

분자의 사중극자모멘트의 계산 (제1보). 연산자법에
 의한 사중극자모멘트행렬요소의 계산

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Calculation of the Molecular Quadrupole Moments (I).
 Calculation for the Quadrupole Moment Matrix
 Elements by Operator Technique

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요 약. 연산자법을 사중극자모멘트행렬요소를 계산하는데 응용하였다.

Spherical harmonics의 전개방법과 사중극자모멘트행렬요소를 Mulliken의 overlap integral로 전환시키는 방법을 사용하여 Slater 궤도함수쌍에 대한 사중극자모멘트행렬요소의 기본식을 유도하였다.

두 방법에 의하여 계산한 사중극자모멘트행렬요소의 값이 일치하였으며 바닥상태의 HCl 분자에 대하여 계산한 사중극자모멘트의 값이 Nesbet의 값과 일치하였다.

ABSTRACT. Operator technique has been applied for calculation of the quadrupole moment matrix elements. Master formulas for the quadrupole moment matrix elements for pairs of Slater type orbitals are derived, one using the expansion method for spherical harmonics and the other the transformed of the quadrupole moment matrix elements into overlap integrals for Mulliken. The numerical values of the quadrupole moment matrix elements evaluated by two methods are in agreement with each other and the calculated quadrupole moment for the ground state of HCl molecule is also in agreement with that of Nesbet.

1. 서 론

Fig. 1에 나타난 것처럼 원점에서 Z_1 및 Z_2 떨어진 점에 위치하는 전하 e_1 및 e_2 로 인하여 임의의 점 P 에 생기는 퍼텐셜에너지는 다음 식으로 기술할 수 있다.¹

$$U = q\phi_0 - \mu_a F_a - \frac{1}{3} \theta_{\alpha\beta} F'_{\alpha\beta} - \frac{1}{15} \Omega_{\alpha\beta\gamma} F''_{\alpha\beta\gamma} \quad (1)$$

여기에서

$$\left. \begin{aligned} q &= \sum_i e_i \\ \mu_a &= \sum_i e_i r_i \\ \theta_{\alpha\beta} &= \frac{1}{2} \sum_i e_i (3r_{ia}r_{i\beta} - r_i^2 \delta_{\alpha\beta}) \\ \Omega_{\alpha\beta\gamma} &= \frac{1}{2} \sum_i e_i [5r_{ia}r_{i\beta}r_{i\gamma} \\ &\quad - (r_{ia}\delta_{\beta\gamma} + r_{i\beta}\delta_{\gamma\alpha} + r_{i\gamma}\delta_{\alpha\beta})] \end{aligned} \right\} (2)$$

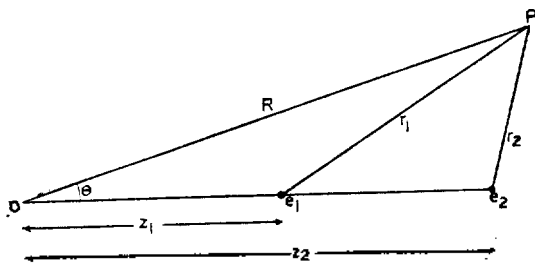


Fig. 1. The position of the arbitrary P relative to the origin O and the point charges e_1 and e_2 .

이며 $q, \mu_\alpha, \theta_{\alpha\beta}$ 및 $\Omega_{\alpha\beta\gamma}$ 는 각각 계의 전하, 쌍극자모멘트, 사중극자모멘트 및 팔중극자모멘트를 나타낸다.

Spherical harmonics 의 전개방법과 쌍극자모멘트행렬요소를 Mulliken 의 overlap integral 로 변환시키는 방법²에 의하여 쌍극자모멘트행렬요소를 계산하는 방법은 이미 보고 되었다.

사중극자모멘트는 전하에 대한 계의 모멘트(second moment)이며 9 개의 성분을 가진 tensor 이지만 이 tensor 는 대칭이고 또 트레이스가 없으므로 (symmetrical and traceless) 일반적으로 다음의 5 개의 독립적인 성분만을 가진다³.

$$\left. \begin{aligned} \theta_{\alpha\beta} &= \theta_{\beta\alpha} \\ \theta_{\alpha\alpha} &= \sum_{\alpha=x,y,z} \theta_{\alpha\alpha} = 0 \end{aligned} \right\} (3)$$

$$\theta_{\alpha\beta} = \begin{cases} \theta_{xx} & \theta_{xy} & \theta_{xz} \\ \theta_{yx} & \theta_{yy} & \theta_{yz} \\ \theta_{zx} & \theta_{zy} & \theta_{zz} \end{cases} \left. \begin{aligned} \theta_{xx} &= \theta_{zz} \\ \theta_{xy} &= \theta_{yx} \\ \theta_{yz} &= \theta_{zy} \\ \theta_{zz} &= -\theta_{xx} - \theta_{yy} \end{aligned} \right\} (4)$$

그러나 $\alpha \neq \beta$ 이면 $\theta_{\alpha\beta} = 0$ 가 되도록 서로 수직인 3 개의 축 (x, y 및 z) 을 택하는 것이 가능하며 이 경우 3 개의 주 사중극자 모멘트 θ_{xx}, θ_{yy} 및 θ_{zz} 만이 남게된다⁴.

$$\theta_{xx} = \frac{1}{2} \sum_i e_i (3x_i^2 - r_i^2) \quad (5)$$

$$\theta_{yy} = \frac{1}{2} \sum_i e_i (3y_i^2 - r_i^2) \quad (6)$$

$$\theta_{zz} = \frac{1}{2} \sum_i e_i (3z_i^2 - r_i^2) \quad (7)$$

만일 전하의 분포가 연속적이라면 식 (5)~(7) 에 있어서 전하의 합을 다음과 같이 전체 공간에

대한 전하밀도 $\rho(r)$ 의 적분으로 바꿀 수 있다.

$$\theta_{xx} = \frac{1}{2} \int (3x^2 - r^2) \rho(r) dr \quad (8)$$

$$\theta_{yy} = \frac{1}{2} \int (3y^2 - r^2) \rho(r) dr \quad (9)$$

$$\theta_{zz} = \frac{1}{2} \int (3z^2 - r^2) \rho(r) dr \quad (10)$$

선형분자(대칭축으로서 z 축을 가진 분자)의 경우

$$\theta_{xx} = -\frac{1}{2} \theta_{zz} = -\frac{1}{2} \theta_{yy} \quad (11)$$

이므로⁵ 이들 분자는 하나의 사중극자모멘트만을 가진다.

양자역학적으로 분자의 사중극자모멘트를 계산하기 위하여 분자의 사중극자모멘트를 핵기여분(nuclear part of the quadrupole moment)과 전자기여분(electronic part of the quadrupole moment)으로 나누어 생각하는 것이 편리하다.

$$\left. \begin{aligned} \theta_{xx} &= \frac{1}{2} \sum_i e_i (3Z_i^2 - R_i^2) \\ &\quad + \frac{1}{2} \int (3z^2 - r^2) \rho(r) dr \\ \theta_{xx} &= \frac{1}{2} \sum_i e_i (3X_i^2 - R_i^2) \\ &\quad + \frac{1}{2} \int (3x^2 - r^2) \rho(r) dr \\ \theta_{yy} &= \frac{1}{2} \sum_i e_i (3Y_i^2 - R_i^2) \\ &\quad + \frac{1}{2} \int (3y^2 - r^2) \rho(r) dr \end{aligned} \right\} (12)$$

(12)식의 첫째 항이 사중극자모멘트의 핵기여분이며 기준점으로 부터 원자핵 까지의 거리 R_i 의 성분 $Z_i, X_i,$ 및 Y_i 와 각 원자핵의 전하 e_i 를 알 수 있으므로 사중극자모멘트의 핵기여분은 쉽게 계산할 수 있다.

(12)식의 둘째 항이 사중극자모멘트에 대한 전자기여분이며 분자내의 전자전하의 분포가 균일하므로 사중극자모멘트의 전자기여분은 전자전하밀도 $\rho(r)$ 의 분포로부터

$$\rho(r) = -e \sum_i |\phi_i(r)|^2 \quad (13)$$

계산할 수 있다.^{6,7}

전자전하의 밀도를 계산하기 위하여 Slater 원

자래도함수와 Gaussian orbitals 을 basis sets 로 사용하여 얻은 SCF 분자래도함수가 사용되었다.⁴

근래에 Gaussian basis functions 을 사용한 ab initio SCF 계산, CNDO 계산^{9,10} Refined Extended Hückel 계산¹¹ 등에 의하여 전자전하의 밀도가 계산되었고 이로부터 분자의 사중극자모멘트의 전자기여분이 계산되었다.

본연구는 $\alpha \neq \beta$ 인 경우 $\theta_{\alpha\beta} = 0$ 가 되도록 서로 수직적인 좌표축을 택할 수 있는 분자에 대하여¹³ 연산자법 (operator technique) 에 의하여 Slater 래도함수에 대한 사중극자행렬요소를 계산하는 새로운 방법을 발전시키기 위하여 시도되었다.

2. 연산자법에 의한 사중극자모멘트행렬요소의 계산

양자역학적으로 분자의 사중극자 모멘트 텐서는 그 분자에 대한 사중극자 모멘트 텐서 연산자의 기대값(expectation value)이다.

$$\theta_{zz} = -e \sum_i \langle \Psi_i | \frac{1}{2} (3x_i^2 - r_i^2) | \Psi_i \rangle + \frac{1}{2} e \sum N_K (3Z_K^2 - R_K^2) \quad (14)$$

$$\theta_{xx} = -e \sum_i \langle \Psi_i | \frac{1}{2} (3x_i^2 - r_i^2) | \Psi_i \rangle + \frac{1}{2} e \sum N_K (3X_K^2 - R_K^2) \quad (15)$$

$$\theta_{yy} = -e \sum_i \langle \Psi_i | \frac{1}{2} (3y_i^2 - r_i^2) | \Psi_i \rangle + \frac{1}{2} e \sum N_K (3Y_K^2 - R_K^2) \quad (16)$$

여기에서 N_K 는 K 원자핵의 전하이코 Z_K , X_K , Y_K 는 각각 원자핵 K 의 x , y , z 축 좌표이며 Ψ_i 는 원자래도함수를 basis function 으로 사용하여 얻은 분자래도함수이다.

$$\Psi_i = \sum_{\mu} C_{\mu i} \phi_{\mu} \quad (17)$$

따라서 x , y 및 z 축 방향의 사중극자모멘트는 다음식으로 나타낼 수 있다.¹²

$$\theta_{zz} = -e \sum_i \sum_{\mu} \sum_{\nu} C_{\mu i} C_{\nu i} \langle \phi_{\mu} | \frac{1}{2} (3x_i^2 - r_i^2) | \phi_{\nu} \rangle + \frac{1}{2} e \sum N_K (3Z_K^2 - R_K^2) \quad (18)$$

$$\theta_{xx} = -e \sum_i \sum_{\mu} \sum_{\nu} C_{\mu i} C_{\nu i} \langle \phi_{\mu} | \frac{1}{2} (3x_i^2 - r_i^2) | \phi_{\nu} \rangle$$

$$+ \frac{1}{2} e \sum N_K (3X_K^2 - R_K^2) \quad (19)$$

$$\theta_{yy} = -e \sum_i \sum_{\mu} \sum_{\nu} C_{\mu i} C_{\nu i} \langle \phi_{\mu} | \frac{1}{2} (3y_i^2 - r_i^2) | \phi_{\nu} \rangle + \frac{1}{2} e \sum N_K (3Y_K^2 - R_K^2) \quad (20)$$

여기에서 $\langle \phi_{\mu} | \frac{1}{2} (3x_i^2 - r_i^2) | \phi_{\nu} \rangle$, $\langle \phi_{\mu} | \frac{1}{2} (3x_i^2 - r_i^2) | \phi_{\nu} \rangle$ 및 $\langle \phi_{\mu} | \frac{1}{2} (3y_i^2 - r_i^2) | \phi_{\nu} \rangle$ 을 x , y 및 z 축 방향의 사중극자모멘트행렬요소라고 부른다.

Spherical Harmonics 의 전개 방법. Spherical harmonics 의 전개 방법에 의하여 사중극자모멘트행렬요소를 계산하기 위하여 사중극자모멘트 연산자를 spherical harmonics 의 꼴로 바꾸는 것이 편리하다.¹⁴

$$\hat{\theta}_{zz} = \frac{1}{2} (3z^2 - r^2) = \left(\frac{4\pi}{5}\right)^{1/2} r^2 Y_{20}(\theta, \phi) \quad (21)$$

$$\hat{\theta}_{xx} = \frac{1}{2} (3x^2 - r^2) = -\frac{1}{2} (3z^2 - r^2) + \frac{3}{2} (x^2 - y^2) = -\frac{1}{2} \left(\frac{4\pi}{5}\right)^{1/2} r^2 Y_{20}(\theta, \phi) + \left(\frac{4\pi}{5}\right)^{1/2} r^2 [Y_{2-2}(\theta, \phi) + Y_{22}(\theta, \phi)] \quad (22)$$

$$\hat{\theta}_{yy} = \frac{1}{2} (3y^2 - r^2) = -\frac{1}{2} \left(\frac{4\pi}{5}\right)^{1/2} r^2 Y_{20}(\theta, \phi) - \left(\frac{4\pi}{5}\right)^{1/2} r^2 [Y_{2-2}(\theta, \phi) + Y_{22}(\theta, \phi)] \quad (23)$$

따라서 기준점 A 에 있어서 (Fig. 2) x , y 및 z 축 방향의 주 사중극자모멘트행렬요소는 다음식으로 나타낼 수 있다.

$$\theta_{zz} = \langle \phi_A | \hat{\theta}_{zz} | \phi_B \rangle = C \langle \phi_A | r^2 Y_{20}(\theta_2, \phi_2) | \phi_B \rangle \quad (24)$$

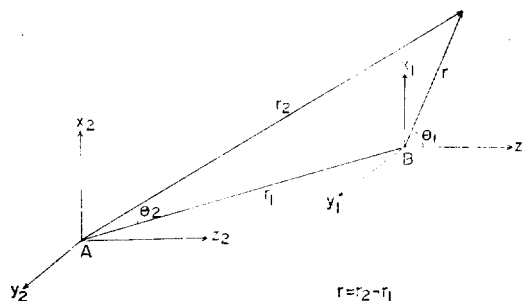


Fig. 2. The coordinate system for the two center integral.

$$\begin{aligned} \theta_{xx} &= \langle \phi_A | \hat{\theta}_{xx} | \phi_B \rangle \\ &= -\frac{1}{2} C \langle \phi_A | r_2^2 Y_{20}(\theta_2, \phi_2) | \phi_B \rangle \\ &\quad + C \langle \phi_A | r_2^2 [Y_{2-2}(\theta_2, \phi_2) \\ &\quad + Y_{22}(\theta_2, \phi_2)] | \phi_B \rangle \\ &= -\frac{1}{2} C \langle \phi_A | r_2^2 Y_{20}(\theta_2, \phi_2) | \phi_B \rangle \\ &\quad + C \{ \langle \phi_A | r_2^2 Y_{2-2}(\theta_2, \phi_2) | \phi_B \rangle \\ &\quad + \langle \phi_A | r_2^2 Y_{22}(\theta_2, \phi_2) | \phi_B \rangle \} \end{aligned} \quad (25)$$

$$\begin{aligned} \theta_{yy} &= \langle \phi_A | \hat{\theta}_{yy} | \phi_B \rangle \\ &= -\frac{1}{2} C \langle \phi_A | r_2^2 Y_{20}(\theta_2, \phi_2) | \phi_B \rangle \\ &\quad - C \langle \phi_A | r_2^2 [Y_{2-2}(\theta_2, \phi_2) \\ &\quad + Y_{22}(\theta_2, \phi_2)] | \phi_B \rangle \\ &= -\frac{1}{2} C \langle \phi_A | r_2^2 Y_{20}(\theta_2, \phi_2) | \phi_B \rangle \\ &\quad - C \{ \langle \phi_A | r_2^2 Y_{2-2}(\theta_2, \phi_2) | \phi_B \rangle \\ &\quad + \langle \phi_A | r_2^2 Y_{22}(\theta_2, \phi_2) | \phi_B \rangle \} \end{aligned} \quad (26)$$

여기에서 $C = \left(\frac{4\pi}{5}\right)$ 이며 $\langle \phi_A | r_2^2 Y_{2p}(\theta_2, \phi_2) | \phi_B \rangle$ 는 사중극자모멘트행렬요소의 허수꼴이다. 식 (27)로 정의한 ϕ_A 와 점 B 에 위치한 ϕ_B 를 기준점 A 에 대하여 전개한 식을 사중극자모멘트행렬요소의 허수꼴에 넣어주면 사중극자모멘트행렬요소의 허수꼴에 대한 일반식을 얻을 수 있다.

$$\begin{aligned} \phi_A &= M r^* \exp(-ar_2) Y_{l_3 m_3}(\theta_2, \phi_2) \\ |\phi_B\rangle &= N r^K \exp(-\beta r) Y_{l_4 m_4}(\theta, \phi) \\ &= 4\pi N \sum_{l_1=0}^l \sum_{l_2=0}^{l_1} \sum_{m_1} \sum_{m_2} (-1)^{l_1} \delta(l_1+l_2, l) \\ &\quad \left\{ \frac{4\pi (2l+1)!}{(2l_1+1)(2l_2+1)} \right\}^{1/2} \end{aligned} \quad (27)$$

$$\begin{aligned} \langle l_1 l_2 m_1 m_2 | l_1 l_2 m l \rangle &= \sum_{n=0}^{\infty} f_n(r_1, r_2) r_1^{l_1} r_2^{l_2} \\ &\quad \sum_{k=-n}^n Y_{nk}^*(\theta_1, \phi_1) Y_{l_1 m_1}(\theta_1, \phi_1) \\ &\quad Y_{nk}(\theta_2, \phi_2) Y_{l_2 m_2}(\theta_2, \phi_2) \end{aligned} \quad (28)$$

여기에서 $K=l$ 이면 $f_n(r_1, r_2) = b_n(r_1, r_2)$ 이고 $K=l+1$ 이면 $f_n(r_1, r_2) = x_n(r_1, r_2)$ 이며 $K=l+2$ 이면 $f_n(r_1, r_2) = h_n(r_1, r_2)$ 이다. ^{15,16)}

$$\begin{aligned} \langle \phi_A | r_2^2 Y_{2p}(\theta_2, \phi_2) | \phi_B \rangle &= NM \sum_{l_1=0}^l \sum_{l_2=0}^{l_1} \sum_{m_1} \sum_{m_2} \sum_{l_3} \sum_{m_3} \\ &\quad \delta(l_1+l_2, l) l_2^{-m+h+m_3+m_4} \\ &\quad r_1^{l_1} Y_{l_3 m_3}^*(\theta_1, \phi_1) \int_0^{\infty} f_n(r_1, r_2) r_2^{l_2+l_3+l_4} \\ &\quad \exp(-ar_2) dr_2 (2l+1)(2n+1)(2l_3+1) \\ &\quad \left\{ \frac{5(2l_3+1)(2l_4+1)(2l)!}{(2l_1)!(2l_2)!} \right\}^{1/2} \begin{pmatrix} l_1 & l_2 & l \\ m_1 m_2 & -m \end{pmatrix} \\ &\quad \begin{pmatrix} n & l_1 & l_4 \\ -h & m_1 m_4 \end{pmatrix} \begin{pmatrix} n & l_2 & l_5 \\ h & m_2 m_5 \end{pmatrix} \begin{pmatrix} l_2 & 2 & l_5 \\ -m_3 & p & m_3 \end{pmatrix} \begin{pmatrix} n & l_1 & l_4 \\ 0 & 0 & 0 \end{pmatrix} \\ &\quad \begin{pmatrix} n & l_2 & l_5 \\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} l_3 & 2 & l_5 \\ 0 & 0 & 0 \end{pmatrix} \end{aligned}$$

여기에서 $p=0$, 또는 ± 2 이다.

사중극자모멘트행렬요소의 허수꼴에 지름적분과 주어진 l_i, m_i, n, h 및 p 에 대응하는 3-j symbol 값을 넣어주면 사중극자모멘트행렬요소의 기본식을 얻을 수 있다. 이 기본식은 Table 1에 나타내었다.

사중극자모멘트행렬요소를 Mulliken의 Overlap Integral로 전환시키는 방법. 사중극자모멘트 연산자를 spherical harmonics의 꼴로 바꾸고 사중극자모멘트행렬요소의 bra 벡터 $\langle \phi_A |$ 를

Table 1. Master formulas for the quadrupole moment matrix elements.

$$\begin{aligned} \langle |s\rangle \hat{\theta}_{zz} |1s\rangle &= 2(\alpha/\beta)^{3/2} (2 \cos^2 \theta - \sin^2 \theta) V_2/\beta^2 \\ \langle 2s | \hat{\theta}_{zz} |1s\rangle &= \left(\frac{4}{3}\right)^{1/2} (\alpha/\beta)^{5/2} (2 \cos^2 \theta - \sin^2 \theta) W_2/\beta^2 \\ \langle 2p_z | \hat{\theta}_{zz} |1s\rangle &= \left(\frac{4}{5}\right) (\alpha/\beta)^{5/2} [2 \cos \theta W_1 + \frac{3}{2} (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) W_3]/\beta^2 \\ \langle 3s | \hat{\theta}_{zz} |1s\rangle &= \left(\frac{8}{45}\right)^{1/2} (\alpha/\beta)^{7/2} (2 \cos^2 \theta - \sin^2 \theta) S_2/\beta^2 \\ \langle 3p_z | \hat{\theta}_{zz} |1s\rangle &= \left(\frac{32}{375}\right)^{1/2} (\alpha/\beta)^{7/2} [2 \cos \theta S_1 + \frac{3}{2} (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) S_3]/\beta^2 \\ \langle 2p_x | \hat{\theta}_{zz} |1s\rangle &= \left(\frac{4}{5}\right) (\alpha/\beta)^{5/2} [2 \sin \theta \cos \phi W_1 - \frac{3}{2} (4 \cos^2 \theta \sin \theta - \sin^3 \theta) \cos \phi W_3]/\beta^2 \end{aligned}$$

$$\begin{aligned}
\langle 2p_x | \hat{\theta}_{xx} | 1s \rangle &= \left(\frac{4}{5}\right) (\alpha/\beta)^{5/2} \{2 \sin \theta \sin \phi W_1 + \frac{3}{2} (4 \cos^2 \theta \sin \theta - \sin^3 \theta) \sin \phi W_3\} / \beta^2 \\
\langle 3d_{xz} | \hat{\theta}_{xx} | 1s \rangle &= \left(\frac{32}{225}\right)^{1/2} (\alpha/\beta)^{7/2} \{S_0 + \frac{5}{7} (2 \cos^2 \theta - \sin^2 \theta) S_2 + \frac{9}{28} (35 \cos^4 \theta - 3 \cos^2 \theta + 3) S_4\} / \beta^2 \\
\langle 3d_{xx} | \hat{\theta}_{xx} | 1s \rangle &= -\left(\frac{8}{147}\right)^{1/2} (\alpha/\beta)^{7/2} \{2 \sin \theta \cos \theta \cos \phi S_2 + 3 \sin \theta (7 \cos^3 \theta - 3 \cos \theta) \cos \phi S_4\} / \beta^2 \\
\langle 2s | \hat{\theta}_{xx} | 2s \rangle &= \left(\frac{2}{3}\right) (\alpha/\beta)^{5/2} \{2 \cos^2 \theta - \sin^2 \theta\} H_2 / \beta^2 \\
\langle 2p_x | \hat{\theta}_{xx} | 2s \rangle &= \left(\frac{48}{225}\right)^{1/2} (\alpha/\beta)^{5/2} \{2 \cos \theta H_1 + \frac{3}{2} (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) H_3\} / \beta^2 \\
\langle 3s | \hat{\theta}_{xx} | 2s \rangle &= \left(\frac{8}{135}\right)^{1/2} (\alpha/\beta)^{7/2} \{2 \cos^2 \theta - \sin^2 \theta\} I_2 / \beta^2 \\
\langle 3p_x | \hat{\theta}_{xx} | 2s \rangle &= \left(\frac{32}{1125}\right)^{1/2} (\alpha/\beta)^{7/2} \{2 \cos \theta I_1 + \frac{3}{2} (2 \cos^2 \theta - \sin^2 \theta) I_3\} / \beta^2 \\
\langle 2p_x | \hat{\theta}_{xx} | 2p_x \rangle &= \left(\frac{16}{75}\right)^{1/2} (\alpha/\beta)^{5/2} \{2 \sin \theta \cos \phi H_1 - \frac{3}{2} (4 \cos^2 \theta \sin \theta - \sin^3 \theta) \cos \phi H_3\} / \beta^2 \\
\langle 2p_z | \hat{\theta}_{xx} | 2p_x \rangle &= \left(\frac{16}{75}\right)^{1/2} (\alpha/\beta)^{5/2} \{2 \sin \theta \sin \phi H_1 + \frac{3}{2} (4 \cos^2 \theta \sin \theta - \sin^3 \theta) \sin \phi H_3\} / \beta^2 \\
\langle 3p_x | \hat{\theta}_{xx} | 2p_x \rangle &= \left(\frac{32}{1125}\right)^{1/2} (\alpha/\beta)^{7/2} \{2 \sin \theta \cos \phi I_1 - \frac{3}{2} (4 \cos^2 \theta \sin \theta - \sin^3 \theta) \cos \phi I_3\} / \beta^2 \\
\langle 3d_{xz} | \hat{\theta}_{xx} | 2p_x \rangle &= \left(\frac{32}{675}\right)^{1/2} (\alpha/\beta)^{7/2} \{I_0 + \frac{5}{7} (2 \cos^2 \theta - \sin^2 \theta) I_2 + \frac{9}{28} (35 \cos^4 \theta - 30 \cos^2 \theta + 3) I_4\} / \beta^2 \\
\langle 3d_{xx} | \hat{\theta}_{xx} | 2p_x \rangle &= -\left(\frac{8}{441}\right)^{1/2} (\alpha/\beta)^{7/2} \{2 \sin \theta \cos \theta \cos \phi I_2 + 3 \sin \theta (7 \cos^3 \theta - 3 \cos \theta) \cos \phi I_4\} / \beta^2 \\
\langle 2p_x | \hat{\theta}_{xx} | 2p_x \rangle &= \left(\frac{4}{15}\right) (\alpha/\beta)^{5/2} \{2S_0 + \frac{55}{14} (2 \cos^2 \theta - \sin^2 \theta) + \frac{9}{14} (35 \cos^4 \theta - 30 \cos^2 \theta + 3) - 2a [1 + (2 \cos^2 \theta - \sin^2 \theta)] \\
&\quad W_1 - \frac{9}{14} a [3(2 \cos^2 \theta - \sin^2 \theta) + (35 \cos^4 \theta - 30 \cos^2 \theta + 3)] W_3\} / \beta^2 \\
\langle 3p_x | \hat{\theta}_{xx} | 2p_x \rangle &= \left(\frac{128}{3375}\right)^{1/2} (\alpha/\beta)^{7/2} \{2X_0 + \frac{55}{14} (2 \cos^2 \theta - \sin^2 \theta) X_2 + \frac{9}{14} (35 \cos^4 \theta - 30 \cos^2 \theta + 3) X_4 \\
&\quad - 2[1 + (2 \cos^2 \theta - \sin^2 \theta)] a S_1 - \frac{9}{14} [3(2 \cos^2 \theta - \sin^2 \theta) + (35 \cos^4 \theta - 30 \cos^2 \theta + 3)] a W_3\} / \beta^2 \\
\langle 2p_x | \hat{\theta}_{xx} | 2p_x \rangle &= -\left(\frac{4}{5}\right) (\alpha/\beta)^{5/2} \left\{ \frac{11}{7} \cos \theta \sin \theta \cos \phi S_2 + \frac{15}{14} \sin \theta (7 \cos^3 \theta - 3 \cos \theta) \cos \phi S_4 + \cos \theta \sin \theta \cos \phi a W_1 \right. \\
&\quad \left. - \frac{3}{2} (4 \cos^3 \theta \sin \theta - \cos \theta \sin^3 \theta) \cos \phi a W_3 \right\} / \beta^2 \\
\langle 3p_x | \hat{\theta}_{xx} | 2p_x \rangle &= -\left(\frac{32}{375}\right)^{1/2} (\alpha/\beta)^{7/2} \left\{ \frac{11}{7} \cos \theta \sin \theta \cos \phi I_2 + \frac{15}{14} \sin \theta (7 \cos^3 \theta - 3 \cos \theta) \cos \phi I_4 + \cos \theta \sin \theta \cos \phi a H_1 \right. \\
&\quad \left. - \frac{3}{2} (4 \cos^3 \theta \sin \theta - \cos \theta \sin^3 \theta) \cos \phi a H_3 \right\} / \beta^2 \\
\langle 3d_{xz} | \hat{\theta}_{xx} | 2p_x \rangle &= \left(\frac{32}{225}\right)^{1/2} (\alpha/\beta)^{7/2} \left\{ \frac{11}{7} \cos \theta X_1 + (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) X_3 + \frac{5}{28} (63 \cos^5 \theta - 70 \cos^3 \theta - 15 \cos \theta) X_5 \right. \\
&\quad \left. - \cos \theta a S_0 - \frac{5}{7} (2 \cos^2 \theta - \sin^2 \theta) \cos a S_2 - \frac{9}{28} (35 \cos^4 \theta - 30 \cos^2 \theta + 3) \cos \theta a S_4 \right\} / \beta^2 \\
\langle 3d_{xx} | \hat{\theta}_{xx} | 2p_x \rangle &= -\left(\frac{32}{675}\right)^{1/2} (\alpha/\beta)^{7/2} \left\{ \frac{3}{7} \sin \theta \cos \phi X_1 + \frac{12}{5} (4 \cos^2 \theta \sin \theta - \sin^3 \theta) \cos \phi X_3 + \frac{15}{14} \sin \theta (21 \cos^4 \theta \right. \\
&\quad \left. - 14 \cos^2 \theta + 1) \cos^2 \theta \sin \theta \cos \phi X_5 - \frac{15}{7} \cos \theta a S_2 - \frac{45}{14} (4 \cos^3 \theta \sin \theta - \cos \theta \sin^3 \theta) \cos \phi a S_4 \right\} / \beta^2 \\
\langle 2p_x | \hat{\theta}_{xx} | 2p_x \rangle &= \left(\frac{4}{15}\right) (\alpha/\beta)^{5/2} \left\{ S_0 - \frac{5}{14} [5(2 \cos^2 \theta - \sin^2 \theta) - 2 \sin \theta \cos 2\phi] S_2 + \frac{3}{28} [3(35 \cos^4 \theta - 30 \cos^2 \theta + 3) \right. \\
&\quad \left. - 5 \sin^2 \theta (7 \cos^3 \theta - 3 \cos \theta) \cos 2\phi] S_4 - [1 - \frac{1}{2} (2 \cos^2 \theta - \sin^2 \theta) - \frac{5}{7} \sin^2 \theta \cos 2\phi] a W_1 \right.
\end{aligned}$$

$$\begin{aligned}
 & + \frac{3}{28} [12(2 \cos^2 \theta - \sin^2 \theta) - 3(35 \cos^4 \theta - 30 \cos^2 \theta + 3) + 5 \sin^2 \theta (7 \cos^3 \theta - 3 \cos \theta) \cos 2 \phi] a W_3 \Big\} / \beta^2 \\
 \langle 3d_{xz} | \hat{\theta}_{zz} | 2p_x \rangle & = \left(\frac{32}{675} \right)^{1/2} (\alpha/\beta)^{7/2} \left\{ \frac{3}{7} \cos \theta X_1 + \frac{4}{5} (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) X^2 - \frac{5}{28} [(63 \cos^5 \theta - 70 \cos^3 \theta + 15 \cos \theta) \right. \\
 & \quad - 21 \sin^2 \theta (3 \cos^3 \theta - \cos \theta) \cos 2 \phi] X_5 - \left[\frac{6}{7} \cos \theta - \frac{3}{7} (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) + \frac{15}{7} \cos \theta \sin^2 \theta \cos 2 \phi \right] a S_2 \\
 & \quad \left. - \left[\frac{5}{7} (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) + \frac{15}{4} \sin^2 \theta (3 \cos^3 \theta - \cos \theta) \cos^2 \phi \right] a S_4 \right\} / \beta^2 \\
 \langle 2p_y | \hat{\theta}_{xx} | 2p_y \rangle & = \left(\frac{4}{15} \right) (\alpha/\beta)^{5/2} \left\{ S_0 - \frac{5}{14} [5(2 \cos^2 \theta - \sin^2 \theta) + 2 \sin^2 \theta \cos 2 \phi] S_2 + \frac{3}{28} [3(35 \cos^4 \theta - 30 \cos^2 \theta + 3) \right. \\
 & \quad + 5 \sin^2 \theta (7 \cos^3 \theta - \cos \theta) \cos 2 \phi] S_4 - \left[1 - \frac{1}{2} (2 \cos^2 \theta - \sin^2 \theta) - \frac{5}{7} \sin^2 \theta \cos 2 \phi \right] a W_1 \\
 & \quad \left. + \frac{3}{28} [12(2 \cos^2 \theta - \sin^2 \theta) - 3(35 \cos^4 \theta - 30 \cos^2 \theta + 3) - 5 \sin^2 \theta (7 \cos \theta - 3 \cos \theta) \cos 2 \phi] a W_3 \right\} / \beta^2 \\
 \langle 3p_x | \hat{\theta}_{xx} | 2p_x \rangle & = \left(\frac{32}{375} \right)^{1/2} (\alpha/\beta)^{7/2} \left\{ X_0 - \frac{5}{14} [5(2 \cos^2 \theta - \sin^2 \theta) + 2 \sin^2 \theta \cos \phi] X_2 + \frac{3}{28} [3(35 \cos^4 \theta - 30 \cos^2 \theta + 3) \right. \\
 & \quad + 5 \sin^2 \theta (7 \cos^3 \theta - 3 \cos \theta) \cos 2 \phi] X_4 - \left[1 - \frac{1}{2} (2 \cos^2 \theta - \sin^2 \theta) - \frac{5}{7} \sin^2 \theta \cos 2 \phi \right] a S_1 \\
 & \quad \left. + \frac{3}{38} [12(2 \cos^2 \theta - \sin^2 \theta) - 3(35 \cos^4 \theta - 30 \cos^2 \theta + 3) - 5 \sin^2 \theta (7 \cos^3 \theta - 3 \cos \theta) \cos 2 \phi] a S_3 \right\} / \beta^2 \\
 \langle 3d_{yz} | \hat{\theta}_{xx} | 2p_x \rangle & = \left(\frac{32}{675} \right)^{1/2} (\alpha/\beta)^{7/2} \left\{ \frac{3}{7} \cos X_1 + \frac{4}{5} (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) X_3 - \frac{5}{28} (63 \cos^5 \theta - 70 \cos^3 \theta + 15 \cos \theta) \right. \\
 & \quad + 21 \sin^2 \theta (3 \cos^3 \theta - \cos \theta) \cos 2 \phi] X_5 - \frac{3}{7} [2 \cos \theta - (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) - 5 \cos \theta \sin^2 \theta \cos 2 \phi] a S_2 \\
 & \quad \left. - 5 \left[\frac{1}{7} (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) - \frac{3}{4} \sin^2 \theta (3 \cos^3 \theta - \cos \theta) \cos 2 \phi \right] a S_4 \right\} / \beta^2 \\
 \langle 3s | \hat{\theta}_{xx} | 3s \rangle & = \left(\frac{4}{45} \right) (\alpha/\beta)^{7/2} (2 \cos^2 \theta - \sin^2 \theta) Y_2 \\
 \langle 3p_x | \hat{\theta}_{xx} | 3s \rangle & = \left(\frac{64}{16875} \right)^{1/2} (\alpha/\beta)^{7/2} (2 \cos \theta Y_1 + \frac{3}{2} (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) Y_3) / \beta^2 \\
 \langle 3p_x | \hat{\theta}_{xx} | 3s \rangle & = \left(\frac{64}{16875} \right)^{1/2} (\alpha/\beta)^{7/2} (2 \sin \theta \cos \phi Y_1 - \frac{3}{2} (4 \cos^2 \theta \sin \theta - \sin^3 \theta) \cos \phi Y_3) / \beta^2 \\
 \langle 3d_z | \hat{\theta}_{xx} | 3s \rangle & = \left(\frac{64}{10125} \right)^{1/2} (\alpha/\beta)^{7/2} \left\{ Y_0 + \frac{5}{7} (2 \cos \theta - \sin^2 \theta) Y_2 + \frac{9}{28} (35 \cos^4 \theta - 30 \cos^2 \theta + 3) Y_4 \right\} / \beta^2 \\
 \langle 3d_{xx} | \hat{\theta}_{xx} | 3s \rangle & = - \left(\frac{16}{6615} \right)^{1/2} (\alpha/\beta)^{7/2} [2 \sin \theta \cos \theta \cos \phi Y_2 + 3 \sin \theta (7 \cos^3 \theta - 3 \cos \theta) \cos \phi Y_4] / \beta^2 \\
 \langle 2p_x | \hat{\theta}_{xx} | 3p_x \rangle & = \left(\frac{128}{3375} \right)^{1/2} (\alpha/\beta)^{5/2} \left\{ 2I_0 + \frac{55}{14} (2 \cos^2 \theta - \sin^2 \theta) I_2 + \frac{9}{14} (35 \cos^4 \theta - 30 \cos^2 \theta + 3) I_4 \right. \\
 & \quad \left. - 2a [1 + (2 \cos^2 \theta - \sin^2 \theta)] H_1 - \frac{9}{14} [3(2 \cos^2 \theta - \sin^2 \theta) + (35 \cos^4 \theta - 30 \cos^2 \theta + 3)] a H_3 \right\} / \beta^2 \\
 \langle 3p_x | \hat{\theta}_{xx} | 3p_x \rangle & = \left(\frac{8}{225} \right) (\alpha/\beta)^{7/2} \left\{ [2E_0 + \frac{55}{14} (2 \cos^2 \theta - \sin^2 \theta) E_2 + \frac{9}{14} (35 \cos^4 \theta - 30 \cos^2 \theta + 3) E_4 \right. \\
 & \quad \left. - 2 [1 + (2 \cos^2 \theta - \sin^2 \theta)] a I_1 - \frac{9}{14} [3(2 \cos^2 \theta - \sin^2 \theta) + (35 \cos^4 \theta - 30 \cos^2 \theta + 3)] a I_3 \right\} / \beta^2 \\
 \langle 3p_x | \hat{\theta}_{xx} | 3p_x \rangle & = - \left(\frac{8}{75} \right) (\alpha/\beta)^{7/2} \left\{ \frac{11}{7} \cos \theta \sin \theta \cos \phi E_2 + \frac{15}{14} \sin \theta (7 \cos^3 \theta - 3 \cos \theta) \cos \phi E_4 + \cos \theta \sin \theta \cos \phi a I_1 \right. \\
 & \quad \left. - \frac{3}{2} (4 \cos^3 \theta \sin \theta - \cos \theta \sin^3 \theta) \cos \phi a I_3 \right\} / \beta^2 \\
 \langle 3d_x | \hat{\theta}_{xx} | 3p_x \rangle & = \left(\frac{64}{3375} \right)^{1/2} (\alpha/\beta)^{7/2} \left\{ \frac{11}{7} \cos \theta E_1 + (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) E_3 + \frac{5}{28} (63 \cos^5 \theta - 70 \cos^3 \theta + 15 \cos \theta) E_5 \right. \\
 & \quad \left. - \cos \theta a I_0 - \frac{5}{7} (2 \cos^2 \theta - \sin^2 \theta) \cos \theta a I_2 - \frac{9}{28} (35 \cos^4 \theta - 30 \cos^2 \theta + 3) \cos \theta a I_4 \right\} / \beta^2
 \end{aligned}$$

$$\begin{aligned}
\langle 3d_{xz} | \hat{\theta}_{zz} | 3p_x \rangle &= - \left(\frac{64}{10125} \right)^{1/2} (\alpha/\beta)^{7/2} \left\{ \frac{3}{7} \sin \theta \cos \phi E_1 + \frac{12}{5} (4 \cos^2 \theta \sin \theta - \sin^3 \theta) \cos \phi E_3 \right. \\
&\quad + \frac{15}{14} \sin \theta (21 \cos^4 \theta - 14 \cos^2 \theta + 1) \cos \phi E_5 - \frac{15}{7} \cos^2 \theta \sin \theta \cos \phi a I_2 \\
&\quad \left. - \frac{45}{14} (4 \cos^3 \theta \sin \theta - \cos \theta \sin^3 \theta) \cos \phi a I_4 \right\} / \beta^2 \\
\langle 2p_x | \hat{\theta}_{zz} | 3p_x \rangle &= \left(\frac{32}{375} \right)^{1/2} (\alpha/\beta)^{5/2} \left\{ I_0 - \frac{5}{14} (5 (2 \cos^2 \theta - \sin^2 \theta) - 2 \sin^2 \theta \cos 2 \phi) I_2 + \frac{3}{28} (3 (35 \cos^4 \theta - 30 \cos^2 \theta + 3) \right. \\
&\quad - 5 \sin^2 \theta (7 \cos^3 \theta - 3 \cos \theta) \cos 2 \phi) I_4 - \left(1 - \frac{1}{2} (2 \cos^2 \theta - \sin^2 \theta) - \frac{5}{7} \sin^2 \theta \cos 2 \phi \right) a H_1 \\
&\quad \left. + \frac{3}{28} (12 (2 \cos^2 \theta - \sin^2 \theta) - 3 (35 \cos^4 \theta - 30 \cos^2 \theta + 3) + 5 \sin^2 \theta (7 \cos^3 \theta - 3 \cos \theta) \cos 2 \phi) a H_3 \right\} / \beta^2 \\
\langle 3p_x | \hat{\theta}_{zz} | 3p_x \rangle &= \left(\frac{8}{75} \right) (\alpha/\beta)^{7/2} \left\{ E_0 - \frac{5}{14} (5 (2 \cos^2 \theta - \sin^2 \theta) - 2 \sin^2 \theta \cos 2 \phi) E_2 + \frac{3}{28} (3 (35 \cos^4 \theta - 30 \cos^2 \theta + 3) \right. \\
&\quad - 5 \sin^2 \theta (7 \cos^3 \theta - 3 \cos \theta) \cos 2 \phi) E_4 - \left(1 - \frac{1}{2} (2 \cos^2 \theta - \sin^2 \theta) - \frac{5}{7} \sin^2 \theta \cos 2 \phi \right) a I_1 \\
&\quad \left. + \frac{3}{28} (12 (2 \cos^2 \theta - \sin^2 \theta) - 3 (35 \cos^4 \theta - 30 \cos^2 \theta + 3) + 5 \sin^2 \theta (7 \cos^3 \theta - 3 \cos \theta) \cos 2 \phi) a I_3 \right\} / \beta^2 \\
\langle 3d_{xz} | \hat{\theta}_{zz} | 3p_x \rangle &= \left(\frac{64}{10125} \right)^{1/2} (\alpha/\beta)^{7/2} \left\{ \frac{3}{7} \cos \theta E_1 + \frac{4}{5} (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) E_3 - \frac{5}{28} (63 \cos^5 \theta - 70 \cos^3 \theta + 15 \cos \theta) \right. \\
&\quad - 21 \sin^2 \theta (3 \cos^3 \theta - \cos \theta) \cos 2 \phi) E_5 - \frac{3}{7} (2 \cos \theta - (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) + 5 \cos \theta \sin^2 \theta \cos 2 \phi) a I_2 \\
&\quad \left. - \left[\frac{5}{7} (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) + \frac{15}{4} \sin^2 \theta (3 \cos^3 \theta - 2 \cos \theta \cos 2 \phi) a I_4 \right] \right\} / \beta^2 \\
\langle 2p_x | \hat{\theta}_{zz} | 3p_x \rangle &= \left(\frac{32}{375} \right)^{1/2} (\alpha/\beta)^{5/2} \left\{ I_0 - \frac{5}{14} (5 (2 \cos^2 \theta - \sin^2 \theta) + 2 \sin^2 \theta \cos 2 \phi) I_2 + \frac{3}{28} (3 (35 \cos^4 \theta - 30 \cos^2 \theta + 3) \right. \\
&\quad + 5 \sin^2 \theta (7 \cos^3 \theta - 3 \cos \theta) \cos 2 \phi) I_4 - \left(1 - \frac{1}{2} (2 \cos^2 \theta - \sin^2 \theta) - \frac{5}{7} \sin^2 \theta \cos 2 \phi \right) a H_1 \\
&\quad \left. + \frac{3}{28} (12 (2 \cos^2 \theta - \sin^2 \theta) - 3 (35 \cos^4 \theta - 30 \cos^2 \theta + 3) - 5 \sin^2 \theta (7 \cos^3 \theta - 3 \cos \theta) \cos 2 \phi) a H_3 \right\} / \beta^2 \\
\langle 3p_x | \hat{\theta}_{zz} | 3p_x \rangle &= \left(\frac{8}{75} \right) (\alpha/\beta)^{7/2} \left\{ E_0 - \frac{5}{14} (5 (2 \cos^2 \theta - \sin^2 \theta) + 2 \sin^2 \theta \cos 2 \phi) E_2 + \frac{3}{28} (3 (35 \cos^4 \theta - 30 \cos^2 \theta + 3) \right. \\
&\quad + 5 \sin^2 \theta (7 \cos^3 \theta - 3 \cos \theta) \cos 2 \phi) E_4 - \left(1 - \frac{1}{2} (2 \cos^2 \theta - \sin^2 \theta) - \frac{5}{7} \sin^2 \theta \cos 2 \phi \right) a I_1 \\
&\quad \left. + \frac{3}{28} (12 (2 \cos^2 \theta - \sin^2 \theta) - 3 (35 \cos^4 \theta - 30 \cos^2 \theta + 3) - 5 \sin^2 \theta (7 \cos^3 \theta - 3 \cos \theta) \cos 2 \phi) a I_3 \right\} / \beta^2 \\
\langle 3d_{yz} | \hat{\theta}_{zz} | 3p_x \rangle &= \left(\frac{64}{10125} \right)^{1/2} (\alpha/\beta)^{7/2} \left\{ \frac{3}{7} \cos \theta E_1 + \frac{4}{5} (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) E_3 - \frac{5}{28} (63 \cos^5 \theta - 70 \cos^3 \theta + 15 \cos \theta) \right. \\
&\quad + 21 \sin^2 \theta (3 \cos^3 \theta - \cos \theta) \cos 2 \phi) E_5 - \frac{3}{7} (2 \cos \theta - (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) + 5 \cos \theta \sin^2 \theta \cos 2 \phi) \\
&\quad \left. - 5 \cos \theta \sin^2 \theta \cos 2 \phi) a I_2 - 5 \left[\frac{1}{7} (2 \cos^3 \theta - 3 \cos \theta \sin^2 \theta) - \frac{3}{4} \sin^2 \theta (3 \cos^3 \theta - \cos \theta) \cos 2 \phi \right] a I_4 \right\} / \beta^2 \\
\langle 1s | \hat{\theta}_{\alpha\alpha} | 1s \rangle &= 2 \sqrt{6} (\alpha/\beta)^{3/2} \sin^2 \theta \cos 2 \phi V_2 / \beta^2 \\
\langle 2s | \hat{\theta}_{\alpha\alpha} | 2s \rangle &= \left(\frac{8}{3} \right) (\alpha/\beta)^{5/2} \sin^2 \theta \cos 2 \phi H_2 / \beta^2 \\
\langle 2s | \hat{\theta}_{\alpha\alpha} | 1s \rangle &= 2 \sqrt{2} (\alpha/\beta)^{5/2} \sin^2 \theta \cos 2 \phi W_2 / \beta^2 \\
\langle 2p_x | \hat{\theta}_{\alpha\alpha} | 1s \rangle &= 2 \sqrt{6} (\alpha/\beta)^{5/2} \cos \theta \sin^2 \theta \cos 2 \phi W_3 / \beta^2 \\
\langle 2p_x | \hat{\theta}_{\alpha\alpha} | 2s \rangle &= 2 \sqrt{2} (\alpha/\beta)^{5/2} \cos \theta \sin^2 \theta \cos 2 \phi H_3 / \beta^2 \\
\langle 2p_x | \hat{\theta}_{\alpha\alpha} | 1s \rangle &= \left(\frac{24}{25} \right)^{1/2} (\alpha/\beta)^{5/2} \left\{ 2 \sin \theta \cos \phi W_1 + \frac{1}{2} [5 \sin^2 \theta \cos 3 \phi - (4 \cos^2 \theta \sin \theta - \sin^3 \theta) \cos \phi] W_3 \right\} / \beta^2 \\
\langle 2p_x | \hat{\theta}_{\alpha\alpha} | 2s \rangle &= \left(\frac{8}{25} \right) (\alpha/\beta)^{5/2} \left\{ 2 \sin \theta \cos \phi H_1 + \frac{1}{2} [5 \sin^2 \theta \cos 3 \phi - (4 \cos^2 \theta \sin \theta - \sin^3 \theta) \cos \phi] H_3 \right\} / \beta^2 \\
\langle 2s | \hat{\theta}_{\alpha\alpha} | 2p_x \rangle &= 2 \sqrt{2} (\alpha/\beta)^{5/2} \{ \cos \theta \sin^2 \theta \cos 2 \phi (S_3 - a W_3) \} / \beta^2
\end{aligned}$$

$$\begin{aligned} \langle 3s | \hat{\theta}_{aa} | 2p_x \rangle &= \left(\frac{16}{15} \right)^{1/2} (\alpha/\beta)^{7/2} \{ \cos \theta \sin^2 \theta \cos 2\phi (X_3 - aS_3) \} / \beta^2 \\ \langle 2p_x | \hat{\theta}_{aa} | 2p_x \rangle &= \left(\frac{24}{49} \right)^{1/2} (\alpha/\beta)^{5/2} \{ \sin^2 \theta \cos 2\phi S_2 - \sin^2 \theta (7 \cos^2 \theta - 1) \cos 2\phi S_4 - \sqrt{7} \cos \theta \sin^2 \theta \cos 2\phi aW_3 \} / \beta^2 \\ \langle 2p_x | \hat{\theta}_{aa} | 2p_x \rangle &= \left(\frac{24}{49} \right)^{1/2} (\alpha/\beta)^{7/2} \{ 2 \cos \theta \sin \theta \cos \phi S_2 + \frac{1}{2} (7 \sin^2 \theta \cos \theta \cos 3\phi - \sin \theta (7 \cos^3 \theta - 3 \cos \theta) \cos \phi) S_4 \\ &\quad - \frac{14}{5} \cos \theta \sin \theta \cos \phi aW_1 - \frac{1}{2} (7 \sin^3 \theta \cos \theta \cos 3\phi - \frac{8}{5} \cos \theta \sin \theta \cos \phi - \sin \theta (7 \cos^3 \theta - 3 \cos \theta) \\ &\quad \cdot \cos \phi aW_3) \} / \beta^2 \\ \langle 3s | \hat{\theta}_{aa} | 3p_x \rangle &= \left(\frac{32}{225} \right)^{1/2} (\alpha/\beta)^{7/2} \{ \cos \theta \sin^2 \theta \cos 2\phi (E_3 - aI_3) \} / \beta^2 \\ \langle 2p_x | \hat{\theta}_{aa} | 3p_x \rangle &= \left(\frac{16}{245} \right)^{1/2} (\alpha/\beta)^{5/2} \{ \sin^2 \theta \cos 2\phi I_2 + \sin^2 \theta (7 \cos^2 \theta - 1) \cos 2\phi I_4 - \sqrt{7} \cos \theta \sin^2 \theta \cos 2\phi aH_3 \} / \beta^2 \\ \langle 3p_x | \hat{\theta}_{aa} | 3p_x \rangle &= \left(\frac{32}{3675} \right)^{1/2} (\alpha/\beta)^{7/2} \{ \sin^2 \theta \cos 2\phi E_2 + \sin^2 \theta (7 \cos^2 \theta - 1) \cos 2\phi E_4 - \sqrt{7} \cos \theta \sin^2 \theta \cos 2\phi aI_3 \} / \beta^2 \\ \langle 3p_x | \hat{\theta}_{aa} | 3p_x \rangle &= \left(\frac{32}{3675} \right)^{1/2} (\alpha/\beta)^{7/2} \{ 2 \cos \theta \sin \theta \cos \phi E_2 + \frac{1}{7} (7 \sin^2 \theta \cos \theta \cos 3\phi - \sin \theta (7 \cos^3 \theta - 3 \cos \theta) \cos \phi) E_4 \\ &\quad - \frac{14}{5} \cos \theta \sin \theta \cos \phi aI_1 - \frac{1}{2} (7 \sin^3 \theta \cos \theta \cos 3\phi - \frac{8}{5} \cos \theta \sin \theta \cos \phi \\ &\quad - \sin \theta (7 \cos^3 \theta - 3 \cos \theta) \cos \phi) aI_3 \} / \beta^2 \\ \langle 2p_x | \hat{\theta}_{aa} | 2p_x \rangle &= \left(\frac{8}{25} \right)^{1/2} (\alpha/\beta)^{5/2} \{ 2S_0 - (2(\cos^2 \theta - \sin^2 \theta) + \frac{66}{7} \sin^2 \theta \cos 2\phi) S_2 + \frac{1}{28} (3(35 \cos^4 \theta - 30 \cos^2 \theta + 3) \\ &\quad - 10 \sin^2 \theta (7 \cos^2 \theta - 1) \cos \phi) S_4 - (2 - (2 \cos^2 \theta - \sin^2 \theta) + 6 \sin^2 \theta \cos 2\phi) aW_1 \\ &\quad - \frac{1}{7} (1 - \frac{3}{4} (35 \cos^4 \theta - 30 \cos^2 \theta + 3) + 24 \sin^2 \theta \cos^2 \phi - 5 \sin^2 \theta (7 \cos^2 \theta - 1) \cos 2\phi) \} aW_3 / \beta^2 \\ \langle 2p_x | \hat{\theta}_{aa} | 3p_x \rangle &= \left(\frac{16}{1125} \right)^{1/2} (\alpha/\beta)^{5/2} \{ 2I_0 - (2(2 \cos^2 \theta - \sin^2 \theta) + \frac{66}{7} \sin^2 \theta \cos 2\phi) I_2 + \frac{1}{28} (3(35 \cos^4 \theta - 30 \cos^2 \theta + 3) \\ &\quad - 10 \sin^2 \theta (7 \cos^2 \theta - 1) \cos 2\phi) I_4 - (2 - (2 \cos^2 \theta - \sin^2 \theta) + 6 \sin^2 \theta \cos 2\phi) aH_1 \\ &\quad - \frac{1}{7} (1 - \frac{3}{4} (35 \cos^4 \theta - 30 \cos^2 \theta + 3) + 24 \sin^2 \theta \cos 2\phi - 5 \sin^2 \theta (7 \cos^2 \theta - 1) \cos 2\phi) aH_3 \} / \beta^2 \\ \langle 3p_x | \hat{\theta}_{aa} | 3p_x \rangle &= \left(\frac{32}{16875} \right)^{1/2} (\alpha/\beta)^{7/2} \{ 2E_0 - (2(2 \cos^2 \theta - \sin^2 \theta) + \frac{66}{7} \sin^2 \theta \cos 2\phi) E_2 + \frac{1}{28} (3(35 \cos^4 \theta - 30 \cos^2 \theta + 3) \\ &\quad - 10 \sin^2 \theta (7 \cos^2 \theta - 1) \cos 2\phi) E_4 - (2 - (2 \cos^2 \theta - \sin^2 \theta) + 6 \sin^2 \theta \cos 2\phi) aI_1 \\ &\quad - \frac{1}{7} (1 - \frac{3}{4} (35 \cos^4 \theta - 30 \cos^2 \theta + 3) + 24 \sin^2 \theta \cos 2\phi - 5 \sin^2 \theta (7 \cos^2 \theta - 1) \cos 2\phi) aI_3 \} / \beta^2 \\ \langle 2p_x | \hat{\theta}_{aa} | 2p_x \rangle &= \left(\frac{8}{25} \right)^{1/2} (\alpha/\beta)^{5/2} \{ -2S_0 + (2(2 \cos^2 \theta - \sin^2 \theta) - \frac{66}{7} \sin^2 \theta \cos 2\phi) S_2 - \frac{1}{28} (3(35 \cos^4 \theta - 30 \cos^2 \theta + 3) \\ &\quad + 10 \sin^2 \theta (7 \cos^2 \theta - 1) \cos 2\phi) S_4 + (2 - (2 \cos^2 \theta - \sin^2 \theta) - 6 \sin^2 \theta \cos 2\phi) aW_1 \\ &\quad + \frac{1}{7} (1 - \frac{3}{4} (35 \cos^4 \theta - 30 \cos^2 \theta + 3) - 24 \sin^2 \theta \cos 2\phi + 5 \sin^2 \theta (7 \cos^2 \theta - 1) \cos 2\phi) aW_3 \} / \beta^2 \\ \langle 3p_x | \hat{\theta}_{aa} | 3p_x \rangle &= \left(\frac{32}{16875} \right)^{1/2} (\alpha/\beta)^{7/2} \{ -2E_0 + (2(2 \cos^2 \theta - \sin^2 \theta) - \frac{66}{7} \sin^2 \theta \cos 2\phi) E_2 - \frac{1}{28} (3(35 \cos^4 \theta - 30 \cos^2 \theta + 3) \\ &\quad + 10 \sin^2 \theta (7 \cos^2 \theta - 1) \cos 2\phi) E_4 + (2 - (2 \cos^2 \theta - \sin^2 \theta) - 6 \sin^2 \theta \cos 2\phi) aI_1 \\ &\quad + \frac{1}{7} (1 - \frac{3}{4} (35 \cos^4 \theta - 30 \cos^2 \theta + 3) - 24 \sin^2 \theta \cos 2\phi + 5 \sin^2 \theta (7 \cos^2 \theta - 1) \cos 2\phi) aI_3 \} / \beta^2 \end{aligned}$$

where $\hat{\theta}_{aa} = \left(\frac{4\pi}{5} \right)^{1/2} r^2 [Y_{2-2}(\theta_2, \phi_2) + Y_{22}(\theta_2, \phi_2)]$

Table 2. The transformed part of the quadrupole moment matrix elements into overlap integrals for Mülliken.

$$\begin{aligned}
 \langle 1s | \hat{\theta}_{zz} &= \left(\frac{9}{2}\right)^{1/2} / \alpha^2 \langle 3d_{z^2} | \\
 \langle 2s | \hat{\theta}_{zz} &= \sqrt{21} / \alpha^2 \langle 4d_{z^2} | \\
 \langle 2p_x | \hat{\theta}_{zz} &= \frac{1}{\alpha^2} \left\{ \sqrt{21} \langle 4s | + \left(\frac{84}{5}\right)^{1/2} \langle 4f_{xz} | \right\} \\
 \langle 2p_x | \hat{\theta}_{zz} &= \frac{1}{\alpha^2} \left\{ \left(\frac{21}{5}\right)^{1/2} \langle 4p_x | - \left(\frac{36}{5}\right)^{1/2} \langle 4f_{xz} | \right\} \\
 \langle 2p_y | \hat{\theta}_{zz} &= \frac{1}{\alpha^2} \left\{ \left(\frac{21}{5}\right)^{1/2} \langle 4p_y | - \left(\frac{36}{5}\right)^{1/2} \langle 4f_{yz} | \right\} \\
 \langle 3s | \hat{\theta}_{zz} &= 3\sqrt{7} / \alpha^2 \langle 5d_{z^2} | \\
 \langle 3p_x | \hat{\theta}_{zz} &= \frac{3}{\alpha^2} \left\{ 2\left(\frac{7}{5}\right)^{1/2} \langle 5p_x | + 3\left(\frac{3}{5}\right)^{1/2} \langle 5f_{xz} | \right\} \\
 \langle 3p_x | \hat{\theta}_{zz} &= \frac{3}{\alpha^2} \left\{ -\left(\frac{7}{5}\right)^{1/2} \langle 5p_x | + 3\left(\frac{2}{5}\right)^{1/2} \langle 5f_{xz} | \right\} \\
 \langle 3p_y | \hat{\theta}_{zz} &= \frac{3}{\alpha^2} \left\{ -\left(\frac{7}{5}\right)^{1/2} \langle 5p_y | + 3\left(\frac{2}{5}\right)^{1/2} \langle 5f_{yz} | \right\} \\
 \langle 3d_{xz} | \hat{\theta}_{zz} &= \frac{1}{\alpha^2} \left\{ 3\sqrt{7} \langle 5s | + 6\left(\frac{7}{5}\right)^{1/2} \langle 5d_{z^2} | + 18\left(\frac{1}{7}\right)^{1/2} \langle 5f_{xz} | \right\} \\
 \langle 3d_{yz} | \hat{\theta}_{zz} &= \frac{1}{\alpha^2} \left\{ 3\left(\frac{5}{7}\right)^{1/2} \langle 5d_{yz} | + 3\left(\frac{30}{7}\right)^{1/2} \langle 5f_{yz} | \right\} \\
 \langle 3d_{yz} | \hat{\theta}_{zz} &= \frac{1}{\alpha^2} \left\{ 3\left(\frac{5}{7}\right)^{1/2} \langle 5d_{yz} | + 3\left(\frac{30}{7}\right)^{1/2} \langle 5f_{yz} | \right\} \\
 \langle 3d_{xy} | \hat{\theta}_{zz} &= \frac{3}{\alpha^2} \left\{ -2\left(\frac{5}{7}\right)^{1/2} \langle 5d_{xy} | + \left(\frac{30}{7}\right)^{1/2} \langle 5f_{xy} | \right\} \\
 \langle 3d_{x^2-y^2} | \hat{\theta}_{zz} &= \frac{3}{\alpha^2} \left\{ -2\left(\frac{5}{7}\right)^{1/2} \langle 5d_{x^2-y^2} | + \left(\frac{30}{7}\right)^{1/2} \langle 5f_{x^2-y^2} | \right\} \\
 \langle 1s | \hat{\theta}_{xx} &= \left(\frac{9}{2}\right)^{1/2} / \alpha^2 \langle 3d_{x^2-y^2} | \\
 \langle 2s | \hat{\theta}_{xx} &= \sqrt{21} / \alpha^2 \langle 4d_{x^2-y^2} | \\
 \langle 3s | \hat{\theta}_{xx} &= 3\sqrt{7} / \alpha^2 \langle 5d_{x^2-y^2} | \\
 \langle 2p_x | \hat{\theta}_{xx} &= \sqrt{9} / \alpha^2 \langle 4f_{x(x^2-y^2)} | \\
 \langle 2p_x | \hat{\theta}_{xx} &= 3\sqrt{3} / \alpha^2 \langle 4f_{x(x^2-y^2)} | + 3\left(\frac{18}{5}\right)^{1/2} / \alpha^2 \langle 4p_x | - \left(\frac{9}{5}\right)^{1/2} / \alpha^2 \langle 4f_{xz} | \\
 \langle 2p_y | \hat{\theta}_{xx} &= 3\sqrt{3} / \alpha^2 \langle 4f_{y(x^2-y^2)} | + 3\left(\frac{18}{5}\right)^{1/2} / \alpha^2 \langle 4p_y | - \left(\frac{9}{5}\right)^{1/2} / \alpha^2 \langle 4f_{yz} | \\
 \langle 3p_x | \hat{\theta}_{xx} &= 3\sqrt{3} / \alpha^2 \langle 5f_{x(x^2-y^2)} | \\
 \langle 3p_x | \hat{\theta}_{xx} &= 9 / \alpha^2 \langle 5f_{x(x^2-y^2)} | + 3\left(\frac{42}{5}\right)^{1/2} \langle 5p_x | - 3\left(\frac{3}{5}\right)^{1/2} \langle 5f_{xz} | \\
 \langle 3p_y | \hat{\theta}_{xx} &= 9 / \alpha^2 \langle 5f_{y(x^2-y^2)} | + 3\left(\frac{42}{5}\right)^{1/2} \langle 5p_y | - 3\left(\frac{3}{5}\right)^{1/2} \langle 5f_{yz} |
 \end{aligned}$$

$$\text{where } \hat{\theta}_{xx} = \left(\frac{4\pi}{5}\right)^{1/2} [Y_{2-2}(\theta, \phi) + Y_{22}(\theta, \phi)]$$

Slater 원자궤도함수로 치환하던 사중극자모멘트 행렬요소에 대한 다음과 같은 일반식을 얻을 수 있다.

$$\begin{aligned}
 \langle \phi_A | \frac{1}{2} (3x^2 - r^2) | \phi_B \rangle = \\
 NC \langle r^{l+2} \exp(-\alpha r) Y_{lm}(\theta, \phi) Y_{20}(\theta, \phi) | \phi_B \rangle \quad (30)
 \end{aligned}$$

$$\begin{aligned}
 \langle \phi_A | \frac{1}{2} (3x^2 - r) | \phi_B \rangle = \\
 -\frac{1}{2} NC \langle r^{l+2} \exp(-\alpha r) Y_{lm}(\theta, \phi) Y_{20}(\theta, \phi) | \phi_B \rangle \\
 + NC \{ \langle r^{l+2} \exp(-\alpha r) Y_{lm}(\theta, \phi) Y_{2-2}(\theta, \phi) | \phi_B \rangle \\
 + \langle r^{l+2} \exp(-\alpha r) Y_{lm}(\theta, \phi) Y_{22}(\theta, \phi) | \phi_B \rangle \} \quad (31)
 \end{aligned}$$

$$\begin{aligned}
 \langle \phi_A | \frac{1}{2} (3y^2 - r^2) | \phi_B \rangle = \\
 -\frac{1}{2} NC \langle r^{l+2} \exp(-\alpha r) Y_{lm}(\theta, \phi) Y_{20}(\theta, \phi) | \phi_B \rangle \\
 - NC \{ \langle r^{l+2} \exp(-\alpha r) Y_{lm}(\theta, \phi) Y_{2-2}(\theta, \phi) | \phi_B \rangle \\
 + \langle r^{l+2} \exp(-\alpha r) Y_{lm}(\theta, \phi) Y_{22}(\theta, \phi) | \phi_B \rangle \} \quad (32)
 \end{aligned}$$

방정식 (26), (27) 및 (28)의 overlap integral을 일반식으로 바꾸면 다음이 된다.²⁷

$$\begin{aligned}
 \langle r^{l+2} \exp(-\alpha r) Y_{lm}(\theta, \phi) Y_{2p}(\theta, \phi) | \phi_B \rangle \\
 = \sum_{l'=l-2}^{l+2} \sum_{m'=-m}^m \left[\frac{(2l+1)5(2l'+1)}{4\pi} \right]^{1/2} \\
 (-1)^m \begin{pmatrix} l & 2 & l' \\ -m & pm' & 0 \end{pmatrix} \begin{pmatrix} l & 2 & l' \\ 0 & 0 & 0 \end{pmatrix} \\
 \langle r^{l+2} \exp(-\alpha r) Y_{l'm'}(\theta, \phi) | \phi_B \rangle \quad (33)
 \end{aligned}$$

여기에서 $p=0$ 또는 ± 2 임.

주어진 l, m, l', m' 및 p 에 대응하는 3- j symbols의 값을 방정식 (29)에 대입하여 얻은 overlap integral의 일반식을 방정식 (26)~(28)에 치환하여 주면 x, y 및 z 축(방향)의 주 사중극자모멘트행렬요소에 대한 전환 overlap integral을 얻을 수 있다. 사중극자모멘트행렬요소를 overlap integral로 전환시킨 부분(transformed part of the quadrupole moment matrix element), $\langle \phi_A | \theta_{\alpha\alpha} | \phi_B \rangle$ 을 Table 2에 나타내었다.

3. 결과 및 고찰

Table 1 및 2에 기술한 기본식을 사용하여 가상적인 NO 분자의 Slater 원자궤도함수에 대하여 사중극자모멘트행렬요소를 계산하여 Table 3에

Table 3. The calculated values of the quadrupole moment matrix elements for a hypothetical No molecule whose Slater constants are 1.95 (N) and 2.275 (O), respectively ($r=1.5\text{\AA}$).

Quadrupole moment matrix	Expansion method	Transformed overlap integral	Mulliken
$\langle 1s \hat{\theta}_{zz} 1s \rangle$	0.025197	$\left(\frac{9}{2}\right)^{1/2} / a^2 \langle 3d_{z^2} 1s \rangle$	0.0251934
$\langle 2s \hat{\theta}_{zz} 1s \rangle$	0.079984	$(21)^{1/2} / a^2 \langle 4d_{z^2} 1s \rangle$	0.079398
$\langle 1s \hat{\theta}_{zz} 2p_z \rangle$	-0.025422	$\left(\frac{9}{2}\right)^{1/2} / a^2 \langle 3d_z^2 2p_z \rangle$	-0.025452
$\langle 1s \hat{\theta}_{zz} 2s \rangle$	0.029510	$\left(\frac{9}{2}\right)^{1/2} \langle 3d_z^2 2s \rangle$	0.029568
$\langle 2s \hat{\theta}_{zz} 2s \rangle$	0.090842	$(21)^{1/2} / a^2 \langle 4d_z^2 2s \rangle$	0.090995
$\langle 2s \hat{\theta}_{zz} 2p_z \rangle$	-0.0561235	$(21)^{1/2} / a^2 \langle 4d_z^2 2p_z \rangle$	-0.056590

나타내었다. Table 3에 나타난것 처럼 사중극자모멘트 연산자를 spherical harmonics 꼴로 바꾼 다음 spherical harmonics의 전개방법에 의하여 계산한 사중극자모멘트행렬요소의 값이 사중극자모멘트행렬요소를 Mulliken의 overlap integral로 변환시킨 사중극자모멘트행렬요소의 전환 overlap integral의 값과 소수점이하 네째 자리까지 일치하였다.

사중극자모멘트연산자를 spherical harmonics 꼴로 바꾼 다음 연산자법에 의하여 분자의 사중극자모멘트는 Table 1 및 2에 주어진 기본식을 사용하여 각 원자궤도함수에 대한 사중극자모멘트행렬요소를 계산하고 분궤도함수의 basis sets에 대한 사중극자모멘트행렬요소의 값을 방정식 (18)~(21)에 넣어주므로써 간단히 계산할 수 있다.

이상의 연산자법은 간단한 분자의 사중극자모멘트를 계산하는데 사용되었으며¹⁸ Nesbet¹⁹의 Hartree Fock 분자궤도함수를 사용하고 본 연구의 연산자법에 의하여 바닥상태의 HCl 분자에 대한 사중극자모멘트를 계산하였을때 본 연구의 방법에 의하여 얻은 사중극자모멘트의 값이 3.457×10^{-26} esu cm² 전자전하밀도의 계산으로부터 얻은 똑같은 분자궤도함수에 대한 Nesbet의

값 3.46×10^{-26} esu cm²과 일치하였다. 이상의 연산자법에 의한 사중극자모멘트행렬요소의 계산은 전자전하밀도의 분포로부터 또는 Bloor 및 Maksic¹²의 방법에 의한 계산과 달리 많은 계산시간을 필요로 하지 않으며 소형 전자계산기를 사용하여 계산할 수 있다는 잇점이 있다.

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