population cases(1, 2 and 3).

case 2

case 1



case 5 case 4 case 6

Figure 1b. Probability density function of the three parameter generalized Pareto distribution for population cases(4, 5 and 6).

ymptotically normal and efficient if a < 1/2 (Smith, 1985). The variance of the distribution exists only for a > -1/2 and skewness for a > -1/3. The main conclusions reached by Hosking and Wallis (1987) were that MLE, although asymptotically the most efficient method, does not clearly display its efficiency even in samples as large as 500, that the method of moments is generally reliable except when a < -0.2 and that PWM estimation may be recommended if it seems likely that a < 0, particularly if it is important that the estimated extreme quantiles should have low bias or that the asymptotic theory should give a good approximation to the standard errors of the estimates.

Although, it would appear in the presence of the above cited literature and particularly in light of Hosking and Wallis (1987) that a new study on parameter and quantile estimation of the 2-parameter generalized Pareto (GPD2) distribution was not warranted. However, a closer scrutiny suggests otherwise. For a given sample data set, the ranges of the distribution parameters are not known in advance. Rather what is known is its mean, variance and skewness, and other moment properties. Therefore, It would be more logical to classify the best estimators in terms of these readily derivable data characteristics than to classify them in terms of a priori unknown parameters. While selecting the range of these characteristics (coefficient of variation in this case), all estimators should satisfy the familiar properties of consistency, asymptotic normality and efficiency. This approach was followed in this study. For theoretical and practical reasons, this study was restricted within the -1/2 < a < 1/2 range.

The objective of this paper is to statistically compare the performance of five estimators and variants of two of them, including the methods of regular moments, two modified moments, probability weighted moments, L-moments, maximum likelihood estimation and entropy, using Monte Carlo simulated data, and statistically evaluate the performance of these estimators. These methods were evaluated based on their relative performance in terms of robustness, variability and bias of large quantile estimates from varying sample sizes.

2. PARAMETER ESTIMATORS

2.1 Regular Moment Estimator (RME)

The moment estimation equations of GPD2 were derived by Hosking and Wallis (1987). Note that $E(1-a(x-c)/b)^r = 1/(1+ar)$ if 1+ra>0. The rth moment of X exists if a>-1/r. Provided that they exist, the moment estimators are

$$\bar{x} = \frac{b}{1+a} \tag{5}$$

$$S^2 = \frac{b}{(1+a)^2(1+2a)} \tag{6}$$

where \overline{x} and s^2 are the mean and variance, respectively. Equations (5) and (6) yield explicit relations for estimation of a and b as

$$a = \frac{1}{2}(\frac{\bar{x}^2}{s^2} - 1) \tag{7}$$

$$b = \frac{1}{2} \overline{x} (\frac{\overline{x}^2}{s^2} + 1) \tag{8}$$

2.2 Modified Moment Estimator (MME)

The regular moment estimator is valid only when a>-2. This somehow limits the practical application. Qaundt(1966) suggested two modified versions of the RME which involve restructuring equation (3) in terms some known property of the data. These two modified methods of moments are briefly outlined below.

2.2.1 Modified Moment Estimator (MME1)

In this modification, equation (4) is replaced by $E[F(x_l)] = F(x_l)$, which yields

$$1 - a \frac{x_1}{h} = \left(\frac{n}{n+1}\right)^a \tag{9}$$

By substituting the value of b from equation (5), one gets

$$\frac{x_1}{\bar{x}} = \frac{1+a}{a} \left[1 - \left(\frac{n}{n+1} \right)^n \right] \tag{10}$$

2.2.2 Modified Moment Estimator (MME2)

In this modification, equation (4) is replaced by $E[x_1] = x_1$. CDF of x_1 is given by

$$Fx_1(x) = 1 - [1 - F(x)]^n = 1 - \left[1 - a\frac{x}{b}\right]^{\frac{n}{a}}$$
 (11)

and its PDF is

$$f_{x_{1}}(x) = \frac{n}{b} \left(1 - a \frac{x}{b} \right)^{\frac{n}{a} - 1}$$
 (12)

Thus,

$$E(x_1) = x_1 = \frac{b}{n+a} \tag{13}$$

Eliminating b using equation (5), one gets

$$\frac{x_1}{\overline{x}} = \frac{1+a}{n+a} \tag{14}$$

2.3 Probability Weighted Moment Estimator

The probability-weighted moments (PWM) estimation equations of GPD2 were given by Hosking and Wallis (1987) as

$$a = \frac{W_0 - 4W1}{2W1 - W_0} \tag{15}$$

$$b = -\frac{2W_0W1}{2W1 - W_0} \tag{16}$$

where $W_r = M_{10r} = E\{x(F)[1-F(x)]^r\}$

2.4 Method of L-Moments (MLM)

The method of L-moments is a modification of the method of probability weighted moments developed by Greenwood et al (1979). Following Hosking and Wallis (1997) L-moments of GPG2 can be described as (a>-1):

$$\lambda_1 = W_0 \tag{17}$$

$$\lambda_2 = W_0 - 2W_1 \tag{18}$$

The shape parameter (a) and the scale parameter (b) can be defined as

$$a = \frac{\lambda_1}{\lambda_2} - 2 \tag{19}$$

$$b = (1+a)\lambda_1 \tag{20}$$

Substituting the values of the L-moments, one gets

$$a = \frac{W_0 - 4W_1}{2W_1 - W_0} \tag{21}$$

$$b = -\frac{2W_0W1}{2W1 - W_0} \tag{22}$$

Equations (21) and (22) are same as equations (15) and (16) of PWM.

2.5 Maximum Likelihood Estimator

The log-likelihood function for GPD2 given

by equation (3) can be written as

$$L = -n \ln b + (\frac{1}{a} - 1) \sum_{i=1}^{n} \ln \left(1 - a \frac{x_i}{b} \right)$$
 (23)

Differentiating the maximum likelihood function L with respect to a and b, two parameter equations are obtained for estimation as:

$$\sum_{i=1}^{N} \left[\frac{x_i/b}{1 - ax_i/b} \right] = \frac{n}{1 - a}$$
 (24)

$$\sum_{i=1}^{N} \left[\ln \left(1 - a \frac{x_i}{b} \right) \right] = -na$$
 (25)

Equations (24) and (25) are solved iteratively. To find the local maximum of log L, a numerical method is required. Due to the very sensitive nature of the log function of the Pareto distribution, the rate of failure given by equation (23) is quite high. As seen from the graphs in Figures 2-a and b and 3-a and b, the local maximum, even if it exists, is sometimes prone to be skipped over, i. E., the solution of equations (24) and (25) is not found. This perhaps was the problem encountered by Hosking and Wallis (1987) when the solution was not found in too many of their cases. In this study, a little laborious but more reliable approach involving two steps was used. First, a feasible range for a wide ranging set of parameters of a and b was marked. In the second stage, solution set was refined using the bisection method.

2.6 Entropy Estimator

The entropy estimation equations of GPD2 are given as

$$E\left[\ln\left(1-a\frac{x_i}{b}\right)\right] = -a \tag{26}$$

$$E\left[\frac{x_i/b}{1-ax_i/b}\right] = \frac{1}{1-a} \tag{27}$$

For a finite data set equations (26) and (27) are similar to equations (24) and (25) respectively.

3. EXPERIMENTAL DESIGN

3.1 Monte Carlo Simulations

The inverse of equation (1) is

$$x(F) = (\frac{b}{a})(1 - F^{a}), a \neq 0$$
(28)

and that of equation (2) is

$$x = -b\ln(1 - F), a = 0 (29)$$

where x (F) denotes the quantile of the cumulative probability P or 1 - F(x).

To assess the performance of the parameter estimation methods outlined above, Monte Carlo sampling experiments were conducted. Eight GPD2 population cases, listed in Table 1, were considered for eight values of the coefficient of variation (CV). These CV values are not exhaustive but do span the range normally encountered in hydrology and environmental and water resources. For each population case, 1000 random samples of size 10, 20, 50, 100, 200, and 500 were generated, and then parameters and quantiles were estimated.

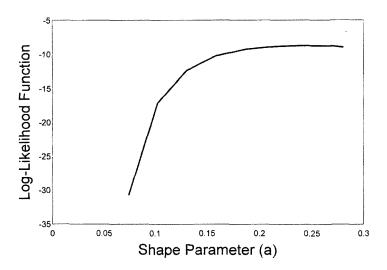


Figure 2a. Variation of log-likelihood function with parameter a: a > 0.

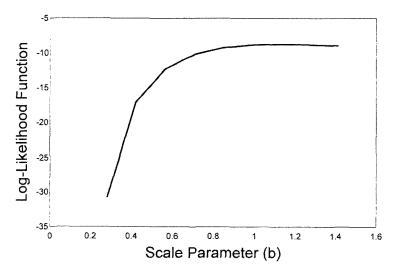


Figure 2b. Variation of log-likelihood function with parameter b: a > 0.

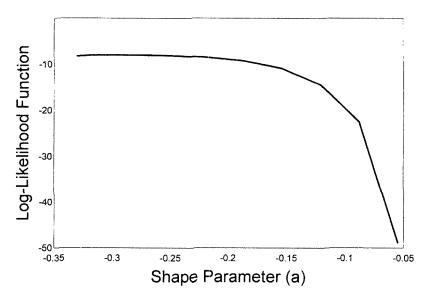


Figure 3a. Variation of log-likelihood function with parameter a: a < 0.

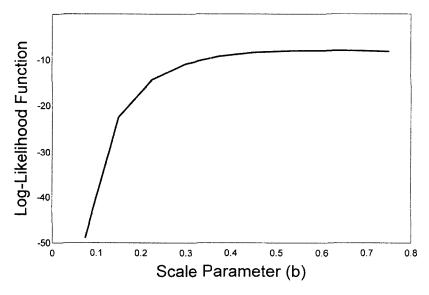


Figure 3b. Variation of log-likelihood function with parameter b: a < 0.

| GPD2 | | Parameter | | | |
|------------|------|-----------|-------|--|--|
| Pupulation | CV | a | b | | |
| case 1 | 0.75 | 0.389 | 1.389 | | |
| case 2 | 0.80 | 0.281 | 1.281 | | |
| case 3 | 0.90 | 0.117 | 1.117 | | |
| case 4 | 0.95 | 0.054 | 1.054 | | |
| case 5 | 1.25 | -0.180 | 0.820 | | |
| case 6 | 1.50 | -0.278 | 0.722 | | |
| case 7 | 2.00 | -0.375 | 0.625 | | |
| case 8 | 2.50 | -0.420 | 0.580 | | |

Table 1 GPD2 Population Cases Considered in Sampling Experiment(u=1)

3.2 Performance Indices

The performance of parameter estimators was evaluated by using the following performance indices:

Standardized bias,

$$BIAS = \frac{E(\hat{x}) - x}{r} \tag{30}$$

Standard Error,

$$SE = \frac{S(\bar{x})}{x} \tag{31}$$

Root Mean Square Error,

$$RMSE = \frac{E\left[\left(\hat{x} - x\right)^2\right]^{0.5}}{x}$$
 (32)

where $\hat{\mathbf{x}}$ is an estimate of x (parameter or quantile), E[X] denotes statistical expectation, and S(X) denotes standard deviation of the respective random variable. $E(\hat{x})$ and $S(\hat{x})$ were calculated as

$$E(\hat{x}) = \frac{1}{N} \sum_{i=1}^{N} \bar{x}_{i}$$
 (33)

$$S(\bar{x}) = \left\{ \frac{1}{N-1} \sum_{i=1}^{N} \left[\hat{x}_{1} - E(\hat{x}) \right]^{2} \right\}^{0.5}$$
 (34)

where the summations are over N estimates of x and N is the number of random samples used in estimation (N = 1000 here). The RMSE can also be expressed as

$$RMSE = \left[\frac{N-1}{N}SE + BIAS^2\right]^{0.5}$$
 (35)

These indices were used to measure the variability of parameter and quantile estimates for each simulation. Although they were used to determine the overall "best" parameter estimation method, our particular interest lies in the bias and variability of estimates of quantiles in the extreme tails of the distribution (P = 0.99, 0.999) when the estimates are based on small samples ($N \le 50$).

Due to the limited number of random number of samples used, the results are not expected to reproduce the true values of BIAS, SE and RMSE, but they do provide a means of comparing the performance of estimation methods used.

3.3 Robustness

The primary objective of this study is to identify a robust estimator for the GPD2. Kuczera (1982a, 1982b) defined a robust estimator as the one that is resistant and efficient over a wide range of population fluctuations. If an estimator performs steadily without undue deterioration in RMSE and BIAS, then it can be expected to perform better than other competing estimators under population conditions different from those on which conclusions were based. Two criteria for identifying a resistant estimator are mini-max and minimum average RMSE (Kuczera, 1982b). Based on the minimum criterion, the preferred estimator is the one whose maximum RMSE for all population cases is minimum. The minimum average criterion is to select the estimator whose RMSE average over the test cases is minimum.

4. RESULTS AND DISCUSSION

The performance of a parameter estimator depends on (1) sample size, N, (2) population coefficient of variance, CV, (3) distribution parameter, and (4) the probability of exceedance or the value of the variable exceeded, called quantile. The sample sizes included were 10, 20, 50, 100, 200, and 500; and the coefficients of variation (CV) for each sample size were 0.75, 0.8, 0.9, 0.95, 1.25, 1.5, 2.0, and 2.5. These CV values cover practically most variables of interest in hydrology and environmental and water resources. Most observed data record lengths are within the ranges of sample sizes considered. The probabilities of non-exceedance considered were 0.8, 0.9, 0.95, 0.99, and 0.999. The results of the GPD2 parameter estimation are summarized in Tables 2-5. It should be remarked that the results of the two modifications of the method of regular moments (RME) presented

earlier were inferior to those of RME, so for economy of space they were not included in the final comparison. Also, MLE and ENT produced identical results and were therefore clubbed together. Similarly, PWM and MLM were identical in their performance and clubbed together for purposes of comparison.

4.1 BIAS in Parameter Estimates

The results of parameter bias are summarized in Table 2. PWM and MLM performed in a superior manner for both parameters a and b for sample sizes and all values of CV. RME produced the highest bias in parameter a as well as for $CV \ge 0.95$, followed by MLE and ENT, regardless of the sample size, but the reverse was true for $CV \le 0.95$ and $N \ge 50$. As the sample size increased beyond 100, the bias in parameters a and b produced by RME, ENT and MLE was not greatly more than that of PWM and MLM if CV was less than 0.95. For CV ≥ 0.95 and N ≥ 200, MLE, ENT, MLM and PWM became comparable. Thus, in terms of bias, it can be concluded that PWM and MLM are the preferred method. For $N \ge 100$, any method would be acceptable for $CV \le 0.95$, but for CV \geq 2.0, the sample size would have to be larger than 500 for RME and greater than 200 for ENT and MLE.

4.2 RMSE in Parameter Estimates

The results of RMSE in parameters are summarized in Table 3. In general, the RSME of *a* method varied with the parameter to be estimated, the sample size and the coefficient of variation.

In terms of RMSE of parameter a, no method performed uniformly better. If $CV \le 0.95$ and $N \ge 20$, RME produced the least RMSE. As the value of CV increased, PWM and MLM per-

Table 2

| 733655 | 0700 |) ATT THE LOCAL TO THE LOCAL TH | | | | . Ch | - P | | (n) | |
|------------------------|------|--|--|--|--|--|--|--|--|--|
| SAMPLE ——— | SIZE | METHOD | | | as in | n Snar | e Para | ameter | (a) | |
| | | cv> | (.75) | (.80) | (. 90) | (.95) | (1.25) | (1.5) | (2.0) | (2.5) |
| 10 | | RME | .393 | .557 | 1.567 | 3.563 | 1.481 | 1.122 | .944 | .925 |
| | | PWM & MLM | .276 | .423 | 1.179 | 2.681 | 1.045 | .780 | .636 | .639 |
| | | MLE & ENT | .363 | .544 | 1.456 | 3.239 | 1.226 | .903 | .749 | .750 |
| 20 | | RME | .162 | .247 | .770 | 1.799 | .898 | .724 | .646 | .649 |
| | | PWM & MLM | .130 | .206 | .609 | 1.344 | .563 | .431 | .360 | .368 |
| | | MLE & ENT | .171 | .265 | .752 | 1.624 | .660 | .499 | .424 | .432 |
| 50 | | RME | .057 | .103 | .292 | .734 | .477 | .414 | .415 | .426 |
| 30 | | PWM & MLM | .048 | .095 | .234 | .551 | .248 | .186 | .171 | .170 |
| | | MLE & ENT | .063 | .122 | .289 | .666 | .291 | .215 | .201 | .199 |
| 100 | | RME | .030 | .042 | .151 | .370 | .282 | .282 | .303 | .322 |
| 100 | | PWM & MLM | .028 | .042 | .112 | .268 | .119 | .099 | .093 | .094 |
| | | MLE & ENT | .028 | .047 | .139 | .323 | .140 | .115 | .110 | .111 |
| | | MIE & ENI | .037 | .047 | .139 | .323 | .140 | .113 | .110 | .111 |
| 200 | | RME | .015 | .020 | .075 | .191 | .168 | .187 | .228 | .247 |
| | | PWM & MLM | .014 | .016 | .054 | .140 | .059 | .048 | .052 | .051 |
| | | MLE & ENT | .018 | .021 | .067 | .169 | .069 | .056 | .061 | .060 |
| 500 | | RME | .009 | .010 | .023 | .078 | .086 | .111 | .159 | .184 |
| | | PWM & MLM | .009 | .009 | .012 | .053 | .026 | .024 | .023 | .026 |
| | | MLE & ENT | .012 | .012 | .015 | .064 | .030 | .027 | .028 | .030 |
| | | | | , | | | 3 - D | + | /h.\ | |
| | | | | | Blas 1 | n Sca. | le Par | ameter | (b) | |
| 10 | | DMF | 142 | | | | | _ | | 553 |
| 10 | | RME | .142 | .145 | .174 | .191 | .285 | .366 | .485 | .553 |
| 10 | | PWM & MLM | .108 | .145 | .174 | .191 | .285 | .366 .213 | .485 | .286 |
| | | PWM & MLM MLE & ENT | .108 .142 | .145 .116 .149 | .174 .135 .166 | .191 .147 .177 | .285 .181 .212 | .366 .213 .247 | .485 .256 .301 | .286 .336 |
| 10 | | PWM & MLM MLE & ENT RME | .108 .142 | .145 .116 .149 | .174 .135 .166 | .191 .147 .177 | .285 .181 .212 | .366 .213 .247 | .485 .256 .301 | .286 .336 |
| | | PWM & MLM MLE & ENT RME PWM & MLM | .108 .142 .062 .054 | .145 .116 .149 .068 | .174 .135 .166 .090 | .191 .147 .177 .097 | .285 .181 .212 .179 .100 | .366 .213 .247 .240 | .485 .256 .301 .338 | .286 .336 .391 .148 |
| | | PWM & MLM MLE & ENT RME | .108 .142 | .145 .116 .149 | .174 .135 .166 | .191 .147 .177 | .285 .181 .212 | .366 .213 .247 | .485 .256 .301 | .286 .336 |
| | | PWM & MLM MLE & ENT RME PWM & MLM | .108 .142 .062 .054 | .145 .116 .149 .068 .060 .077 | .174 .135 .166 .090 | .191 .147 .177 .097 .074 .090 | .285 .181 .212 .179 .100 .117 | .366 .213 .247 .240 .113 .131 | .485 .256 .301 .338 .135 .159 | .286 .336 .391 .148 |
| 20 | | PWM & MLM MLE & ENT RME PWM & MLM MLE & ENT | .108 .142 .062 .054 | .145 .116 .149 .068 .060 | .174 .135 .166 .090 .073 | .191 .147 .177 .097 .074 .090 | .285 .181 .212 .179 .100 .117 | .366 .213 .247 .240 .113 .131 | .485 .256 .301 .338 .135 .159 | .286 .336 .391 .148 .174 .274 |
| 20 | | PWM & MLM MLE & ENT RME PWM & MLM MLE & ENT | .108 .142 .062 .054 .071 | .145 .116 .149 .068 .060 .077 | .174 .135 .166 .090 .073 .091 | .191 .147 .177 .097 .074 .090 | .285 .181 .212 .179 .100 .117 | .366 .213 .247 .240 .113 .131 | .485 .256 .301 .338 .135 .159 | .286 .336 .391 .148 .174 |
| 20 | | PWM & MLM MLE & ENT RME PWM & MLM MLE & ENT RME PWM & MLM | .108 .142 .062 .054 .071 | .145 .116 .149 .068 .060 .077 .029 .027 .035 | .174 .135 .166 .090 .073 .091 .034 .028 .034 | .191 .147 .177 .097 .074 .090 .040 .031 .037 | .285 .181 .212 .179 .100 .117 .094 .041 .049 | .366 .213 .247 .240 .113 .131 .145 .050 .058 | .485 .256 .301 .338 .135 .159 .218 .056 .066 | .286 .336 .391 .148 .174 .274 .065 .076 |
| 20 | | PWM & MLM MLE & ENT RME PWM & MLM MLE & ENT RME PWM & MLM MLE & ENT | .108 .142 .062 .054 .071 .021 .019 .025 | .145 .116 .149 .068 .060 .077 .029 .027 .035 | .174 .135 .166 .090 .073 .091 .034 .028 .034 | .191 .147 .177 .097 .074 .090 .040 .031 .037 | .285 .181 .212 .179 .100 .117 .094 .041 .049 | .366 .213 .247 .240 .113 .131 .145 .050 .058 | .485 .256 .301 .338 .135 .159 .218 .056 .066 | .286 .336 .391 .148 .174 .274 .065 .076 |
| 20 | | PWM & MLM MLE & ENT RME PWM & MLM MLE & ENT RME PWM & MLM MLE & ENT RME RME | .108 .142 .062 .054 .071 .021 .019 .025 | .145 .116 .149 .068 .060 .077 .029 .027 .035 | .174 .135 .166 .090 .073 .091 .034 .028 .034 | .191 .147 .177 .097 .074 .090 .040 .031 .037 | .285 .181 .212 .179 .100 .117 .094 .041 .049 | .366 .213 .247 .240 .113 .131 .145 .050 .058 | .485 .256 .301 .338 .135 .159 .218 .056 .066 | .286 .336 .391 .148 .174 .274 .065 .076 |
| 20 | | PWM & MLM MLE & ENT RME PWM & MLM MLE & ENT RME PWM & MLM MLE & ENT RME PWM & MLM RME & ENT | .108 .142 .062 .054 .071 .021 .019 .025 | .145 .116 .149 .068 .060 .077 .029 .027 .035 | .174 .135 .166 .090 .073 .091 .034 .028 .034 | .191 .147 .177 .097 .074 .090 .040 .031 .037 | .285 .181 .212 .179 .100 .117 .094 .041 .049 | .366 .213 .247 .240 .113 .131 .145 .050 .058 | .485 .256 .301 .338 .135 .159 .218 .056 .066 | .286 .336 .391 .148 .174 .274 .065 .076 |
| 20 50 100 | | PWM & MLM MLE & ENT RME PWM & MLM MLE & ENT RME PWM & MLM MLE & ENT RME PWM & MLM MLE & ENT | .108 .142 .062 .054 .071 .021 .019 .025 | .145 .116 .149 .068 .060 .077 .029 .027 .035 | .174 .135 .166 .090 .073 .091 .034 .028 .034 .018 | .191 .147 .177 .097 .074 .090 .040 .031 .037 | .285 .181 .212 .179 .100 .117 .094 .041 .049 | .366 .213 .247 .240 .113 .131 .145 .050 .058 .099 .026 .030 | .485 .256 .301 .338 .135 .159 .218 .056 .066 .168 .033 .039 | .286 .336 .391 .148 .174 .274 .065 .076 .213 .036 .042 |
| 20 50 100 | | PWM & MLM MLE & ENT RME PWM & MLM MLE & ENT | .108 .142 .062 .054 .071 .021 .019 .025 .011 .011 | .145 .116 .149 .068 .060 .077 .029 .027 .035 | .174 .135 .166 .090 .073 .091 .034 .028 .034 .018 .014 .017 | .191 .147 .177 .097 .074 .090 .040 .031 .037 .019 .014 | .285 .181 .212 .179 .100 .117 .094 .041 .049 .058 .021 .025 | .366 .213 .247 .240 .113 .131 .145 .050 .058 .099 .026 .030 | .485 .256 .301 .338 .135 .159 .218 .056 .066 .168 .033 .039 | .286 .336 .391 .148 .174 .274 .065 .076 .213 .036 .042 |
| 20 50 100 | | PWM & MLM MLE & ENT RME PWM & MLM MLE & ENT | .108 .142 .062 .054 .071 .021 .019 .025 .011 .014 | .145 .116 .149 .068 .060 .077 .029 .027 .035 .011 .010 .013 | .174 .135 .166 .090 .073 .091 .034 .028 .034 .018 .017 | .191 .147 .177 .097 .074 .090 .040 .031 .037 .019 .014 .017 | .285 .181 .212 .179 .100 .117 .094 .041 .049 .058 .021 .025 | .366 .213 .247 .240 .113 .131 .145 .050 .058 .099 .026 .030 | .485 .256 .301 .338 .135 .159 .218 .056 .066 .168 .033 .039 | .286 .336 .391 .148 .174 .065 .076 .213 .036 .042 .165 |
| 20 50 100 200 | | PWM & MLM MLE & ENT RME PWM & MLM MLE & ENT | .108 .142 .062 .054 .071 .021 .019 .025 .011 .014 .006 .008 | .145 .116 .149 .068 .060 .077 .029 .027 .035 .011 .010 .013 | .174 .135 .166 .090 .073 .091 .034 .028 .034 .018 .017 | .191 .147 .177 .097 .074 .090 .040 .031 .037 .019 .014 .017 | .285 .181 .212 .179 .100 .117 .094 .041 .049 .058 .021 .025 | .366 .213 .247 .240 .113 .131 .145 .050 .058 .099 .026 .030 | .485 .256 .301 .338 .135 .159 .218 .056 .066 .168 .033 .039 .126 .016 | .286 .336 .391 .148 .174 .274 .065 .076 .213 .036 .042 .165 .017 .020 |

Table 3

| SAMPLE SIZE | E METHOD | | I | RMSE i | n Shar | e Par | ameter | (a) | |
|-------------|-----------|-------|--------------|--------|--------|--------------|--------|-------|-------|
| | CV> | (.75) | (.80) | (.90) | "(.95) | (1.25) | (1.5) | (2.0) | (2.5) |
| 10 | RME | 1.481 | 1.812 | 4.131 | 8.393 | 2.462 | 1.676 | 1.253 | 1.182 |
| | PWM & MLM | 1.349 | 1.757 | 4.060 | 8.439 | 2.490 | 1.654 | 1.201 | 1.124 |
| | MLE & ENT | 1.589 | | | | | | 1.303 | |
| 20 | RME | .818 | 1.041 | 2.318 | 4.813 | 1.513 | 1.043 | .829 | .799 |
| | PWM & MLM | .878 | 1.153 | 2.614 | 5.422 | 1.632 | 1.067 | .793 | .739 |
| | MLE & ENT | 1.034 | 1.333 | 2.936 | 5.994 | 1.766 | 1.144 | .861 | .800 |
| 50 | RME | .467 | .580 | 1.272 | 2.738 | .900 | .638 | .537 | .518 |
| | PWM & MLM | .533 | .683 | 1.520 | 3.231 | .971 | .648 | .491 | .451 |
| | MLE & ENT | .627 | .790 | | | 1.051 | | .533 | .488 |
| 100 | RME | .319 | .395 | .868 | 1.861 | . 637 | .465 | .402 | .394 |
| | PWM & MLM | .370 | .474 | 1.058 | 2.233 | .672 | .450 | .357 | .324 |
| | MLE & ENT | .436 | .474 .548 | 1.189 | 2.468 | .672 .727 | .483 | .387 | .351 |
| 200 | RME | .220 | .275 | .597 | 1.288 | .468 | .349 | .311 | .307 |
| | PWM & MLM | .258 | .335 | .734 | 1.550 | .472 | | .262 | .240 |
| | MLE & ENT | .304 | .387 | .825 | 1.714 | .511 | .347 | .284 | .260 |
| 500 | RME | .138 | .172 | .370 | .808 | .323 | | .230 | .232 |
| | PWM & MLM | .163 | .211 | .458 | .975 | .295 | .206 | .174 | .163 |
| | MLE & ENT | .192 | .244 | .514 | 1.078 | .319 | .221 | .188 | .177 |
| | | | R | MSE in | Scal | e Para | meter | (b) | |
| 10 | RME | .617 | .594 | .612 | .594 | . 652 | .721 | .881 | 1.032 |
| | PWM & MLM | .564 | | .593 | .592 | .626 | .648 | .689 | .712 |
| | MLE & ENT | .664 | .659 | .666 | .654 | | . 695 | .747 | .772 |
| 20 | RME | .366 | .356 | .366 | .358 | .398 | | | .655 |
| | PWM & MLM | .373 | .372 | .388 | .380 | .397 | .409 | .424 | .438 |
| | MLE & ENT | .440 | .430 | .436 | .420 | .430 | .439 | .460 | .474 |
| 50 | RME | .212 | .208 | .205 | .208 | .232 | .271 | .335 | .409 |
| | PWM & MLM | .224 | .224 | .223 | .226 | .233 | .244 | .244 | .253 |
| | MLE & ENT | .264 | .259 | | .250 | | | .265 | .274 |
| 100 | RME | .146 | .143 | .143 | .144 | .161 | .184 | .244 | .292 |
| | PWM & MLM | .156 | .155 | .157 | .158 | .162 | .162 | .170 | .172 |
| | MLE & ENT | .184 | .179 | .176 | .175 | .175 | .174 | .185 | .187 |
| 200 | RME | .101 | .100 | .098 | .100 | .114 | .131 | | .215 |
| | PWM & MLM | | | .108 | | | .115 | | .122 |
| | MLE & ENT | .128 | .127 | .122 | .120 | .122 | .123 | .127 | .132 |
| 500 | RME | .064 | | .062 | .062 | .075 | .090 | | .154 |
| | PWM & MLM | .069 | .069 | .068 | .068 | .070 | .072 | | .077 |
| | MLE & ENT | .081 | .079 | .077 | .075 | .076 | .077 | .082 | .083 |

Table 4

Bias in quantiles

| | | | | PROBA | BILITY | OF NON | -EXCEED! | NCE = | .800 | |
|-----------------------------------|--|--|--|--|---|---|--|--|--|---|
| n | METHOD | CV> | (.75) | (.80) | (.90) | (.95) | (1.25) | (1.5) | (2.0) | (2.5) |
| 10 | RME | | 028 | 026 | 017 | 006 | .026 | .060 | .120 | .145 |
| | PWM & | MLM | 031 | 032 | 030 | 021 | 017 | 009 | .012 | .013 |
| | MLE & | | 217 | 193 | 190 | 168 | 099 | 065 | 005 | .051 |
| 20 | RME | | 013 | 010 | 004 | 001 | .027 | .050 | .099 | .116 |
| | PWM & | MLM | 016 | 015 | 012 | 010 | 006 | 007 | .001 | 003 |
| | MLE & | | 116 | 113 | 099 | 094 | 093 | 065 | 038 | .022 |
| 50 | RME | | 007 | 003 | 001 | .001 | .016 | .038 | .069 | .098 |
| | PWM & | MLM | 008 | 005 | 004 | 004 | 004 | 001 | 005 | 004 |
| | MLE & | | 046 | 036 | 043 | 042 | 039 | 052 | 028 | 022 |
| 100 | RME | | 003 | 003 | .000 | 001 | .012 | .027 | .061 | .081 |
| | PWM & | MLM | 004 | 004 | 002 | 003 | 001 | 001 | .000 | 002 |
| | MLE & | ENT | 020 | 023 | 024 | 022 | 027 | 026 | 032 | 017 |
| 200 | RME | | 001 | 002 | 001 | .001 | .006 | .018 | .045 | .065 |
| | PWM & | MLM | 001 | 003 | 002 | .000 | 002 | 002 | 002 | 004 |
| | MLE & | ENT | 011 | 012 | 011 | 011 | 014 | 018 | 019 | 013 |
| 500 | RME | | .000 | 001 | .001 | .000 | .004 | .012 | .034 | .051 |
| | PWM & | MLM | .000 | 001 | .000 | 001 | .000 | .000 | 001 | 002 |
| | MLE & | | 003 | 004 | 008 | 004 | 005 | 005 | 007 | 006 |
| | | | | | | | | | | |
| | | | | | | | -EXCEEDA | | . 900 | |
| n | METHOD | GA> | (.75) | (.80) | (.90) | (.95) | (1.25) | (1.5) | (2.0) | (2.5) |
| 10 | RME | | 044 | 050 | 054 | 048 | 046 | 031 | .004 | .014 |
| | PWM & | | 038 | 046 | 052 | 047 | 059 | 060 | 050 | 059 |
| | MLE & | ENT | .233 | .206 | .200 | .177 | .103 | .066 | .005 | 052 |
| 20 | RME | | 023 | 023 | 026 | 026 | 022 | 016 | .012 | .016 |
| | PWM & | | 021 | 023 | 026 | 025 | 031 | 038 | 037 | 048 |
| | MLE & | ENT | .125 | .121 | .104 | .098 | .097 | .067 | .039 | 023 |
| 50 | RME | | 010 | 010 | 010 | 011 | 013 | 002 | .010 | .027 |
| | PWM & | | 010 | 010 | 010 | 011 | 016 | 016 | 024 | 025 |
| 100 | MLE & | ENT | .049 | .039 | .045 | .044 | .041 | .053 | .028 | .023 |
| 100 | POPLE | | 005 | 005 | 005 | 006 | 005 | 001 | .016 | .025 |
| | DOM: C | | | | | | | | | |
| | PWM & | | 005 | 005 | 005 | 006 | 006 | 009 | 010 | 015 |
| 200 | MLE & | | .022 | .024 | .025 | .023 | .028 | .027 | .033 | .018 |
| 200 | MLE & RME | ENT | .022 002 | .024 003 | .025 003 | .023 002 | .028 | .027 001 | .033 | .018 .021 |
| 200 | MLE & RME PWM & | ENT MLM | .022 002 002 | .024 003 003 | .025 003 003 | .023 002 002 | .028 004 004 | .027 001 006 | .033 .011 008 | .018 .021 010 |
| | MLE & RME PWM & MLE & | ENT MLM | .022 002 002 .012 | .024 003 003 .013 | .025 003 003 .012 | .023 002 002 .012 | .028 004 004 .014 | .027 001 006 .018 | .033 .011 008 .019 | .018 .021 010 .014 |
| 200 500 | MLE & RME PWM & MLE & RME | ENT MLM ENT | .022 002 002 .012 001 | .024 003 003 .013 001 | .025 003 003 .012 .000 | .023 002 002 .012 001 | .028 004 004 .014 002 | .027 001 006 .018 | .033 .011 008 .019 | .018 .021 010 .014 .018 |
| | MLE & RME PWM & MLE & | MLM ENT MLM | .022 002 002 .012 | .024 003 003 .013 | .025 003 003 .012 | .023 002 002 .012 | .028 004 004 .014 | .027 001 006 .018 .000 002 | .033 .011 008 .019 .009 | .018 .021 010 .014 .018 |
| | MLE & RME PWM & MLE & RME PWM & | MLM ENT MLM | .022 002 002 .012 001 001 | .024 003 003 .013 001 002 | .025 003 003 .012 .000 .000 | .023 002 002 .012 001 001 | .028 004 004 .014 002 001 | .027 001 006 .018 .000 002 | .033 .011 008 .019 .009 004 | .018 .021 010 .014 .018 |
| 500 | MLE & RME PWM & MLE & RME PWM & MLE & MLE & MLE & MLE & | ENT MLM ENT MLM ENT | .022 002 002 .012 001 001 | .024 003 003 .013 001 002 .004 | .025 003 003 .012 .000 .000 | .023 002 002 .012 001 001 .005 | .028 004 004 .014 002 001 .005 | .027 001 006 .018 .000 002 .005 | .033 .011 008 .019 .009 004 .007 | .018 .021 010 .014 .018 005 |
| 500 n | MLE & RME PWM & MLE & RME PWM & MLE & | ENT MLM ENT MLM ENT | .022 002 002 .012 001 001 .003 | .024003003 .013001002 .004 PROBAN | .025 003 003 .012 .000 .000 .008 | .023 002 002 .012 001 001 .005 DF NON- (.95) | .028 004 004 .014 002 001 .005 | .027001006 .018 .000002 .005 | .033 .011 008 .019 .009 004 .007 | .018 .021 010 .014 .018 005 .006 |
| 500 | MLE & RME PWM & MLE & METHOD | ENT MLM ENT MLM ENT | .022 002 002 .012 001 001 .003 | .024 003 003 .013 001 002 .004 PROBAN (.80) | .025 003 003 .012 .000 .000 .008 | .023 002 002 012 001 005 DF NON- (.95) | .028 004 004 014 002 001 .005 -EXCREDA (1.25) | .027 001 006 .018 .000 002 .005 | .033 .011 008 .019 .009 004 .007 .950 (2.0) | .018 .021 010 .014 .018 005 .006 |
| 500 n | MLE & RME PWM & MLE & RME PWM & MLE & METHOD RME PWM & | ENT MLM ENT MLM ENT CV> | .022 002 002 .012 001 003 (.75) 046 029 | .024 003 003 .013 001 002 .004 PROBAN (.80) 059 044 | .025 003 003 .012 .000 .000 .008 SILITY (| .023 002 002 012 001 005 DF NON- (.95) 076 056 | .028 004 004 014 002 001 .005 -EXCREDA (1.25) 104 083 | .027001006 .018 .000002 .005 NCE = (1.5)107092 | .033 .011 008 .019 004 .007 .950 (2.0) 095 093 | .018 .021 010 .014 .018 005 .006 |
| n 10 | MLE & RME PWM & MLE & MLE & METHOD | ENT MLM ENT MLM ENT CV> | .022 002 002 .012 001 003 (.75) | .024 003 003 .013 001 002 .004 PROBAN (.80) 059 044 219 | .025 003 003 .012 .000 .000 .008 BILITY ((.90) 076 058 211 | .023 002 002 001 001 005 DF NON- (.95) 076 056 186 | .028 004 004 002 001 .005 -EXCREDA (1.25) 104 083 107 | .027001006 .018 .000002 .005 NCE = (1.5)107092068 | .033 .011 008 .019 .009 004 .007 .950 (2.0) 095 093 005 | .018 .021 010 .014 .018 005 .006 (2.5) 098 109 |
| 500 n | MLE & RME PWM & MLE & MLE & MLE & METHOD | ENT MLM ENT MLM ENT CV> | .022 002 002 .012 001 001 .003 (.75) 046 029 250 024 | .024003003 .013001002 .004 PROBAN (.80)059044219029 | .025 003 003 .012 .000 .008 3XLITY (.90) 076 058 211 040 | .023 002 002 .012 001 005 NON- (.95) 076 056 186 043 | .028 004 004 .014 002 001 .005 -EXCREDA (1.25) 104 083 107 064 | .027001006 .018 .000002 .005 NCE = (1.5)107092068074 | .033 .011 008 .019 .009 004 .007 .950 (2.0) 095 093 005 | .018 .021 010 .014 .018 005 .006 |
| n 10 | MLE & RME PWM & MLE & MLE & METHOD RME PWM & METHOD RME PWM & MLE & RME PWM & RME PW | ENT MLM ENT MLM ENT CV> MLM ENT MLM | .022 002 002 .012 001 003 (.75) 046 029 250 024 016 | .024003003 .013001002 .004 PROBAN (.80)059044219029021 | .025 003 003 .012 .000 .008 31LITY ((.90) 076 058 211 040 030 | .023 002 002 .012 001 005 DF NON- (.95) 076 056 186 043 031 | .028 004 004 .014 002 001 .005 -EXCREDA (1.25) 104 083 107 064 045 | .027001006 .018 .000002 .005 NCE = (1.5)107092068074058 | .033 .011 -008 .019 .009 004 .007 .950 (2.0) 095 093 005 066 063 | .018 .021 010 .014 .018 005 .006 (2.5) 098 109 .053 075 081 |
| 500 n 10 20 | MLE & RME PWM & MLE & MLE & MLE & MLE & RME PWM & MLE & RME PWM & MLE & RME PWM & MLE & ML | ENT MLM ENT MLM ENT CV> MLM ENT MLM | .022 002 002 .012 001 003 (.75) 046 029 250 024 016 134 | .024003003 .013001002 .004 PROBAN (.80)059044219029021129 | .025 003 003 .012 .000 .008 008 076 058 211 040 030 110 | .023 002 002 .012 001 005 DF NON- (.95) 076 056 186 043 043 031 103 | .028 004 004 .014 002 001 .005 -EXCREDA (1.25) 104 083 107 064 045 100 | .027001006 .018 .000002 .005 NCE = (1.5)107092068074058069 | .033 .011 -008 .019 .009 004 .007 .950 (2.0) 095 093 066 063 040 | .018 .021 010 .014 .018 005 .006 (2.5) 098 109 .053 075 081 |
| n 10 | MLE & RME PWM & MLE & MLE & MLE & MLE & RME PWM & MLE & RME PWM & RME RME RME RME RME RME RME RME RME | ENT MLM ENT MLM ENT CV> MLM ENT MLM ENT | .022 002 002 .012 001 003 (.75) 046 029 250 024 016 134 | .024003003 .013001002 .004 PROBAN (.80)059044219029021129013 | .025 003 003 .012 .000 .000 .008 BILITY ((.90) 076 058 211 040 030 110 016 | .023 002 002 .012 001 005 DF NON- (.95) 076 056 186 043 031 103 103 | .028 004 004 014 002 001 .005 -EXCREDA (1.25) 104 083 107 064 045 100 038 | .027001006 .018 .000002 .005 NCE = (1.5)107092068074058069040 | .033 .011 008 .019 .009 004 .007 .950 (2.0) 095 093 093 066 063 040 046 | .018 .021 010 .014 .018 005 .006 (2.5) 098 109 .053 075 081 |
| 500 n 10 20 | MLE & RME PWM & MLE & METHOD RME PWM & METHOD RME PWM & MLE & RME PWM & RM | ENT MLM ENT CV> MLM ENT MLM ENT MLM ENT MLM ENT | .022 002 002 .012 001 003 (.75) 046 029 250 024 016 134 011 007 | .024003003 .013001002 .004 PROBAN (.80)059044219029021129013010 | .025 003 003 .012 .000 .008 3XLITY (.90) 076 058 211 040 030 110 016 012 | .023 002 002 .012 001 005 NON- (.95) 076 056 186 043 031 103 019 014 | .028 004 004 .014 002 005 -EXCREDA (1.25) 104 083 107 064 045 100 038 023 | .027001006 .018 .000002 .005 NCE = (1.5)107092068074058069040025 | .033 .011 008 .019 .009 007 .950 (2.0) 095 093 066 063 040 046 037 | .018 .021 010 .014 .018 005 .006 (2.5) 098 109 .053 075 081 .023 |
| n 10 20 | MLE & RME PWM & MLE & METHOD RME PWM & MLE & RME PWM | ENT MLM ENT CV> MLM ENT MLM ENT MLM ENT MLM ENT | .022 002 002 .012 001 003 (.75) 046 029 250 024 016 134 011 | .024003003 .013001002 .004 PROBAN (.80)059044219029021129013010041 | .025 003 003 .012 .000 .000 .008 3ILITY (.90) 076 058 211 040 030 110 016 012 048 | .023 002 002 .012 001 005 DF NON- (.95) 076 056 186 043 031 019 014 014 | .028004004014002001 .005 -EXCREDA (1.25)104083107064045100038023042 | .027001006 .018 .000002 .005 NCE = (1.5)107092068074058069025055 | .033 .011 -008 .019 .009 004 .007 .950 (2.0) 095 093 005 066 063 040 046 037 029 | .018 .021 010 .014 .018 005 .006 (2.5) 098 109 .053 075 081 .023 041 023 |
| 500 n 10 20 | MLE & RME PWM & MLE & MLE & MLE & RME PWM & RME PWM & RME PWM & RME PWM & RME RME | ENT MLM ENT CV> MLM ENT MLM ENT MLM ENT | .022 002 002 .012 001 003 (.75) 046 029 250 024 016 134 011 005 053 006 | .024003003 .013001002 .004 PROBAN (.80)059044219029013010041007 | .025 003 000 .000 .000 .008 BILITY ((.90) 076 058 211 040 030 110 016 012 012 | .023 002 002 .012 001 005 DF NON- (.95) 076 056 186 043 031 019 014 014 | .028004004002001 .005 -EXCEEDA (1.25)104083107064045100038023042021 | .027001006 .018 .000002 .005 NCE = (1.5)107092068074058069040025055028 | .033 .011 -008 .019 .009 004 .007 .950 (2.0) 095 093 005 066 063 040 046 037 029 028 | .018 .021 -010 .014 .018 005 .006 (2.5) 098 109 .053 075 081 .023 040 |
| n 10 20 | MLE & RME PWM & MLE & MLE & MLE & MLE & RME PWM & MLE & RME PW | ENT MLM ENT CV> MLM ENT MLM ENT MLM ENT MLM ENT MLM ENT | .022 002 002 001 001 .003 (.75) 046 029 250 024 016 134 011 007 053 006 004 | .024003003 .013001002 .004 PROBAN (.80)059044219029021129013010041007005 | .025 003 003 .012 .000 .008 BILITY (.90) 076 058 211 040 030 110 016 012 048 012 | .023002002001001005 DF NON- (.95)076056186043031103014046011008 | .028004004002001 .005 -EXCREDA (1.25)104083107064045100038023042021010 | .027001006 .018 .000002 .005 NCE = (1.5)107092068074058069040025055 | .033 .011 008 .019 .009 007 .950 (2.0) 095 093 066 063 046 040 037 029 028 017 | .018 .021 010 .014 .018 005 .006 (2.5) 098 109 .053 075 081 023 041 023 |
| n 10 20 50 | MLE & RME PWM & MLE & METHOD RME PWM & MLE & RME PWM & RME PWM & RME & | ENT MLM ENT CV> MLM ENT MLM ENT MLM ENT MLM ENT MLM ENT | .022 002 002 .012 001 003 (.75) 046 029 024 016 134 016 134 016 134 016 134 007 053 004 | .024003003 .013001002 .004 PROBAN (.80)059044219029021129021129021129021129021129021129021029 | .025 003 003 .012 .000 .008 3XLITY (.90) 076 058 211 040 030 110 012 048 012 048 009 027 | .023 002 002 .012 001 005 NON- (.95) 076 056 043 031 043 031 019 014 046 011 046 011 008 024 | .028004004002001 .005 -EXCREDA (1.25)104083107064045100038023042021010029 | .027001006 .018 .000002 .005 NCE = (1.5)107092068074058069040025055028014027 | .033 .011 008 .019 .009 007 .950 (2.0) 095 093 066 063 040 046 037 029 028 028 | .018 .021 010 .014 .018 005 .006 (2.5) 098 109 .053 075 081 .023 041 023 024 024 |
| n 10 20 | MLE & RME PWM & MLE & METHOD RME PWM & MLE & RME PWM & RME & RME | ENT MLM ENT MLM ENT CV> MLM ENT MLM ENT MLM ENT MLM ENT | .022 002 002 .012 001 003 (.75) 046 029 250 024 016 134 011 007 053 006 004 | .024003003 .013001002 .004 PROBAN (.80)059044219021129013010041007005026004 | .025 003 003 .012 .000 .000 .008 3ILITY (.90) 076 058 211 040 030 110 016 012 048 009 006 | .023 002 002 .012 001 005 OF NON- (.95) 076 056 186 043 031 103 019 014 046 011 008 004 | .028004004014002001 .005 -EXCREDA (1.25)104083107064045100038023042021010029014 | .027001006 .018 .000002 .005 NCE = (1.5)107092069074058069025055028014027020 | .033 .011 -008 .019 .009 -004 .007 .950 (2.0) 095 093 005 066 063 040 046 037 029 028 017 023 | .018 .021 010 .014 .018 005 .006 (2.5) 098 109 .053 075 081 .023 041 023 029 024 |
| n 10 20 50 | MLE & RME PWM & & RME | ENT MLM ENT CV> MLM ENT MLM ENT MLM ENT MLM ENT MLM ENT MLM ENT | .022 002 002 .012 001 001 .003 (.75) 046 029 250 016 134 011 007 053 006 004 029 | .024003003 .013001002 .004 PROBAN (.80)059044219029021129013010041007005026004003 | .025003000 .000 .000 .008 SILITY ((.90)076058211040030110016012048009006027005 | .023002002001001005 DF NON- (.95)076056186043031103019014046011008024004003 | .028004004014002001 .005 -EXCREDA (1.25)104083107064045100038023021010029014006 | .027001006 .018 .000002 .005 NCE = (1.5)107092068074058069040025028014027008 | .033 .011 -008 .019 .009 004 .007 .950 (2.0) 095 093 005 066 063 040 046 037 029 028 017 | .018 .021 -010 .014 .018 005 .006 (2.5) 098 109 .053 075 081 .023 040 041 023 024 015 |
| n 10 20 50 100 200 | MLE & RME PWM & RME & RME & RME PWM & RME | ENT MLM ENT CV> MLM ENT MLM ENT MLM ENT MLM ENT MLM ENT MLM ENT | .022 002 002 .012 001 003 (.75) 046 029 250 024 016 134 011 007 053 004 023 004 023 001 001 | .024003003 .013001002 .004 PROBAN (.80)059044219029021129021129013010041007005026004003013 | .025 003 003 .012 .000 .000 .008 3ILITY (.90) 076 058 211 040 030 110 012 048 012 048 006 027 005 027 005 | .023002002001001005 DF NON- (.95)076056186043041046011014046011008024004003013 | .028004004002001 .005 -EXCREDA (1.25)104083107064045100038023042021010029014006015 | .027001006 .018 .000002 .005 NCE = (1.5)107092068074058058040025055028014027020008019 | .033 .011 008 .019 .009 004 .007 .950 (2.0) 095 093 066 063 040 040 046 037 029 028 028 023 023 | .018 .021 010 .014 .018 005 .006 (2.5) 098 109 .053 075 081 .023 041 023 024 018 029 018 029 |
| n 10 20 50 | MLE & RME PWM & RME RME PWM & RME & RME PWM & RME RME RME RME | ENT MLM ENT MLM ENT CV> MLM ENT MLM ENT MLM ENT MLM ENT MLM ENT | .022 002 002 001 001 .003 046 029 029 024 016 134 007 053 006 023 004 023 002 | .024003003 .013001002 .004 PROBAN (.80)059044219029021129021029031010041007005026004003013002 | .025003003 .012 .000 .008 SILITY (.90)076058211040030110012048009006027005004013001 | .023002002001001005 DF NON- (.95)076056186043031103019014046011008024003003013002 | .028004004002001 .005 -EXCREDA (1.25)104083107064045100038023042021010029014006015007 | .027001006 .018 .000002 .005 NCE = (1.5)1070920580740580690400250250200000019011 | .033 .011 008 .019 .009 007 .950 (2.0) 095 093 066 063 040 046 037 029 028 017 034 023 012 023 | .018 .021 010 .014 .018 005 .006 (2.5) 098 109 .053 075 081 .023 040 041 023 024 018 022 015 025 |
| n 10 20 50 100 200 | MLE & RME PWM & RME & RME & RME PWM & RME | ENT MLM ENT | .022 002 002 .012 001 003 (.75) 046 029 250 024 016 134 011 007 053 004 023 004 023 001 001 | .024003003 .013001002 .004 PROBAN (.80)059044219029021129021129013010041007005026004003013 | .025 003 003 .012 .000 .000 .008 3ILITY (.90) 076 058 211 040 030 110 012 048 012 048 006 027 005 027 005 | .023002002001001005 DF NON- (.95)076056186043041046011014046011008024004003013 | .028004004002001 .005 -EXCREDA (1.25)104083107064045100038023042021010029014006015 | .027001006 .018 .000002 .005 NCE = (1.5)107092068074058058040025055028014027020008019 | .033 .011 008 .019 .009 004 .007 .950 (2.0) 095 093 066 063 040 040 046 037 029 028 028 023 023 | .018 .021 010 .014 .018 005 .006 (2.5) 098 109 .053 075 081 .023 041 023 024 018 029 018 029 |

Table 4(Conted.)

| | | | | PROBAL | BILITY (| OF NON- | -EXCEEDA | NCE = | .990 | |
|------------------------------|---|--|---|--|--|---|---|--|--|--|
| n | METHOD | CV> | (.75) | (.80) | (.90) | (.95) | (1.25) | (1.5) | (2.0) | (2.5) |
| 10 | RME | | 019 | 047 | 090 | 104 | 201 | 242 | 277 | 303 |
| | PWM & | MLM | .033 | .008 | 016 | 024 | 077 | 102 | 124 | 158 |
| | MLE & | ENT | .268 | .234 | .223 | .195 | .111 | .071 | .006 | 054 |
| 20 | RME | | 009 | 021 | 051 | 063 | 137 | 184 | 218 | 252 |
| | PWM & | MLM | .020 | .010 | 008 | 013 | 038 | 062 | 079 | 111 |
| | MLE & | ENT | .143 | .137 | .116 | .109 | .104 | .071 | .041 | 024 |
| 50 | RME | | 004 | 012 | 021 | 027 | 085 | 115 | 162 | 180 |
| | PWM & | MLM | .008 | .000 | 003 | 005 | 021 | 023 | 044 | 051 |
| | MLE & | ENT | .057 | .044 | .050 | .049 | .044 | .057 | .030 | .024 |
| 100 | RME | | 003 | 005 | 012 | 015 | 051 | 085 | 122 | 146 |
| | PWM & | MLM | .003 | .002 | .000 | 003 | 007 | 014 | 019 | 029 |
| | MLE & | ENT | .025 | .028 | .028 | .025 | .030 | .028 | .035 | .018 |
| 200 | RME | | 001 | 003 | 007 | 007 | 032 | 059 | 098 | 119 |
| | PWM & | MLM | .002 | .001 | 001 | 001 | 004 | 006 | 012 | 017 |
| | MLE & | ENT | .013 | .014 | .013 | .013 | .015 | .020 | .020 | .014 |
| 500 | RME | | 001 | 002 | 001 | 004 | 016 | 036 | 072 | 091 |
| | PWM & | MLM | .000 | .000 | .002 | 001 | 002 | 003 | 006 | 008 |
| | MLE & | | .004 | .004 | .009 | .005 | .005 | .005 | .008 | .006 |
| | | | | | | | | | | |
| <u>-</u> | | | | PROBAL | BILITY (| OF NON- | -EXCEEDA | NCE = | . 999 | |
| - n | METHOD | CV> | (.75) | PROBAL (.80) | (.90) | OF NON- | | (1.5) | .999 | (2.5) |
| - n 10 | METHOD RME | CV> | (.75) .060 | | | | | | | (2.5) |
| | | | | (.80) | (.90) | (.95) | (1.25) | (1.5) | (2.0) | 502 |
| | RME | MLM | .060 | (.80) | (.90) 047 .180 235 | (.95) 082 .160 205 | (1.25) 277 .096 115 | (1.5) 367 .063 073 | (2.0) 454 .005 006 | 502 050 |
| | RME PWM & | MLM | .060 | (.80) .021 .182 | (.90) 047 .180 | (.95) 082 .160 | (1.25) 277 .096 | (1.5) 367 .063 | (2.0)454 .005006378 | 502 050 .055 |
| 10 | RME PWM & MLE & | MLM ENT | .060 .203 287 | (.80) .021 .182 249 | (.90) 047 .180 235 | (.95) 082 .160 205 | (1.25) 277 .096 115 | (1.5) 367 .063 073 | (2.0)454 .005006378 .037 | 502 050 .055 |
| 10 | RME PWM & MLE & RME | MLM ENT MLM | .060 .203 287 .037 | (.80) .021 .182 249 .021 | (.90) 047 .180 235 027 | (.95) 082 .160 205 049 | (1.25)277 .096115195 | (1.5)367 .063073291 | (2.0)454 .005006378 | 502 050 .055 431 |
| 10 | RME PWM & MLE & RME PWM & | MLM ENT MLM | .060 .203 287 .037 | .021 .182 249 .021 | (.90) 047 .180 235 027 | (.95) 082 .160 205 049 .089 | (1.25)277 .096115195 .090 | (1.5)367 .063073291 .063 | (2.0)454 .005006378 .037042296 | 502 056 .055 437 022 |
| 10 | RME PWM & MLE & RME PWM & MLE & | MLM ENT MLM ENT | .060 .203 287 .037 .108 | (.80) .021 .182 249 .021 .106 | (.90) 047 .180 235 027 .094 122 | (.95) 082 .160 205 049 .089 114 | (1.25)277 .096115195 .090108 | (1.5)367 .063073291 .063073 | (2.0)454 .005006378 .037042 | 502 056 .055 433 022 .024 |
| 10 | RME PWM & MLE & RME PWM & MLE & RME | MLM ENT MLM ENT | .060 .203 287 .037 .108 154 | (.80) .021 .182 249 .021 .106 146 .003 .034 | (.90)047 .180235027 .094122009 .041053 | (.95)082 .160205049 .089114019 .040051 | (1.25)277 .096115195 .090108125 .038045 | (1.5)367 .063073291 .063073195 .050058 | (2.0)454 .005006378 .037042296 .027030 | 502 050 .055 433 022 342 .022 |
| 10 | RME PWM & MLE & RME PWM & MLE & RME PWM & | MLM ENT MLM ENT | .060 .203 287 .037 .108 154 .015 | (.80) .021 .182 249 .021 .106 146 .003 .034 047 | (.90)047 .180235027 .094122009 .041053006 | (.95)082 .160205049 .089114019 .040051011 | (1.25)277 .096115195 .090108125 .038045075 | (1.5)367 .063073291 .063073195 .050 | (2.0)454 .005006378 .037042296 .027030236 | 502 050 .055 437 022 342 .022 |
| 10 20 50 | RME PWM & MLE & RME PWM & MLE & RME PWM & RME PWM & RME | MLM ENT MLM ENT MLM ENT | .060 .203 287 .037 .108 154 .015 .043 | (.80) .021 .182 249 .021 .106 146 .003 .034 | (.90)047 .180235027 .094122009 .041053 | (.95)082 .160205049 .089114019 .040051 | (1.25)277 .096115195 .090108125 .038045 | (1.5)367 .063073291 .063073195 .050058 | (2.0)454 .005006378 .037042296 .027030236 .032 | 502 056 437 022 342 .022 289 .017 |
| 10 20 50 | RME PWM & MLE & RME PWM & MLE & RME PWM & RME PWM & RME PWM & RME | MLM ENT MLM ENT MLM ENT | .060 .203 287 .037 .108 154 .015 .043 061 .007 .019 | (.80) .021 .182249 .021 .106146 .003 .034047 .004 .021029 | (.90)047 .180235027 .094122009 .041053006 .023030 | (.95)082 .160205049 .089114019 .040051011 .021026 | (1.25)277 .096115195 .090108125 .038045075 .026031 | (1.5)367 .063073291 .063073195 .050058148 .025029 | (2.0)454 .005006378 .037042296 .027030236 .032035 | 502 050 .055 43 022 .024 342 .022 289 .017 |
| 10 20 50 | RME PWM & MLE & RME PWM & MLE & RME PWM & RME PWM & RME PWM & RME | MLM ENT MLM ENT MLM ENT | .060 .203 287 .037 .108 154 .015 .043 061 .007 | (.80) .021 .182 249 .021 .106 146 .003 .034 047 | (.90)047 .180235027 .094122009 .041053006 .023 | (.95)082 .160205049 .089114019 .040051011 .021026005 | (1.25)277 .096115195 .090108125 .038045075 .026031047 | (1.5)367 .063073291 .063073195 .050058148 .025029104 | (2.0)454 .005006378 .037042296 .027030236 .032035194 | 502 050 .055 43 022 .024 342 .022 289 .017 |
| 10 20 50 | RME PWM & MLE & RME PWM & MLE & RME PWM & RME PWM & MLE & RME PWM & RME PWM & RME | MLM ENT MLM ENT MLM ENT MLM ENT | .060 .203 287 .037 .108 154 .015 .043 061 .007 .019 | (.80) .021 .182249 .021 .106146 .003 .034047 .004 .021029 | (.90)047 .180235027 .094122009 .041053006 .023030 | (.95)082 .160205049 .089114019 .040051011 .021026 | (1.25)277 .096115195 .090108125 .038045075 .026031 | (1.5)367 .063073291 .063073195 .050058148 .025029 | (2.0)454 .005006378 .037042296 .027030236 .032035194 .018 | 502 056 .055 43 022 342 .022 282 283 019 242 |
| 10 20 50 | RME PWM & MLE & RME PWM & RME RME RME RME | MLM ENT MLM ENT MLM ENT MLM ENT | .060 .203 287 .037 .108 154 .015 .043 061 .007 .019 027 | (.80) .021 .182249 .021 .106146 .003 .034047 .004 .021029 .002 .011015 | (.90)047 .180235027 .094122009 .041053006 .023030004 | (.95)082 .160205049 .089114019 .040051011026005 .011014 | (1.25)277 .096115195 .090108125 .038045075 .026031047 .013016 | (1.5)367 .063073291 .063073195 .050058148 .025029104 | (2.0)454 .005006378 .037042296 .027030236 .032035194 .018021 | 502 056 .055 43 022 342 .022 024 015 019 |
| 10 20 50 | RME PWM & RME PWM & RME PWM & RME PWM & MLE & RME PWM & RME RME PWM & RME PWM & RME PWM & RME RME PWM & RME | MLM ENT MLM ENT MLM ENT MLM ENT | .060 .203 287 .037 .108 154 .015 .043 061 .007 .019 027 | (.80) .021 .182249 .021 .106146 .003 .034047 .004 .021029 .002 | (.90)047 .180235027 .094122009 .041053006 .023030004 | (.95)082 .160205049 .089114019 .040051011021026005 | (1.25)277 .096115195 .090108125 .038045075 .026031047 .013 | (1.5)367 .063073291 .063073195 .050058148 .025029104 .017 | (2.0)454 .005006378 .037042296 .027030236 .032035194 .018 | 502 056 .055 43 022 342 .022 024 015 019 |
| 10 20 50 100 200 | RME PWM & RME PWM & RME PWM & RME PWM & MLE & RME PWM & RME RME | MLM ENT MLM ENT MLM ENT MLM ENT | .060 .203 -287 .037 .108 154 .015 .043 061 .007 .019 027 .004 | (.80) .021 .182249 .021 .106146 .003 .034047 .004 .021029 .002 .011015 | (.90)047 .180235027 .094122009 .041053006 .023030004 .011014 | (.95)082 .160205049 .089114019 .040051011026005 .011014 | (1.25)277 .096115195 .090108125 .038045075 .026031047 .013016 | (1.5)367 .063073291 .063073195 .050058148 .025029104 .017020 | (2.0)454 .005006378 .037042296 .027030236 .032035194 .018021 | |

Table 5

RMSE in quantiles

| | | | Pi | ROBABILIT | Y OF NO | N-EXCEEDA | NCE = | . 800 | |
|------------------------------|---|---|--|--|---|--|--|--|---|
| n | METHOD C | 7> (. | 75) (. | 80) (.9 | 0) (.95) | (1.25) | (1.5) | (2.0) | (2.5) |
| 10 | RME | | | 247 .2 | 85 .302 | .397 | .466 | .630 | .789 |
| | PWM & MI | | | 251 .2 | | | .401 | .452 | .474 |
| | MLE & El | | | 869 1.0 | | | 1.560 | 1.730 | 1.902 |
| 20 | RME | | | 180 .2 | | | .326 | .429 | .509 |
| 2.0 | PWM & MI | | | | | | | | |
| | | | | 181 .2 | | | .282 | .305 | .315 |
| | MLE & El | | | 580 .6 | | | 1.208 | 1.358 | 1.332 |
| 50 | RME | | | | 30 .137 | | .206 | .257 | .323 |
| | PWM & MI | м. | 106 . | 115 .1 | 31 .138 | .164 | .180 | .191 | .199 |
| | MLE & El | T. | 283 . | 315 .3 | 97 .438 | .653 | .828 | .917 | .999 |
| 100 | RME | | 074 . | 082 .0 | 93 .098 | .120 | .137 | .185 | .219 |
| | PWM & MI | | | 082 .0 | | | .125 | .136 | .138 |
| | MLE & EN | | | 219 .2 | | | .554 | | .724 |
| 200 | | | | | | | | .703 | |
| 200 | RME | | | 058 .0 | | | .096 | .127 | .152 |
| | PWM & MI | | | 058 .0 | | | .089 | .094 | .097 |
| | MLE & EN | T. | 130 . | 151 .1 | 91 .210 | .308 | .392 | .512 | .527 |
| 500 | RME | | 034 . | 036 .0 | 41 .043 | .053 | .060 | .078 | .098 |
| | PWM & MI | м. | 034 . | 037 .0 | 42 .043 | .053 | .056 | .060 | .062 |
| | MLE & EN | | | 095 .1 | | | .239 | .314 | .361 |
| | TIBE & EI | - | | 055 .1 | 19 .131 | 191 | ,239 | -214 | .361 |
| | | | PI | ROBABILIT | Y OF NON | -EXCEEDA | NCE = | . 900 | |
| n | METHOD CV | '> (. | 75) (. | 80) (.9 | 0) (.95) | (1.25) | (1.5) | (2.0) | (2.5) |
| 10 | RME | | | 232 .2 | | | .466 | .617 | .771 |
| | PWM & MI | | 213 . | 234 .2 | 77 .296 | .384 | .419 | .477 | .504 |
| | MLE & EN | T. | 888 . | 926 1.0 | 95 1.116 | 1.407 | 1.606 | 1.771 | 1.942 |
| 20 | RME | | | 165 .1 | | | .333 | .430 | .505 |
| | PWM & MI | | | 168 .1 | | .269 | .302 | .331 | |
| | MLE & EN | | | | | | | | .343 |
| | | | | 618 .7 | | 1.091 | 1.244 | 1.390 | 1.359 |
| 50 | RME | | | 102 .1 | | .177 | .215 | .264 | .325 |
| | PWM & MI | | 094 . | 104 .1: | 26 .134 | .174 | .195 | .213 | .224 |
| | MLE & EN | т. | 303 . | 335 .4 | 19 .460 | . 677 | .852 | .939 | 1.020 |
| 100 | RME | | | 072 .0 | | .126 | .146 | .191 | .220 |
| • • | PWM & MI | | | 074 .0 | | .124 | .138 | .155 | .158 |
| | MLE & EN | | | | | | | | |
| 200 | | | | 233 .2 | | .468 | .570 | .719 | .739 |
| 200 | RME | | | 051 .0 | | .089 | .103 | .132 | .152 |
| | PWM & MI | | | 052 .0 | | .088 | .099 | .110 | .114 |
| | MLE & EN | T. | 139 . | 161 .20 | .220 | .319 | .403 | .524 | .538 |
| 500 | RME | | 028 . | 032 .03 | .042 | .056 | .064 | .079 | .096 |
| | PWM & MI | | | 033 .03 | | .056 | .063 | .071 | .075 |
| | MLE & EN | | | | | | | | |
| | MLE & EN | | | 101 .12 | 25 .137 | .198 | .246 | .322 | .368 |
| | | | PR | OBABILIT | Y OF NON | -EXCEEDA | NCE = | . 950 | |
| | | | | | | | | | (2.5) |
| 'n | METHOD CV | > (. | 75) (.: | 80) (.90 | 0) (.95) | (1.25) | (1.5) | (2.0) | ,, |
| n 10 | RME | | 221 .: | 242 .29 | 91 .314 | (1.25) | .492 | .630 | .778 |
| | | | 221 .: | | 91 .314 | | | | |
| | RME | м .: | 221 .: 229 .: | 242 .29 | 91 .314 99 .324 | .424 | .492 | .630 .541 | .778 .578 |
| | RME PWM & ML | M .: | 221 .: 229 .: 952 .: | 242 .29 251 .29 986 1.15 | 91 .314 99 .324 55 1.172 | .424 .429 1.458 | .492 .475 1.654 | .630 .541 1.813 | .778 .578 1.982 |
| 10 | RME PWM & ML MLE & EN RME | M .: | 221 .: 229 .: 952 .: | 242 .29 251 .29 986 1.15 | 91 .314 99 .324 55 1.172 08 .224 | .424 .429 1.458 .304 | .492 .475 1.654 .362 | .630 .541 1.813 .453 | .778 .578 1.982 .523 |
| 10 | RME PWM & ML MLE & EN RME PWM & ML | M | 221 .: 229 .: 952 .: 150 .: | 242 .29 251 .29 986 1.15 172 .20 183 .21 | 91 .314 99 .324 55 1.172 08 .224 16 .233 | .424 .429 1.458 .304 .309 | .492 .475 1.654 .362 .352 | .630 .541 1.813 .453 .389 | .778 .578 1.982 .523 .403 |
| 10 20 | RME PWM & ML MLE & EN RME PWM & ML MLE & EN | M | 221 .: 229 .: 952 .: 150 .: 162 .: | 242 .29 251 .29 986 1.15 172 .20 183 .21 | 91 .314 99 .324 55 1.172 08 .224 16 .233 13 .785 | .424 .429 1.458 .304 .309 | .492 .475 1.654 .362 .352 | .630 .541 1.813 .453 .389 | .778 .578 1.982 .523 .403 |
| 10 | RME PWM & ML MLE & EN PWM & ML MLE & EN RME | M | 221 .: 229 .: 952 .: 150 .: 162 .: 599 .: | 242 .29 251 .29 986 1.15 172 .20 183 .23 558 .74 | 91 .314 99 .324 55 1.172 08 .224 16 .233 13 .785 32 .143 | .424 .429 1.458 .304 .309 1.130 | .492 .475 1.654 .362 .352 1.281 | .630 .541 1.813 .453 .389 1.423 | .778 .578 1.982 .523 .403 1.388 |
| 10 20 | RME PWM & ML MLE & EN RME PWM & ML MLE & EN | M | 221 229 952 150 162 599 | 242 .29 251 .29 986 1.15 172 .20 183 .21 | 91 .314 99 .324 55 1.172 08 .224 16 .233 13 .785 32 .143 | .424 .429 1.458 .304 .309 | .492 .475 1.654 .362 .352 1.281 .241 | .630 .541 1.813 .453 .389 1.423 .289 .259 | .778 .578 1.982 .523 .403 |
| 10 20 50 | RME PWM & ML MLE & EN PWM & ML MLE & EN RME | M | 221 229 952 150 162 599 | 242 .29 251 .29 986 1.15 172 .20 183 .23 558 .74 | 91 .314 99 .324 55 1.172 08 .224 16 .233 13 .785 32 .143 | .424 .429 1.458 .304 .309 1.130 | .492 .475 1.654 .362 .352 1.281 | .630 .541 1.813 .453 .389 1.423 | .778 .578 1.982 .523 .403 1.388 |
| 10 20 | RME PWM & ML MLE & EN PWM & ML MLE & EN RME PWM & ML | M | 221 229 952 150 162 599 094 103 325 | 242 .29 251 .29 986 1.15 172 .20 183 .23 558 .74 105 .13 | 91 .314 99 .324 55 1.172 08 .224 16 .233 13 .785 32 .143 10 .150 12 .484 | .424 .429 1.458 .304 .309 1.130 .200 .204 | .492 .475 1.654 .362 .352 1.281 .241 .233 .878 | .630 .541 1.813 .453 .389 1.423 .289 .259 | .778 .578 1.982 .523 .403 1.388 .346 .274 |
| 10 20 50 | RME PWM & ML MLE & EN RME PWM & ML MLE & EN RME PWM & ML MLE & EN RME RME RME | M | 221 229 952 150 162 1599 103 325 325 655 665 | 242 .29 251 .29 986 1.15 172 .20 183 .23 5558 .74 105 .13 114 .14 357 .44 | 91 .314 99 .324 65 1.172 08 .224 16 .233 13 .785 32 .143 10 .150 12 .484 92 .102 | .424 .429 1.458 .304 .309 1.130 .200 .204 .701 | .492 .475 1.654 .362 .352 1.281 .241 .233 .878 .168 | .630 .541 1.813 .453 .389 1.423 .289 .259 .961 .213 | .778 .578 1.982 .523 .403 1.388 .346 .274 1.041 |
| 10 20 50 | RME PWM & ML MLE & EN RME PWM & ML MLE & EN RME PWM & ML MLE & EN RME PWM & ML | M | 221 229 952 150 162 1599 103 103 103 103 105 . | 242 .29 251 .29 386 1.15 172 .20 183 .23 558 .74 105 .13 114 .14 357 .44 | 91 .314 99 .324 55 1.172 08 .224 66 .233 13 .785 82 .143 10 .150 12 .484 92 .102 | .424 .429 1.458 .304 .309 1.130 .200 .204 .701 .144 .147 | .492 .475 1.654 .362 .352 1.281 .241 .233 .878 .168 | .630 .541 1.813 .453 .389 1.423 .289 .259 .961 .213 .192 | .778 .578 1.982 .523 .403 1.388 .346 .274 1.041 .239 |
| 10 20 50 | RME PWM & ML MLE & EN PWM & ML MLE & EN RME PWM & ML MLE & EN RME PWM & ML MLE & EN | M | 221 229 952 952 150 162 599 103 325 325 3065 072 2215 | 242 .29 251 .29 986 1.15 172 .20 183 .23 5558 .74 105 .13 114 .14 357 .44 075 .09 082 .09 | 91 .314 99 .324 55 1.172 98 .224 16 .233 13 .785 12 .143 10 .150 12 .484 102 .102 109 .107 | . 424 . 429 1. 458 . 304 . 309 1. 130 . 200 . 204 . 701 . 144 . 147 . 485 | .492 .475 1.654 .352 1.281 .241 .233 .878 .168 .167 | .630 .541 1.813 .453 .389 1.423 .289 .259 .961 .213 .192 .736 | .778 .578 1.982 .523 .403 1.388 .346 .274 1.041 .239 .197 .754 |
| 10 20 50 | RME PWM & ML MLE & EN RME PWM & ML MLE & EN RME PWM & ML MLE & EN RME PWM & ML RME PWM & ML RME RME RME | M | 221 | 242 .2251 .29 286 1.15 172 .20 183 .23 5558 .74 105 .13 114 .14 357 .44 775 .09 248 .30 252 .06 | 91 .314 99 .324 95 1.172 188 .224 16 .233 13 .785 82 .143 10 .150 12 .484 10 .102 109 .107 189 .333 166 .073 | .424 .429 1.458 .304 .309 1.130 .200 .204 .701 .144 .147 .485 .104 | .492 .475 1.654 .352 1.281 .241 .233 .878 .168 .167 .587 | .630 .541 1.813 .453 .389 1.423 .289 .259 .961 .213 .192 .736 .152 | .778 .578 1.982 .523 .403 1.388 .346 .274 1.041 .239 .197 .754 |
| 10 20 50 | RME PWM & ML MLE & EN RME PWM & ML | M M M M M M M M M M M M M M M M M M M | 221 | 242 .2251 .29 986 1.15 172 .20 183 .23 5558 .76 105 .11 14 .14 357 .44 075 .09 82 .09 248 .30 255 .00 | 91 .314 99 .324 55 1.172 18 .224 16 .233 13 .785 82 .143 10 .150 12 .484 92 .102 19 .107 18 .333 16 .073 | .424 .429 1.458 .304 .309 1.130 .200 .204 .701 .144 .147 .485 .104 | .492 .475 1.654 .352 1.281 .241 .233 .878 .168 .167 | .630 .541 1.813 .453 .389 1.423 .289 .259 .961 .213 .192 .736 | .778 .578 1.982 .403 1.388 .346 .274 1.041 .239 .197 .754 .169 |
| 10 20 50 100 200 | RME PWM & ML MLE & EN | M M M M M M M M M M M M M M M M M M M | 221 | 242 .2251 .29 286 1.15 172 .20 183 .23 5558 .74 105 .13 114 .14 357 .44 775 .09 248 .30 252 .06 | 91 .314 99 .324 55 1.172 18 .224 16 .233 13 .785 82 .143 10 .150 12 .484 92 .102 19 .107 18 .333 16 .073 | .424 .429 1.458 .304 .309 1.130 .200 .204 .701 .144 .147 .485 .104 | .492 .475 1.654 .352 1.281 .241 .233 .878 .168 .167 .587 | .630 .541 1.813 .453 .389 1.423 .289 .259 .961 .213 .192 .736 .152 | .778 .578 1.982 .403 1.388 .346 .274 1.041 .239 .197 .754 .169 |
| 10 20 50 | RME PWM & ML MLE & EN RME PWM & ML | M T M | 221 | 242 .2251 .29 986 1.15 172 .20 183 .23 5558 .76 105 .11 14 .14 357 .44 075 .09 82 .09 248 .30 255 .00 | 91 .314 99 .324 55 1.172 08 .224 .66 .233 13 .785 12 .143 10 .150 12 .484 99 .107 98 .333 66 .073 66 .073 | .424 .429 1.458 .304 .309 1.130 .200 .204 .701 .144 .147 .485 .104 | .492 .475 1.654 .362 .352 1.281 .241 .233 .878 .168 .167 .587 .123 .121 .415 | .630 .541 1.813 .453 .389 1.423 .289 .259 .961 .213 .192 .736 .152 | .778 .578 1.982 .523 .403 1.388 .346 .274 1.041 .239 .197 .754 .165 |
| 10 20 50 100 200 | RME PWM & ML MLE & EN | M | 221 229 2952 209 . | 242 .29 2851 .29 986 1.15 172 .20 183 .23 5558 .74 105 .13 114 .14 357 .44 357 .49 082 .09 248 .30 052 .00 052 .00 077 .21 077 .21 | 91 .314 99 .324 55 1.172 28 .224 16 .233 13 .785 14 .150 12 .484 10 .150 12 .484 10 .102 10 .073 10 .073 10 .073 | .424 .429 1.458 .304 .309 1.130 .200 .204 .701 .144 .147 .485 .104 .331 .068 | .492 .475 1.654 .362 .352 1.281 .241 .233 .878 .167 .587 .123 .121 .415 | .630 .541 1.813 .453 .389 1.423 .259 .961 .213 .192 .736 .152 .141 .537 | .778 .578 1.982 .523 .403 1.386 .274 1.041 .239 .197 .754 .169 .145 |
| 10 20 50 100 200 | RME PWM & ML RME PWM & ML MLE & EN RME | M T | 221 | 242 .29 251 .29 986 1.15 172 .20 183 .21 5558 .74 105 .11 114 .14 357 .44 357 .49 359 .09 248 .30 355 .06 358 .07 358 .07 3 | 91 .314 99 .324 95 1.172 188 .224 16 .233 13 .785 82 .143 10 .150 12 .484 12 .102 99 .107 99 .073 10 .073 10 .073 10 .073 | . 424 . 429 1. 458 . 304 . 309 1. 130 . 200 . 204 . 701 . 144 . 147 . 485 . 104 . 331 | .492 .475 1.654 .362 .352 1.281 .241 .233 .878 .168 .167 .587 .123 .121 .415 | .630 .541 1.813 .453 .389 1.423 .289 .259 .961 .213 .192 .736 .152 | .778 .578 1.982 .523 .403 1.388 .346 .274 1.041 .239 .197 .754 .165 |

Table 5(Conted.)

| | | | | PROBA | BILITY | OF NON- | EXCEEDA | NCE = | . 990 | |
|------------------------------|---|---|--|--|---|--|--|--|---|--|
| n | METHOD | CV> | (.75) | (.80) | (.90) | (.95) | (1.25) | (1.5) | (2.0) | (2.5 |
| | | | PROBA | BILITY | OF EXC | CEEDANCE | = .9 | 90 | | |
| n | METHOD | | | | | | 4 | | | |
| 10 | RME | | .290 | .311 | .369 | .398 .482 | .517 | .586 | .704 | .83 |
| | PWM & | MLM | .362 | .382 | .448 | .482 | .630 | .712 | .810 | .87 |
| | MLE & | ENT | 1.021 | 1.050 | 1.218 | 1.232 | 1.510 | 1.703 | 1.856 | |
| 20 | RME | | .206 | 1.050 .229 .285 | .273 | .295 | .402 | .463 | .545 | . 60 |
| | PWM & | MLM | .260 | .285 | .328 | | | .555 | .621 | . 63 |
| | MLE & | | | .701 | .784 | .825 | | | 1.457 | 1.41 |
| 50 | RME | | .131 | .143 | .181 | .198 | .285 | | | .43 |
| | PWM & | MLM | .163 | .177 | .216 | .233 | .328 | | | .46 |
| | MLE & | | .348 | .380 | .466 | .233 .508 | .726 | .904 | | 1.06 |
| 100 | RME | | .092 | | .128 | .143 | .215 | .249 | .299 | .32 |
| | PWM & | MLM | .114 | | .154 | .166 | .215 .236 | .278 | .332 | .34 |
| | MLE & | | .230 | .264 | .324 | .350 | .502 | .605 | .754 | .77 |
| 200 | RME | | .066 | .073 | .092 | .103 | | .193 | | .24 |
| | PWM & | MLM | .081 | .090 | .109 | | .168 | | | .25 |
| | MLE & | | .160 | | .224 | | .343 | | | .56 |
| 500 | RME | | .042 | | .057 | .064 | .112 | .135 | .163 | .18 |
| | | MLM | .051 | | | | .107 .213 | | | .17 |
| | | | | | | | | | | |
| | MLE & | ENT | .099 | .114 | .139 | .151 | .213 | .261 | .337 | .38 |
| | MLE & | ENT | .099 | .114 | .139 | .151 OF NON- | | | | .38 |
| n | MIL & | | .099 | PROBA | .139 | | -EXCEEDA | NCE = | .999 | |
| | METHOD | | (.75) | .114 PROBA | .139 BILITY (| OF NON- | EXCEED# | (1.5) | .999 | (2.5 |
| n 10 | METHOD RME | | (.75) .459 | PROBA (.80) .481 | .139 BILITY ((.90) .550 | OF NON- (.95) | (1.25) .677 | (1.5) .736 | .999 (2.0) | (2.5 |
| | METHOD RME | CV> | (. 75) .459 | PROBA (.80) .481 .816 | .139 BILITY ((.90) .550 .984 | OF NON- (.95) .576 1.010 | (1.25) .677 1.311 | (1.5) .736 1.514 | .999 (2.0) .825 1.690 | (2.5 .93 1.86 |
| 10 | METHOD RME PWM & MLE & | CV> | (.75) .459 .773 | PROBA (.80) .481 .816 1.119 | .139 BILITY (.90) .550 .984 1.285 | OF NON- (.95) .576 1.010 1.295 | .677 1.311 1.565 | .736 1.514 1.754 | .999 (2.0) .825 1.690 1.900 | (2.5 .93 1.86 2.06 |
| | METHOD RME PWM & MLE & RME | CV> | (.75) .459 .773 | PROBA (.80) .481 .816 1.119 | .139 BILITY (.90) .550 .984 1.285 | OF NON- (.95) .576 1.010 1.295 .443 | .677 1.311 1.565 .575 | .736 1.514 1.754 .626 | .999 (2.0) .825 1.690 1.900 | (2.5 .93 1.86 2.06 |
| 10 | METHOD RME PWM & MLE & RME PWM & | CV> MLM ENT MLM | (.75) .459 .773 1.095 .321 .486 | .114 PROBA (.80) .481 .816 1.119 .354 .545 | .139 BILITY (.90) .550 .984 1.285 .414 .633 | OF NON- (.95) .576 1.010 1.295 .443 .676 | .677 1.311 1.565 .575 1.016 | (1.5) .736 1.514 1.754 .626 1.173 | .999 (2.0) .825 1.690 1.900 .690 1.327 | (2.5 .93 1.86 2.06 .73 |
| 10 20 | METHOD RME PWM & MLE & RME PWM & RME | CV> MLM ENT MLM | (.75) .459 .773 1.095 .321 .486 .689 | .114 PROBA (.80) .481 .816 1.119 .354 .545 .747 | .139 (.90) .550 .984 1.285 .414 .633 .827 | .576 1.010 1.295 .443 .676 | (1.25) .677 1.311 1.565 .575 1.016 1.213 | (1.5) .736 1.514 1.754 .626 1.173 1.358 | .999 (2.0) .825 1.690 1.900 .690 1.327 1.492 | .93 1.86 2.06 .73 1.30 |
| 10 | METHOD RME PWM & RME RME PWM & MLE & RME | CV> MLM ENT MLM ENT | (.75) .459 .773 1.095 .321 .486 .689 | .114 PROBA (.80) .481 .816 1.119 .354 .545 .747 .215 | .139 (.90) .550 .984 1.285 .414 .633 .827 .277 | .576 1.010 1.295 .443 .676 .867 | (1.25) .677 1.311 1.565 .575 1.016 1.213 .440 | .736 1.514 1.754 .626 1.173 1.358 .491 | .999 (2.0) .825 1.690 1.900 .690 1.327 1.492 .531 | .93 1.86 2.06 .73 1.30 1.44 |
| 10 20 | METHOD RME PWM & RME PWM & RME PWM & RME RME PWM & | CV> MLM ENT MLM ENT | (.75) .459 .773 1.095 .321 .486 .689 .195 | .114 PROBA (.80) .481 .816 1.119 .354 .545 .747 .215 .295 | .139 (.90) .550 .984 1.285 .414 .633 .827 .277 | .576 1.010 1.295 .443 .676 .867 .311 | .677 1.311 1.565 .575 1.016 1.213 .440 .631 | (1.5) .736 1.514 1.754 6.626 1.173 1.358 .491 .804 | .999 (2.0) .825 1.690 1.900 .690 1.327 1.492 .531 .896 | .93 1.86 2.06 .73 1.30 1.44 .57 |
| 10 20 50 | METHOD RME PWM & MLE & RME PWM & MLE & RME PWM & MLE & RME | CV> MLM ENT MLM ENT | (.75) .459 .773 1.095 .321 .486 .689 .195 .264 | .114 PROBA (.80) .481 .816 1.119 .354 .545 .747 .215 .295 .405 | .139 (.90) .550 .984 1.285 .414 .633 .827 .277 .377 .492 | .576 1.010 1.295 .443 .676 .867 .311 .417 | .677 1.311 1.565 .575 1.016 1.213 .440 .631 .753 | .736 1.514 1.754 .626 1.173 1.358 .491 .804 | .999 (2.0) .825 1.690 1.900 .690 1.327 1.492 .531 .896 1.007 | (2.5 .93 1.86 2.06 .73 1.30 1.44 .57 .97 |
| 10 20 | METHOD RME PWM & MLE & RME PWM & RME PWM & RME RME PWM & RME | CV> MLM ENT MLM ENT | (.75) .459 .773 1.095 .321 .486 .689 .195 .264 | .114 PROBA (.80) .481 .816 1.119 .354 .545 .747 .215 .295 .405 .155 | .139 BILITY (.90) .550 .984 1.285 .414 .633 .827 .277 .377 .492 .199 | 0F NON- (.95) .576 1.010 1.295 .443 .676 .867 .311 .417 .534 | .677 1.311 1.565 .575 1.016 1.213 .440 .631 .753 .352 | .736 1.514 1.754 .626 1.173 1.358 .491 .804 | .999 (2.0) .825 1.690 1.900 .690 1.327 1.492 .531 .896 1.007 .440 | (2.5 .93 1.86 2.06 .73 1.30 1.44 .57 .97 |
| 10 20 50 | METHOD RME PWM & MLE & RME PWM & RME RME PWM & RME PWM & RME | CV> MLM ENT MLM ENT MLM ENT MLM ENT | (.75) .459 .773 1.095 .321 .486 .689 .195 .264 .374 | .114 PROBA (.80) .481 .816 1.119 .354 .545 .747 .215 .295 .405 .155 .205 | .139 BILITY (.90) .550 .984 1.285 .414 .633 .827 .277 .377 .492 .199 .262 | 0F NON- (.95) .576 1.010 1.295 .443 .676 .867 .311 .417 .534 .225 .287 | .677 1.311 1.565 .575 1.016 1.213 .440 .631 .753 .352 .436 | .736 1.514 1.754 .626 1.173 1.358 .491 .804 .931 .391 | .999 (2.0) .825 1.690 1.900 .690 1.327 1.492 .531 .896 1.007 .440 .686 | (2.5 .93 1.86 2.06 .73 1.30 1.44 .57 .97 1.08 |
| 10 20 50 | METHOD RME PWM & RME RME | CV> MLM ENT MLM ENT MLM ENT MLM ENT | (.75) .459 .773 1.095 .321 .486 .689 .195 .264 .374 .134 | .114 PROBA (.80) .481 .816 1.119 .354 .545 .747 .215 .295 .4055 .155 .205 .281 | .139 BILITY (.90) .550 .984 1.285 .414 .633 .827 .277 .377 .492 .199 .262 .342 | 0F NON- (.95) .576 1.010 1.295 .443 .676 .867 .311 .417 .534 .225 .287 .367 | .677 1.311 1.565 .575 1.016 1.213 .440 .631 .753 .352 .436 .521 | .736 1.514 1.754 .626 1.173 1.358 .491 .804 .931 .391 .538 | .999 (2.0) .825 1.690 1.900 .690 1.327 1.492 .531 .896 1.007 .440 .686 | (2.5 .93 1.86 2.06 .73 1.30 1.44 .57 .97 1.08 .46 .70 |
| 10 20 50 | METHOD RME PWM & RME PWM & RME RME PWM & RME PWM & RME RME RME RME RME RME RME RME | MLM ENT MLM ENT MLM ENT | (.75) .459 .773 1.095 .321 .486 .689 .195 .264 .374 .135 .174 .247 | .114 PROBA (.80) .481 .816 1.119 .354 .545 .747 .215 .295 .405 .1555 .205 .281 .110 | .139 BILITY (.90) .550 .984 1.285 .414 .633 .827 .277 .377 .492 .199 .262 .342 .143 | 0F NON- (.95) .576 1.010 1.295 .443 .676 .867 .311 .417 .534 .225 .287 .367 .162 | .677 1.311 1.565 .575 1.016 1.213 .440 .631 .753 .352 .436 .521 .273 | .736 1.514 1.754 .626 1.173 1.358 .491 .804 .931 .391 .538 .623 | .999 (2.0) .825 1.690 1.900 .690 1.327 1.492 .531 .896 1.007 .440 .686 .772 .361 | (2.5 .93 1.86 2.06 .73 1.30 1.44 .57 .97 1.08 .40 .70 .78 .38 |
| 10 20 50 | METHOD RME PWM & RME PWM & RME PWM & RME PWM & RME RME PWM & RME PWM & RME | CV> MLM ENT MLM ENT MLM ENT MLM ENT MLM ENT | (.75) .459 .773 1.095 .321 .486 .689 .195 .264 .374 .135 .174 .247 .095 | PROBA (.80) .481 .816 1.119 .354 .545 .747 .215 .295 .405 .155 .205 .281 .110 .142 | .139 BILITY (.90) .550 .984 1.285 .414 .633 .827 .277 .377 .492 .199 .262 .342 .143 .181 | 0F NON- (.95) .576 1.010 1.295 .443 .676 .867 .311 .417 .534 .225 .287 .367 .162 .200 | .677 1.311 1.565 .575 1.016 1.213 .440 .631 .753 .352 .436 .521 .273 .298 | .736 1.514 1.754 .626 1.173 1.358 .491 .804 .931 .391 .538 .623 .321 | .999 (2.0) .825 1.690 1.900 .690 1.327 1.492 .531 .896 1.007 .440 .686 .772 .361 .500 | (2.5 .93 1.86 2.06 .73 1.30 1.44 .57 .97 1.08 .40 .70 .78 .38 .51 |
| 10 20 50 100 200 | METHOD RME PWM & RME PWM & RME PWM & RME PWM & RME RME PWM & RME PWM & RME RME PWM & RME | CV> MLM ENT MLM ENT MLM ENT MLM ENT MLM ENT | (.75) .459 .773 1.095 .321 .486 .689 .195 .264 .374 .135 .174 .247 | .114 PROBA (.80) .481 .816 1.119 .354 .545 .747 .215 .295 .405 .155 .205 .281 .110 .142 .195 | .139 (.90) .550 .984 1.285 .414 .633 .827 .277 .377 .492 .199 .262 .342 .343 .181 .237 | 0F NON- (.95) .576 1.010 1.295 .443 .676 .867 .311 .417 .534 .225 .287 .367 .162 .200 .256 | (1.25) .677 1.311 1.565 .575 1.016 1.213 .440 .631 .753 .352 .436 .521 .273 .298 .355 | .736 1.514 1.754 .626 1.173 1.358 .491 .804 .931 .391 .538 .623 .321 .380 .441 | .999 (2.0) .825 1.690 1.900 .690 1.327 1.492 .531 .896 1.007 .440 .686 .772 .361 .500 .563 | (2.5 .93 1.86 2.06 .73 1.30 1.44 .57 .97 1.08 .46 .70 .78 .38 .51 |
| 10 20 50 | METHOD RME PWM & RME PWM & RME PWM & RME PWM & RME RME PWM & RME PWM & RME RME PWM & RME | CV> MLM ENT MLM ENT MLM ENT MLM ENT | (.75) .459 .773 1.095 .321 .486 .689 .195 .264 .374 .135 .174 .247 .095 | .114 PROBA (.80) .481 .816 1.119 .354 .545 .747 .215 .295 .405 .155 .205 .281 .110 .142 .195 .069 | .139 BILITY (.90) .550 .984 1.285 .414 .633 .827 .277 .377 .492 .199 .262 .342 .143 .181 .237 .090 | 0F NON- (.95) .576 1.010 1.295 .443 .676 .867 .311 .417 .534 .225 .287 .367 .162 .200 .256 .102 | (1.25) .677 1.311 1.565 .575 1.016 1.213 .440 .631 .753 .352 .436 .521 .273 .298 .355 .198 | .736 1.514 1.754 .626 1.173 1.358 .491 .804 .931 .391 .538 .623 .321 .380 .441 .241 | .999 (2.0) .825 1.690 1.900 .690 1.327 1.492 .531 .896 1.007 .440 .686 .772 .361 .500 .563 .276 | (2.5 .93 1.86 2.06 .73 1.30 1.44 .57 .97 1.08 .46 .70 .78 .38 .51 .57 |
| 10 20 50 100 200 | METHOD RME PWM & RME PWM & RME PWM & RME PWM & RME RME PWM & RME PWM & RME RME PWM & RME | CV> MLM ENT MLM ENT MLM ENT MLM ENT MLM ENT MLM ENT | (.75) .459 .773 1.095 .321 .486 .689 .195 .264 .374 .135 .174 .247 | .114 PROBA (.80) .481 .816 1.119 .354 .545 .747 .215 .295 .405 .155 .205 .281 .110 .142 .195 | .139 (.90) .550 .984 1.285 .414 .633 .827 .277 .377 .492 .199 .262 .342 .343 .181 .237 | 0F NON- (.95) .576 1.010 1.295 .443 .676 .867 .311 .417 .534 .225 .287 .367 .162 .200 .256 | (1.25) .677 1.311 1.565 .575 1.016 1.213 .440 .631 .753 .352 .436 .521 .273 .298 .355 .198 | .736 1.514 1.754 .626 1.173 1.358 .491 .804 .931 .391 .538 .623 .321 .380 .441 | .999 (2.0) .825 1.690 1.900 .690 1.327 1.492 .531 .896 1.007 .440 .686 .772 .361 .500 .563 | (2.5 .93 1.86 2.06 .73 1.30 1.44 .57 .97 1.08 .46 .70 .78 .38 .51 |

formed better for $N \ge 200$; the performance of ENT and MLE was not greatly inferior.

In terms of RMSE in parameter b, PWM and MLM performed in a uniformly superior manner for $CV \ge 0.95$ and for $N \ge 100$. For $CV \le 0.95$ and $N \ge 20$, RMSE produced by RME was the smallest of all the methods. However, overall all methods were somewhat comparable. Thus, one concludes that PWM and MLM are the preferred methods in terms of RMSE of parameters a and b for large values of CV and small sample sizes. For smaller values of CV and large sample sizes, RME would be the preferred method.

4.3 BIAS in Quantiles Estimates

The results of bias in quantile estimation for different probabilities of non-exceedance (P) are summarized in Table 4. Overall, PWM and MLM performed the best in terms of quantile bias for a range of values of the sample size, CV and the probability of non-exceedance (P). The next best method was RME, followed by MLE and ENT. In general, the quantile bias increased with increasing CV and increasing P but decreased with increasing sample size. For largesample sizes, $N \ge 200$, the quantile bias was small in all cases, regardless of the method. For $N \ge 20$, PWM and MLM exhibited uniformly lower bias for all P=s, sample sizes and CV=s. Thus, PWM or MLM would be the preferred method. If the sample size is more than 20 and $CV \le 0.95$, RME yielded small bias and would therefore be acceptable for practical purposes. For larger values of CV, the sample size would have to be much larger, say, greater than 200. ENT and MLE would be acceptable for sample size greater than 200 if P was less than 0.95 and CV was less than 2.5.

4.4 RMSE in Quantiles Estimates

The values of RMSE for different quantiles estimated by GPD2 are summarized in Table 5. RMSE of a given quantile for a given method varied with the sample size and the coefficient of variation. In general, for a given quantile, RMSE increased with CV, regardless of the sample size; of course, it decreased with increasing sample size. Furthermore, RMSE increased with increasing quantile for the same value of CV and sample size.

For P (the probability of non-exceedance) \geq 0.99, RME produced the least the least value of RMSE regardless of the sample size and the value of CV. The second lowest value of RMSE was produced by MLM and PWN and the highest value was produced by MLE and ENT. However, the reverse was true for P \leq 0.9. For large sample sizes $N \geq$ 200, RME became comparable to MLM and PWM for all values of CV and P. MLE and ENT did not perform in a comparable manner. Thus, it is concluded that for large floods and higher CVs, RME would be the preferred method, whereas, for smaller floods and lower Cvs, MLM and PWM would also be comparable to RME.

5. CONCLUDING REMARKS

The following conclusions are drawn from this study: PWM and MLM performed better than RME, ENT and MLE in general. In terms of parameter bias, PWM and MLM were uniformly better than ENT and MLE. This was also true of the methods for RMSE. In terms of quanile bias, PWM and MLM performed uniformly better. In terms of RMSE, RME performed better for large values of P and CV than did PWM and MLM and was the preferred method. However, for smaller CVs and low values of P. PWM

and MLM were comparable.

REFERENCES

- Barrett, J. H., 1992. An extreme value analysis of the flow of Burbage Brook. Stochastic Hydrology and Hydraulics, Vol. 6, pp. 151-165.
- Baxter, M. A., 1980. Minimum variance unbiased estimation of the parameter of the Pareto distribution. Biometrika, Vol. 27, pp. 133-138.
- Cook, W. L. and Mumme, D. C., 1981. Estimation of Pareto parameters by numerical methods. In Statistical Distributions in Scientific Work, C. Taillie et al (eds), Vol. 5, pp. 127-132.
- Davison, A. C., 1984a. Modelling excesses over high thresholds, with an application. In Statistical Extremes and Applications, J. Tiago de Oliveira (ed.), pp. 461-482.
- Davison, A. C., 1984b. A statistical model for contamination due to long-range atmospheric transport of radionuclides. unpublished Ph.D. thesis, Department of Mathematics, Imperial College of Science and Technology, London, England.
- Davison, A. C. and Smith, R. C., 1990. Models for exceedances over high thresholds. J. R. Statist. Soc. B, Vol. 52, No. 3, pp. 393-442.
- DuMouchel, W., 1983. Estimating the stable index in order to measure tail thickness. Ann. Statist., Vol. 11, pp. 1019-1036.
- Hosking, J. R. M. and Wallis, J. R., 1987. Parameter and quantile estimation for the generalized Pareto distribution. Technometrics, Vol. 29, No. 3, pp. 339-349.
- Joe, H., 1987. Estimation of quantiles of the maximum of N observations. Biometrika, Vol. 74, pp. 347-354.

- Kuczera, G., 1982a. Combining site-specific and regional information: An empirical Bayes approach. Water Resources Research, Vol. 18, No. 2, pp. 306-314.
- Kuczera, G., 1982b. Robust flood frequency models. Water Resources Research, Vol. 18 No. 2, pp. 315-324.
- Moharram, S. H., Gosain, A. K. and Kapoor, P. N., 1993. A comparative estimation of the generalized Pareto distribution. Journal of Hydrology, Vol. 150, pp. 169-185.
- Ochoa, I. D., Bryson, M. C. and Shen, H. W., 1980. On the occurrence and importace of Paretian-tailed distribution in hydrology. Journal of Hydrology, Vol. 48, pp. 53-62.
- Pickands, J., 1975. Statistical inference using extreme order statistics. Ann. Statist., Vol. 3, pp. 119-131.
- Quandt, R. E., 1966. Old and new methods of estimation of the Pareto distribution. Biometrika, Vol. 10, pp. 55-82.
- Rosbjerg, D., Madsen, H. and Rasmussen, P. F., 1992. Prediction in partial duration series with generalized Pareto-distributed exceedances. Water Resources Research, Vol. 28, No. 11, pp. 3001-3010.
- Saksena, S. K. and Johnson, A. M., 1984. Best unbiased estimators for the parameters of a two-parameter Pareto distribution. Biometrika, Vol. 31, pp. 77-83.
- Singh, V. P., 1998. Entropy-Based Parameter Estimation in Hydrology. Kluwer Academic Publishers, Boston.
- Singh, V. P. and Guo, H., 1995a. Parameter estimation for 2-parameter Pareto distribution by POME. Water Resources Management, Vol. 9, pp. 81-93.
- Singh, V. P. and Guo, H., 1995b. Parameter estimation for 3-parameter generalized Pareto distribution by the principle of maximum

- entropy (POME). Hydrological Sciences Journal, Vol. 40 (2), pp. 165-181.
- Singh, V. P. and Guo, H., 1997. Parameter estimation for 3-parameter generalized Pareto distribution by POME. Stochastic Hydrology and Hydraulics, Vol. 11, pp. 211-227.
- Singh, V. P. and Rajagopal, A. K., 1986. A new method of parameter estimation for hydrologic frequency analysis. Hydrological Science and Technology, Vol. 2, No. 3, pp. 33-40.
- Smith, J. A., 1991. Estimating the upper tail of flood frequency distributions. Water Resources Research, Vol. 23, No. 8, pp. 1657-1666.
- Smith, R. L., 1984. Threshold methods for sample extremes," In Statistical Extremes and Applications (ed. J. Trago de Oliveita), pp. 621-638.
- Smith, R. L., 1987. Estimating tails of probability distributions. Ann. Statist., Vol. 15, pp. 1174-1207.
- Van Montfort, M. A. J. V. and Witter, J. V., 1985.

- Testing exponentiality against generalized Pareto distribution. Journal of Hydrology, Vol. 78, pp. 305-315.
- Van Montfort, M. A. J. and Witter, J. W., 1986. The generalized pareto distribution applied to rainfall depths. Hydrological Sciences Journal, Vol. 31, No. 2, pp. 151-162.
- Van Montfort, M. A. J. and Witter, J. W., 1991. The first and the second e of the extreme value distribution, EV1. Stochastic Hydrology and Hydraulics, Vol. 5, pp. 69-76.
- Wang, Q. J., 1991. The POT model described by the generalized Pareto distribution with Poisson arrival rate. Journal of Hydrology, Vol.129, pp. 263-280.

Department of Civil and Environmental Engineering, Louisiana State University, Baton Rouge, LA70803-6405, U. S. A

(E-mail: cesing@lsu.edu)

Department of Civil Engineering, United Arab Emirates University, Al-Ain, UAE