

# 시뮬레이션 실험설계에서 분산감소기법의 응용

## Application of Variance Reduction Techniques in Designed Simulation Experiments\*

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### Abstract

We develop a variance reduction technique in one simulation experiment whose purpose is to estimate the parameters of a first-order linear model. This method utilizes the control variates obtained during the course of simulation run under Schruben and Margolin's method (S-M method). The performance of this method is shown to be similar in estimating the main effects, and to be superior to S-M method in estimating the overall mean response in the hospital simulation experiment. For the general case, we consider that a proposed method may yield a better result than S-M method if selected control variates are highly correlated with the response at each design point.

## 1. INTRODUCTION

The variance reduction techniques of common random numbers and antithetic variates have been used successfully in simulation experiments that are designed to estimate an hypothesized metamodel of the mean response of interest and levels of the input factors set by the simulation analyst. (Discussions of these two variance reduction techniques are given by Bratley, Fox and Schrage [1] and Law and Kelton [5].) Schruben and Margolin showed that, for first-order metamodels, the method of common random numbers across all design points in the experiment yields superior estimates

of the unknown parameters of main effects in the relationship to the method of conducting all simulation runs with independent, and randomly selected random number streams. Furthermore, they exploited the random number assignment rule which uses a combination of common random numbers and antithetic random number streams across all design points in a simulation experiment for first-order relationship whose design matrix admits orthogonal blocking into two blocks. Their assignment rule is superior to the use of common random numbers alone, and that of independent random number streams when we estimate the parameters for the main effects. However, in estimating the overall mean,

\* 본 연구는 1993년도 동아대학교 학술연구조성비에 의하여 이루어졌음.

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Schruben and Margolin's method (S-M method) may not be better than the independent streams for a certain case. The requisite assumptions as well as performance evaluations for their assignment rule have been documented by Schruben [11] and Tew and Wilson [13].

Also in simulation experiments, the method of control variates has been successfully applied to reduce the variability of the estimator of the mean response [1,4,7,10]. This method tries to take advantage of correlation between the response of interest and control variates (concomitant variables) obtained during the course of simulation run and to counteract the unknown variability of the estimator for the mean response of system. Thus, we consider the way of using a useful information of observed control variates in keeping with the benefit of blocking of S-M method.

As Schruben and Margolin noted, the efficiency gain of their method highly depends on the induced correlation between two responses in the same block. Also the simulation efficiency of the control variates method is determined by the correlation between the response and a set of control variates. Typically the control variates are observed independently on each setting of factors in the factor space. Therefore, in effectively using the control variates under the S-M method, the key issues are how to adjust the responses with the control variates and whether the adjusted responses show the similar correlation structure as the S-M method yields.

In this research, we propose a new method applying control variates to S-M rule in order to improve the simulation efficiency of the S-M method. We investigate conditions under which this method may yield better results than the S-M rule with respect to the unconditional variances of the estimator for the parameters of interest. We also explore the simulation efficiency of a proposed method through the simulation experiment on a selected model.

## 2. BACKGROUND AND NOTATION

In this section we provide the statistical framework necessary to formally define a simulation experiment and its associated simulation model. Usually the goals of simulation

study include either a determination of the settings for the input factors (experimental design points) that yields an optimal value of the system response or an understanding of the relationship between the response and the settings of input factors over the region of interest in the factor space. We consider simulation studies consisting of  $m$  design points and we run simulation  $n$  times at each design point. We let  $y_{ij}$  be the observed response from the  $j$ th replication at the  $i$ th design point. Also we let  $y_i$  be the mean response of the  $i$ th run. For the  $i$ th design point, the values of  $p$  interesting factors are specified by the design point  $x_i = (x_{i1}, x_{i2}, \dots, x_{ip})$  in the  $p$ -dimensional factor space.

In this paper, it is assumed that the relationship of the mean response to the factor settings is linear in unknown parameters. If we run a simulation  $m$  experimental points, the mean response at each design point can be expressed as follows:

$$y_i = \beta_0 + \beta_1 x_{i1} + \beta_2 x_{i2} + \dots + \beta_p x_{ip} + \epsilon_i, \quad i = 1, 2, \dots, m, \quad (1)$$

where  $\beta_i$  is the model parameter, and  $\epsilon_i$  is the error term. That is, the selection of  $m$  such experimental points constitutes the traditional experimental design. We now define the  $(m \times (p+1))$  design matrix  $X$  having a left column of 1's and element  $(i,k+1)$  equal to  $x_{ik}$ . Then the linear response model in (1) is given by

$$y = X\beta + \epsilon, \quad (2)$$

where  $y = (y_1, y_2, \dots, y_m)'$  is the vector of observed mean responses,  $\beta = (\beta_0, \beta_1, \dots, \beta_p)'$  is a vector of unknown parameters and  $\epsilon = (\epsilon_1, \epsilon_2, \dots, \epsilon_m)'$  is a vector of random errors. It is assumed that  $\epsilon_i$ 's are IID  $N(0, \sigma^2/n)$  for all experimental points. By a reparameterization of the factor level, the design matrix  $X$  may be chosen as an orthogonal matrix in the experimental design [12].

### 3. S-M METHOD

In computer simulation, an experimenter can control over the random number streams that drive a simulation model. The selection of streams of random numbers completely determines the simulation output. We let the random number streams  $r_{ij}$  denote the sequence of the random numbers having the uniform distribution  $U(0,1)$ . Assume that the simulation model requires  $g$  such random number streams to drive all of its stochastic components for a single replication at each design point. Also let  $R_i$  be the set of  $g$  random number streams for the  $i$ th replication:  $R_i = (r_{i1}, r_{i2}, \dots, r_{ig})$  ( $i=1, 2, \dots, n$ ).

When two replications are made with independent streams either at the design points or within each design point, two responses have zero correlation. If we use the common random numbers for the  $i$ th replication at two design points, a positive correlation of  $\rho_+$  is induced between two observations of the responses [1,11,12]. On the other hand, using the antithetic set of streams for the  $i$ th replication at two design points induces a negative correlation of  $\rho_-$  between two observations of the responses [2,5,11,12].

For the first order linear model in (2), Schruben and Margolin exploited the random number assignment rule which uses a combination of common random numbers and antithetic streams in a simulation experiment designed to estimate the parameters  $\beta$  when the design matrix  $X$  admits orthogonal blocking into two blocks. For the  $i$ th replication, S-M rule uses (a) the same set of random  $R_i$  across all  $m_1$  design points in the first block, and (b) the same set of antithetic random number streams  $(1-R_i)$  across all  $m_2$  design points in the second block ( $m=m_1+m_2$ ). Under the assumptions that (a) induced correlations  $\rho_+$  and  $\rho_-$  are constant, and (b)  $\rho_+ \geq -\rho_- > 0$ , the covariance matrix of the mean responses  $y = (y_1, y_2, \dots, y_m)'$  is given by

$$\begin{aligned} \text{Cov}(y) &= \sigma_y^2/n \begin{pmatrix} 1 & \rho_+ & \vdots & \rho_+ & \rho_- & \rho_- & \vdots & \rho_- \\ \rho_+ & 1 & \vdots & \rho_+ & \rho_- & \rho_- & \vdots & \rho_- \\ \vdots & \vdots & \ddots & \vdots & \vdots & \vdots & \ddots & \vdots \\ \rho_+ & \rho_+ & \vdots & 1 & \rho_- & \rho_- & \vdots & \rho_- \\ \rho_- & \rho_- & \vdots & \rho_- & 1 & \rho_+ & \vdots & \rho_- \\ \rho_- & \rho_- & \vdots & \rho_- & \rho_+ & 1 & \vdots & \rho_- \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \ddots & \vdots \\ \rho_- & \rho_- & \vdots & \rho_- & \rho_+ & \rho_+ & \vdots & 1 \end{pmatrix} \\ &= \sigma_y^2/n [(\rho_+ + \rho_-) \mathbf{XGX}'/2 + (\rho_+ + \rho_-) \mathbf{ZZ}'/2 + (1 - \rho_+) \mathbf{I}_m], \end{aligned} \tag{3}$$

where  $G$  is a  $(p+1) \times (p+1)$  matrix whose first row and first column entry is 1 with all other entries 0, and  $z$  is a  $(m \times 1)$  vector whose first  $m_1$  elements are 1's and remaining  $m_2$  elements are -1's (see equation (16) on p.245 in [12]). For the dispersion matrix given as above, it is known that the ordinary least squares (OLS) estimators of  $\beta$  in (2) and the weighted least squares (WLS) estimators are identical (see equation (63) in [9]). Schruben and Margolin [12] showed that the covariance matrix of estimator for  $\beta$  is given as follows

$$\text{Cov}(\hat{\beta}) = \sigma_y^2/n [(\rho_+ + \rho_-)G/2 + (1 - \rho_+)(X'X)^{-1}]. \tag{4}$$

With respect to the design criterion of D-optimality, Schruben and Margolin's assignment rule (S-M rule) yields the OLS estimator of  $\beta$  with a smaller D-value than the assignment of (a) one common random numbers to all design points, or (b) a different streams to each design point for the  $i$ th replication under a certain condition, respectively. However, comparing the covariance matrix of the estimators indicates that S-M method may yield the greater variance of estimator for  $\beta_0$  than independent streams for a certain case.

As we see the equation (4), the efficiency gain of S-M method highly depends on the induced correlation  $\rho_+$  between two responses in the same block. Thus, to be effective in applying the control variates method in conjunction with S-M method, we are concerned (a) whether the correlation between two adjusted responses in the same block is reduced or not, and (b) how effective the controls are in reducing

the variance of the mean response of each design point.

#### 4. APPLICATION OF CONTROL VARIATES TO S-M RULE

During the course of simulation run, often we can obtain the concomitant variables (control variates) which are strongly correlated with the response of interest at a little additional cost. Typically, controls are observed independently at each of the levels of factor variables during the experiment, and the mean of each control is known. We let  $c_{ij}$  be a vector of  $s$  controls corresponding to  $y_{ij}$  and  $c_i$  be the  $(s \times 1)$  mean vector of  $c_{ij}$ 's ( $j=1,2,\dots,n$ ). When the length of the simulation run is sufficiently large at each design point, it seems reasonable to assume that the mean response  $y_i$ , ( $i=1, 2, \dots, m$ ) and  $s$  mean control vector  $c_i$  ( $i=1, 2, \dots, m$ ) have the  $(s+1)$ -variate normal distribution:  $(y_i, c_i)' \sim N_{s+1}((\mu_{y_i}, \mu_c)', \Sigma)$ ; where

$$\Sigma = \frac{1}{n} \begin{pmatrix} \sigma_y^2 & \sigma'_{yc} \\ \sigma_{yc} & \Sigma_c \end{pmatrix}; \tag{5}$$

$\sigma_{yc}$  is a covariance between  $y_1$  and  $c_1$ ; and  $\Sigma_c$  is a covariance of  $c_1$  [4,7,11].

Under this assumption, we try to counteract an unknown deviation of  $(y_i - \mu_{y_i})$  by subtracting a known deviation ( $c_i - \mu_c$ ) from  $y_i$ . That is, the adjusted response of the  $i$ th design point is given by

$$y_1(\alpha_1) = y_1 - \alpha_1'(c_1 - \mu_c), \tag{6}$$

where  $\alpha_1$  is a coefficient vector of controls. The value of  $\alpha_1$  which minimizes  $\text{Var}(y_1(\alpha_1))$  is known to be  $\alpha_1 = \Sigma_c^{-1} \sigma_{yc}$ , and the resulting variance is  $\text{Var}(y_1(\alpha_1)) = (1 - R_{yc}^2) \sigma^2$ , where  $R_{yc}^2 = \sigma^2 \sigma'_{yc} \Sigma_c^{-1} \sigma_{yc}$  [4].

Thus the adjusted responses  $y_1(\alpha_1)$  ( $i=1,2,\dots,m$ ) across  $m$  design points have the  $m$ -variates normal distribution. Also conditing on the controls, the adjusted mean response at each design point is an unbiased estimator of the mean response [3]. Therefore, similarly as we assume the linear response model of (2), the adjusted mean responses can be written as

the linear model given by

$$y(\Lambda) = X\beta + \epsilon^*, \tag{7}$$

where  $y(\Lambda) = (y_1(\alpha_1), y_2(\alpha_2), \dots, y_m(\alpha_m))'$  and  $\epsilon^*$  is a vector of error terms.

Since the S-M rule uses the commom random numbers to drive the stochastic components of the simulation model for the factor setting in the same block, it allows the same controls for the design points in the same block. That is, the observation of the mean control variates across the  $m$  design points for the  $n$  replications is given by

$$C = \begin{pmatrix} c_1 \\ c_2 \\ \vdots \\ c_{m_1} \\ c_{m_1+1} \\ \vdots \\ c_m \end{pmatrix} = \begin{pmatrix} c_1 \\ c_1 \\ \vdots \\ c_1 \\ c_{m_1+1} \\ \vdots \\ c_{m_1+1} \end{pmatrix},$$

where the first  $m_1$  design points are in the first block, and the second  $m_2 (= m - m_1)$  design points are in the second block. The controls of two design points in the different blocks are negatively correlated. Thus a covariance structure of the adjusted mean responses is quite different from that of the mean responses obtained by S-M rule directly. To identify the covariance of  $y(\Lambda)$ , we first establish the relationships between the response and controls, and between controls across the design points and replicates as follows:

Property 1: Homogeneity of response across replicates,

$$\text{Var}(y_{ij}) = \sigma_y^2 \text{ for } i=1, 2, \dots, m \text{ and } j=1, 2, \dots, n.$$

Property 2: Homogeneity of response covariances across replicates in either the same block or the different blocks,

$$\text{Cov}(y_{ii}, y_{kl}) = \begin{cases} \rho - \sigma_y^2 & \text{for design points } i \text{ and } k \\ & \text{in the same block, and } j=1, \\ \rho - \sigma_y^2 & \text{for design points } i \text{ and } k \\ & \text{in the different block, and } j=1, \\ 0, & \text{otherwise.} \end{cases}$$

Property 3: Homogeneity of response-control covariances across replicates in either the same block or the different blocks, and independence of the response and control variates observed on different replicates,

$$\text{Cov}(y_{ij}, c_{ki}) = \begin{cases} \sigma_{yc}' & \text{for design points } i \text{ and } k \\ & \text{in the same block, and } j=1. \\ \sigma_{yc}^* & \text{for design points } i \text{ and } k \\ & \text{in the different block, and } j=1. \\ 0' & \text{otherwise.} \end{cases}$$

Property 4: Homogeneity of control variates covariances across design points and replicates,

$$\text{Cov}(c_{ij}) = \Sigma_c \text{ for } i = 1, 2, \dots, m, \text{ and } k = 1, 2, \dots, n.$$

Property 5: Homogeneity of control-variates covariances across replicates in either the same block or the different blocks, and independence of the control variates observed on different replicates,

$$\text{Cov}(c_{ij}, c_{kl}) = \begin{cases} \Sigma_c & \text{for design points } i \text{ and } k \\ & \text{in the same block, and } j=1. \\ \Sigma_c^* & \text{for design points } i \text{ and } k \\ & \text{in the different block, and } j=1. \\ 0_{\text{SSS}} & \text{otherwise.} \end{cases}$$

Properties 1 and 2 are adopted from the assumptions established by Schruben and Margolin [12]. Similarly to these relationships, we establish Properties 3, 4 and 5. Under the Properties 1-5, we consider the covariance structure of the adjusted responses for the cases that the optimal coefficient vector of control variates is known and unknown.

When the optimal value of  $\alpha = \Sigma_c^{-1} \sigma_{yc}$  is known, the variance of the mean controlled response at the *i*th design point given by

$$\text{Var}(y_i - c_i' \alpha) = \text{Var}\left(\sum_{j=1}^n y_{ij}/n - \sum_{j=1}^n c_{ij}' \alpha/n\right) = \sum_{j=1}^n \text{Var}(y_{ij} - c_{ij}' \alpha)/n^2 \tag{8}$$

by Property 3. If we develop this equation, and replace  $\alpha$  with  $\Sigma_c^{-1} \sigma_{yc}$ , then we find, by Property 3,

$$\text{Var}(y_i - c_i' \alpha) = \sum_{j=1}^n \{\text{Var}(y_{ij}) - 2\text{Cov}(y_{ij}, c_{ij}' \alpha) + \alpha' \text{Cov}(c_{ij}, c_{ij}' \alpha)\}/n^2$$

$$\begin{aligned} & (c_{ij}) \alpha' \}/n^2 \\ & = \sum_{j=1}^n (\sigma_y^2 - 2\sigma_{yc}' \alpha + \alpha' \Sigma_c \alpha)/n^2 = \sigma_y^2 (1 - R_{yc}^2)/n, \end{aligned} \tag{9}$$

where  $R_{yc}^2 = \sigma_y^{-2} \sigma_{yc}' \Sigma_c^{-1} \sigma_{yc}$  is the multiple correlation coefficient between  $y_{ij}$  and  $c_{ij}$ . This equation shows that the response adjusted by the control variates with known coefficient  $\alpha$  has a variance reduced by  $(1 - R_{yc}^2)$  over that given by in (3). By the Corollary 5.2.1 in Mood, Graybill and Boes [6], the covariance between two controlled responses of the design points *i* and *k* in the same block is also given by

$$\begin{aligned} \text{Cov}(y_i - c_i' \alpha, y_k - c_k' \alpha) &= \text{Cov}(y_i, y_k) - \text{Cov}(y_i, c_k' \alpha) \\ &\quad - \text{Cov}(y_k, c_i' \alpha) + \alpha' \text{Cov}(c_i, c_k) \alpha, \end{aligned} \tag{10}$$

where each term is developed as follows:

$$\begin{aligned} \text{Cov}(y_i, y_k) &= \text{Cov}\left(\sum_{j=1}^n y_{ij}/n, \sum_{l=1}^n y_{kl}/n\right) = \sum_{j=1}^n \sum_{l=1}^n \text{Cov}(y_{ij}, y_{kl})/n^2 \\ &= \sum_{j=1}^n \text{Cov}(y_{ij}, y_{ij})/n^2 = \rho + \sigma_y^2/n \text{ (by properties 1 and 2);} \end{aligned} \tag{11}$$

$$\text{Cov}(y_i, c_k' \alpha) = \text{Cov}\left(\sum_{j=1}^n y_{ij}/n, \sum_{l=1}^n c_{kl}' \alpha/n\right) = \sum_{j=1}^n \sum_{l=1}^n \text{Cov}(y_{ij}, c_{kl}' \alpha)/n^2$$

which reduces to, by Property 3 and replacement of  $\alpha$  into this equation,

$$\text{Cov}(y_i, c_k' \alpha) = \sum_{j=1}^n \text{Cov}(y_{ij}, c_{kj}' \alpha)/n^2 = \sigma_{yc}' \Sigma_c^{-1} \sigma_{yc} /n; \tag{12}$$

Similar to this equation, we have

$$\text{Cov}(y_k, c_i' \alpha) = \sigma_{yc}' \Sigma_c^{-1} \sigma_{yc} /n; \tag{13}$$

$$\begin{aligned} \alpha' \text{Cov}(c_i, c_k) \alpha &= \alpha' \text{Cov}\left(\sum_{j=1}^n c_{ij}/n, \sum_{l=1}^n c_{kl}/n\right) = \alpha' \sum_{j=1}^n \text{Cov}(c_{ij}, c_{kj}) \alpha \\ &= \sigma_{yc}' \Sigma_c^{-1} \sigma_{yc} /n, \end{aligned} \tag{14}$$

by Properties 4 and 5, and substitution of  $\alpha$  with  $\Sigma_c^{-1}\sigma_{y_c}$ . Plugging (11)-(14) into (10) gives that

$$\text{Cov}(y_i - c_i'\alpha, y_k - c_k'\alpha) = (\rho_+ \sigma_y^2 - \sigma_{y_c}' \Sigma_c^{-1} \sigma_{y_c}) / n = (\rho_+ - R_{y_c}^*) \sigma_y^2 / n. \tag{15}$$

As we see in this equation, the covariance between two controlled responses in the same block also decreases by the same amount as in the variance reduction of the controlled response in (3). If two controlled responses at design points  $i$  and  $k$  are not in the same block, in the similar procedures given above, we find each term in (10) as follows:

$$\text{Cov}(y_i, y_k) = \rho_- \sigma_y^2 / n \text{ (by Property 2);} \tag{16}$$

$$\text{Cov}(y_i, c_k'\alpha) = \sum_{j=1}^n \text{Cov}(y_{ij}, c_{kj}'\alpha) / n^2 = \sigma_{y_c}' \Sigma_c^{-1} \sigma_{y_c} / n \text{ (by Property 3);} \tag{17}$$

$$\text{Cov}(y_i, c_k'\alpha) = \sum_{j=1}^n \text{Cov}(y_{ij}, c_{kj}'\alpha) / n^2 = \sigma_{y_c}' \Sigma_c^{-1} \sigma_{y_c} / n \text{ (by Property 3);} \tag{18}$$

$$\alpha' \text{Cov}(c_i, c_k)\alpha = \sigma_{y_c}' \Sigma_c^{-1} \Sigma_c^* \Sigma_c^{-1} \sigma_{y_c} / n \text{ (by Properties 3, 4 and 5).} \tag{19}$$

Substitution of each term in (10) with equations (16)-(19) yields

$$\text{Cov}(y_i - c_i'\alpha, y_k - c_k'\alpha) = (\rho_- \sigma_y^2 - 2\sigma_{y_c}' \Sigma_c^{-1} \sigma_{y_c}^* + \sigma_{y_c}' \Sigma_c^{-1} \Sigma_c^* \Sigma_c^{-1} \sigma_{y_c}) / n = \sigma_y^2 (\rho_- - R_{y_c}^*) / n, \tag{20}$$

where  $R_{y_c}^* = \sigma_y^{-2} (2\sigma_{y_c}' \Sigma_c^{-1} \sigma_{y_c}^* - \sigma_{y_c}' \Sigma_c^{-1} \Sigma_c^* \Sigma_c^{-1} \sigma_{y_c})$ . The term  $\sigma_y^2 R_{y_c}^*$  can be interpreted as a difference between the covariance of the two responses and that of the two responses adjusted by the control variates when there exist the correlations among  $y_i, c_i, y_k,$  and  $c_k$ . For the case of a single control variate ( $s=1$ ), the term  $R_{y_c}^*$  can be written as

$$R_{y_c}^* = \sigma_y^{-2} \sigma_c^{-2} \{ 2\sigma_{y_c} \sigma_{y_c}^* - \sigma_{y_c}^2 (-\rho_c \sigma_c^2) \sigma_c^{-2} \} = 2\rho_{y_c} \rho_{y_c}^* + \rho_c \rho_{y_c}^2; \tag{21}$$

where  $\rho_{y_c}$  is the correlation coefficient between  $y_{ij}$ , and  $c_{ij}$ ;  $\rho_{y_c}^*$  is the correlation coefficient between  $y_{ij}$ , and  $c_{kj}$  which are in two different blocks;  $-\rho_c$  ( $\rho_c > 0$ ) is the correlation coefficient between  $c_{ij}$  and  $c_{kj}$  in two different blocks. Instead of identifying the relationship among  $\rho_{y_c}, \rho_{y_c}^*$  and  $\rho_c$  analytically, we compute this relationship based on the data set obtained from the simulation run given the example. The computational results show that  $\rho_{y_c}^* \doteq \rho_c \rho_{y_c}$ . When this relationship holds, we get

$$R_{y_c}^* \doteq -2\rho_c \rho_{y_c}^2 + \rho_c \rho_{y_c}^2 = -\rho_c \rho_{y_c}^2 < 0, \tag{22}$$

which implies the negative correlation between the two controlled responses in the two different blocks is reduced by approximately  $\rho_c \rho_{y_c}^2$  for the case of a single control variate.

We now consider the covariance matrix of the controlled responses across the  $m$  design points. From equations (9), (15) and (20), if we divide the covariance matrix by the variance of the controlled response in (9), then we obtain the covariance matrix of the  $m$  controlled responses as follows:

$$\text{Cov}(y(A)) = (1 - R_{y_c}^2) \sigma_y^2 / n$$

$$\begin{pmatrix} 1 & r & \dots & r & q & q & \dots & q \\ r & 1 & \dots & r & q & q & \dots & q \\ \vdots & \vdots & \ddots & \vdots & \vdots & \vdots & \ddots & \vdots \\ r & r & \dots & 1 & q & q & \dots & q \\ q & q & \dots & q & 1 & r & \dots & r \\ q & q & \dots & q & r & 1 & \dots & r \\ \vdots & \vdots & \ddots & \vdots & \vdots & \vdots & \ddots & \vdots \\ q & q & \dots & q & r & r & \dots & 1 \end{pmatrix} \tag{23}$$

where  $y(A) = y - C\alpha$ ,  $r = (\rho_+ - R_{y_c}^2) / (1 - R_{y_c}^2)$  and  $q = (\rho_- - R_{y_c}^*) / (1 - R_{y_c}^2)$ . This covariance matrix can be written in another form given by

$$\text{Cov}(y(A)) = (1 - R_{y_c}^2) \sigma_y^2 / n [(r+q)XGX'/2 + (r+q)zz'/2 + (1-r)I_m], \tag{24}$$

where  $G$  and  $z$  are defined in (3). For a dispersion matrix having the above pattern, the weighted least squares estimator

for  $\beta$  is equal to the OLS estimator:  $\beta = (X'X)^{-1}X'y(A)$ . Taking the variance operation on the estimator of  $\beta$  and substituting  $Cov(y(A))$  yields

$$\begin{aligned} Cov(\hat{\beta}) &= (X'X)^{-1}X'Cov(y(A))X(X'X)^{-1} \\ &= \sigma^2y(1-R_{yc^2})(X'X)^{-1}[(r+q)XGX/2 + (r+q) \\ &\quad zz'/2 + (1-r)I_m]X(X'X)^{-1} \\ &= \sigma^2y(1-R_{yc^2})/n [(r+q)G/2 + (1-r)(X'X)^{-1}] \end{aligned}$$

since  $X'z = z'X = 0$ . Substitution for  $r$  and  $q$  in (23) into the above equation finally gives

$$\begin{aligned} Cov(\hat{\beta}) &= \sigma^2y(1-R_{yc^2})/n [\{(\rho_+ - R_{yc^2})/(1 - R_{yc^2}) \\ &\quad + (\rho_- - R_{yc^*})/(1-R_{yc^2})\}G/2 \\ &\quad + \{1 - (\rho_+ - R_{yc^2})/(1 - R_{yc^2})\}(X'X)^{-1}] \\ &= \sigma^2y[\{(\rho_+ + \rho_-) - (R_{yc^2} + R_{yc^*})\}G/2 + (1- \\ &\quad \rho_+)(X'X)^{-1}], \end{aligned}$$

where  $R_{yc^*} = \sigma_y^{-2}(2\sigma_{yc}\Sigma_c^{-1}\sigma_{yc}^* - \sigma_{yc}\Sigma_c^{-1}\Sigma_c^* \Sigma_c^{-1}\sigma_{yc})$ . Comparing this equation with equation (3), we note that the variances of  $(\beta_1, \beta_2, \dots, \beta_p)$  are same as those obtained by S-M rule, but the variance of  $\beta_0$  is less than that in (4) if  $R_{yc^2} + R_{yc^*} > 0$ . Under the relationship in (22), this condition holds for the case that  $s=1$  since

$$R_{yc^2} + R_{yc^*} = \rho^2_{yc} - \rho_c \rho_{yc^2} = (1 - \rho_c)\rho_{yc^2} > 0. \quad (26)$$

We next consider a more practical situation that the optimal value of  $\alpha$  is unknown. In this case, we have to estimate it by its sample analogue. That is, for the  $i$ th design point, we estimate it by

$$\hat{\alpha}_i = \hat{\Sigma}_{c(i)} \hat{\sigma}_{yc(i)} \quad (27)$$

where  $\hat{\Sigma}_{c(i)} = \sum_{j=1}^n (c_{ij} - c_1)(c_{ij} - c_1)/(n-1)$  and  $\hat{\sigma}_{yc(i)} = \sum_{j=1}^n (y_{ij} - y_1)(c_{ij} - c_1)/(n-1)$ .

Then the adjusted mean response at the  $i$ th design point is given by

$$y_i(\hat{\alpha}_i) = (y_i - \hat{\alpha}_i' c_i). \quad (28)$$

It is known that the  $y_i(\hat{\alpha}_i)$  is the unbiased estimator of mean response for the  $i$ th design point and has the normal distribution [4]. Given the control variates  $c_i$ , we can obtain the sample covariance matrix of the adjusted response as follows:

$$\widehat{Cov}(y(A)) = \sum_{j=1}^n \{y(j) - y(\hat{\alpha})\} \{y(j) - y(\hat{\alpha})\}'$$

where  $y(j) = [y_{1j}(\hat{\alpha}_1), y_{2j}(\hat{\alpha}_2), \dots, y_{mj}(\hat{\alpha}_m)]'$  and  $y(\hat{\alpha}) = \sum_{i=1}^m y_i(\hat{\alpha})/n$  is the mean vector of the adjusted responses across the  $m$  design points.

Different from the known case of  $\alpha$ , it is not easy to get the covariance matrix of the estimator  $\beta$  unconditionally on the observed control variates by using similar procedures for obtaining the equation (25). Thus, instead of deriving the unconditional covariance of  $\beta$ , given  $c_i$  ( $i=1, 2, \dots, n$ ), we compute the sample covariance of the estimator,

$$Cov(\hat{\beta}) = (X'X)^{-1}X'\widehat{Cov}(y(A))X(X'X)^{-1}$$

and compare this result with that obtained by S-M method without applying control variates. We note that for a single design point, if we estimate the unknown  $\alpha_1$ , then the variance of its mean response is increased by the amount of  $(n-2)/(n-s-2)$ , where  $s$  is the number of control variates (see the discussions of loss factor in [4]). Therefore, if this factor is not negligible, the variance of the mean response at each design point achieved by the control variates should compensate the variance increment of the estimator due to the estimation of  $\alpha_1$  for the preference of this method to S-M method.

## 5. EXAMPLE

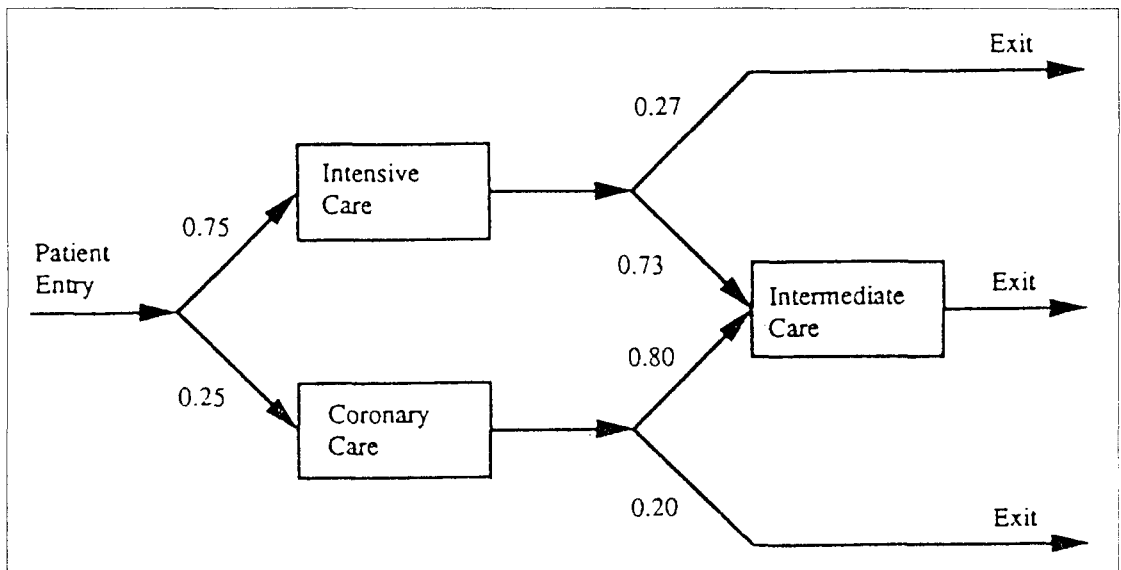
### 5.1 Description of System and Model

To compare the performances of the proposed method and the S-M method, we conduct the simulation experiment on

the hospital resource allocation model originally given by Schruben and Masrgolin [12]. <Figure 1> shows the operation of the hospital unit in terms of patient path types of resource (see Figure A in [12]). The hospital unit consists of three types of resources that are devoted to specialized care: intensive care, coronary care and intermediate care. Patients arrive at the hospital unit according to a poisson process with an arrival rate of 3.3 per day. Upon entering the hospital, 75% of the patients need intensive care, and 25% need coronary care. The service time distribution at intensive care is lognormal with mean 3.4 days and standard

a new facility to provide better service to the patients. The administration's decision is complicated by conflicting interest of several groups since no one knows how the numbers of each type of bed will affect the frequency with which the patients can not be accommodated. To help resolve this conflict, a statistically designed simulation experiment is conducted.

To estimate the effect of the number of beds of three types to failure rate of the patients, Schruben and Margolin considered a linear model including a overall mean, all main effects and pairwise interactions, and implemented  $2^3$  factorial design: three factors (three types of beds) having two levels



<Figure 1> Hospital Resource Allocation Model

deviation 1.6 days. After intensive care, 27% of the patients leave the hospital and 73% go to the intermediate care unit. Intermediate care stay for intensive care is distributed lognormally with mean 15.0 days and standard deviation 7.0 days. Finally, the length of intermediate care for coronary patients is distributed lognormally with mean 17.0 days and standard deviation 3.0 days. When the patients admission to special care units which are unavailable, they can not be accommodated and balk from the system.

The hospital administration now considers construction of

for each factor. The experimental conditions for the eight design points are given in <Table 1>. Their simulation results show that two factor interaction effects are negligible.

Based on these results, we also consider the linear model consisting only of the overall mean ( $\beta_0$ ) and all main main effects ( $\beta_1, \beta_2, \beta_3$ ). We used the same simulation output obtained by S-M method and additionally collected a single standardized control of the interarrival time of the patients to the system (see the definition of the standardized control variates in [14]). This control variate is independent of three



<Table 1> Experimental Design Points in 2<sup>3</sup> Factorial Design

Experimental DesignPoint		Number of Beds (Intensive)	Number of beds (Coronary)	Number of Beds (Intermediate)
Block 1	1	13(-1)	4(-1)	15(-1)
	2	13(-1)	6(+1)	17(+1)
	3	15(+1)	4(-1)	17(+1)
	4	15(+1)	6(+1)	15(-1)
Block 2	5	13(-1)	4(-1)	17(+1)
	6	13(-1)	6(+1)	15(-1)
	7	15(+1)	4(-1)	15(-1)
	8	15(+1)	6(+1)	17(-1)

factor variables since we use different number streams for driving the arrival process of the patient to the system. The adjusted response of interest (failure rate of patient) at the *i*th design point is given by

$$y_i(\hat{\alpha}_i) = y_i - \hat{\alpha}_i c_i,$$

where  $y_i$  is the mean response observed by the S-M method,  $\hat{\alpha}_i$  is the estimator of the coefficient of the control (see equation (27)), and  $c_i$  is the mean control variate. We assume that the adjusted response,  $y_i(\hat{\alpha}_i)$ , can be described by the linear model as follows:

$$y_i(\hat{\alpha}_i) = \beta_0 + \beta_1 x_{i1} + \beta_2 x_{i2} + \beta_3 x_{i3} + \epsilon_i, \quad i = 1, 2, \dots, 8, \quad (30)$$

where  $\beta_0$  is the overall mean;  $\beta_j$  is the main effect of the *j*th factor variable (number of the specialized care beds);  $x_{ij}$  is 1 (-1) if the *j*th factor is at the high (low) level for a design point *i* (by a reparameterization of the factor variables); and the  $\epsilon_i$  is the error term. Clearly the (8x4) design matrix  $X=(x_{ij})$  in <Table 1> admits the orthogonal blocking into two blocks. We partitioned the  $X$  into two blocks: the first block includes the design points 1-4, and the second block includes the design points 5-8.

We coded this model in SLAM II and conducted the 200 replications independently at a given design point according to the random number assignment rule of S-M method. We

simulate this system for 1500 days. To reduce the initial bias, we collected the necessary statistics after a warm period of length 300 time units.

### 5.2 Experimental Results and Inferences

The variances of the responses at the eight points are in the range from 1.88 to 2.19 for the S-M method, and those of the controlled responses for the proposed method are in the range from 0.43 to 0.67. As we expected, the latter method substantially reduces the variances in estimating the mean responses across all design points. Tables 2 and 3 show the sample correlation matrices obtained by two methods. The S-M method yields the correlation coefficients in the range from 0.98 to 0.99 between responses in the same block, and from -0.54 to -0.51 between responses in different blocks. From <Table 3>, we note that the correlations between two controlled responses in the same block are in the range from 0.92 to 0.98, and those from two different blocks are in the range from -0.24 to -0.20 for the proposed method. To explore the notion that the induced correlations are consistent with that developed in equation (23), we estimated the appropriate statistics:  $\hat{\rho}_+ = 0.985$  and  $\hat{R}_{yc} = -0.867$ . Then, from equation (23), the correlation coefficient between the two controlled responses in the same block is esmated by

$$(\hat{\rho}_+ - \hat{R}_{yc}^2)/(1 - \hat{R}_{yc}^2) = (0.985 - 0.767)/(1 - 0.767) = 0.94.$$

〈Table 2〉 Correlation Matrix of Responses: S-M method

	$y_1$	$y_2$	$y_3$	$y_4$	$y_5$	$y_6$	$y_7$	$y_8$
$y_1$	1.000	0.986	0.989	0.981	-0.540	-0.528	-0.539	-0.527
$y_2$	0.986	1.000	0.980	0.989	-0.540	-0.526	-0.540	-0.526
$y_3$	0.989	0.980	1.000	0.986	-0.525	-0.514	-0.526	-0.513
$y_4$	0.981	0.989	0.986	1.000	-0.530	-0.517	-0.531	-0.518
$y_5$	-0.540	-0.540	-0.525	-0.530	1.000	0.990	0.992	0.986
$y_6$	-0.528	-0.526	-0.514	-0.517	0.990	1.000	0.988	0.992
$y_7$	-0.539	-0.540	-0.526	-0.531	0.992	0.988	1.000	0.990
$y_8$	-0.527	-0.526	-0.513	-0.518	0.986	0.992	0.990	1.000

〈Table 3〉 Correlation Matrix of Responses: Proposed Method

	$y_1$	$y_2$	$y_3$	$y_4$	$y_5$	$y_6$	$y_7$	$y_8$
$y_1$	1.000	0.941	0.954	0.920	-0.219	-0.236	-0.229	-0.234
$y_2$	0.941	1.000	0.916	0.954	-0.194	-0.201	-0.210	-0.209
$y_3$	0.954	0.916	1.000	0.943	-0.208	-0.226	-0.223	-0.226
$y_4$	0.920	0.954	0.943	1.000	-0.214	-0.226	-0.233	-0.231
$y_5$	-0.219	-0.194	-0.208	-0.214	1.000	0.965	0.971	0.955
$y_6$	-0.236	-0.201	-0.226	-0.226	0.965	1.000	0.957	0.976
$y_7$	-0.229	-0.210	-0.223	-0.233	0.971	0.957	1.000	0.969
$y_8$	-0.234	-0.209	-0.226	-0.231	0.955	0.976	0.969	1.000

〈Table 4〉 Estimators for Model Parameters

Parameter	S-M rule	Proposed Method
$\beta_0$	45.722	45.670
$\beta_1$	-0.291	-0.290
$\beta_2$	-0.378	-0.378
$\beta_3$	-1.805	-1.805

〈Table 5〉 Variances of Estimators and D-Value of  $Cov(\hat{\beta})$

Parameter	S-M rule	Proposed Method
$\beta_0$	0.472	0.200
$\beta_1$	0.003	0.003
$\beta_2$	0.005	0.005
$\beta_3$	0.001	0.001
D-Value	$9.4 \times 10^{-9}$	$3.9 \times 10^{-9}$

responses in the same block. However, the same sort of conjecture is difficult to make for correlations between two controlled responses in the two different blocks since  $R_{yc}^{**}$  in (23) is a complex function of the control variates and responses.

We now compare the performances of the two methods with respect to the sample variances of the estimators, and the D-values of the sample covariance matrices. 〈Table 4〉 provides the estimators for the model parameters obtained by two methods, and 〈Table 5〉 presents their variances and the D-values of the estimators' covariance matrix. From 〈Table 4〉, we note (a) in estimating the overall mean response, the proposed method is superior to S-M method, and (b) in estimating the main factor effects, the performances of both methods are similar.

This result indicates that the simulation result in 〈Table 3〉 is consistent with that given equation (23) for two

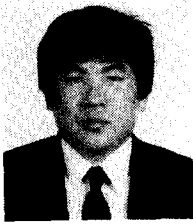
## 6. CONCLUSIONS

In applying the S-M method, the magnitude of the correlation between two responses in the same block is critical to the efficiency of this method in reducing the variances of the estimators for the main effects and interaction effects of the factor variables. The S-M method inflates the variance of estimator of the overall mean response when the difference between  $\rho_+$  and  $\rho_-$  is not small. The proposed method focuses on reducing the variance of the estimator for the overall mean response by the use of control variates in the application of the S-M rule. When the relationships between the response and controls are known, the combined method always yields better results than S-M method. Simulation results on the selected model indicate a promising evidence that a combined method may yield better results than S-M method even though we have to estimate the unknown coefficients of control variates. For the case that an effective set of controls can be identified and synchronization of the random number streams is difficult to achieve in the model, we consider that the combined method utilizing the control variates with S-M method yields better results than S-M method.

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