# Temperature Stable, Low Ringing Noise Memory Cores

Ho-Bin Im\*

Ampex Memory Products Division El Segundo, California

(Received March 25, 1978)

# 온도에 안정하고 잡음이 적은 메모리코어에 대한 연구

임 호 빈한국 과학원 재료 공학과

(1978년 3월 25일 접수)

### 초 록

Zn<sub>0.105</sub> Co<sub>0.025</sub> Li<sub>0.435-1/2r</sub> Ni<sub>x</sub> Fe<sub>2.435-1/2r-y</sub> Mn<sub>y</sub> O<sub>4</sub> 조성의 메모리코어 특성과 Nb<sub>2</sub>O<sub>5</sub> 및 V<sub>2</sub>O<sub>5</sub>의 소량 철가가 square-loop 성질에 주는 영향을 연구하였다. 위의 조성에서 닉켈의 양 x는 0에서 0.15까지, 그리고 망간의 양 y는 0.05에서 0.25까지 변화시켰다. Nb<sub>2</sub>O<sub>5</sub>의 양은 각자 위의 화학식에 대하여 0.005에서 0.015까지 변화시켰다.

실험결과에 의하면 Mn<sup>+3</sup>를 octahedral 자리에 첨가하였을 때에는 잡음이 감소되었고 메모리코어의 spuareness 와 보자련의 온도계수가 중가하였다. 닉켈을 첨가하였을 때에는 메모리코어의 squareness 와 잡음이 증가하였다.

 $Nb_2O_5$  돌 소량 첨가하였을 때에는 square-loop성질이 개선되었음에 비하여  $V_2O_5$ 를 소량 첨가하였을 대에는 square-loop성질이 나빠졌다.

### Introduction

The ferrite cores widely used as information storage elements in high-speed computers must exhibit rectangular magnetic hysteresis loops. "Square-loop cores" today are fabricated from materials chosen from several ferrite solid-solution systems which include coppermanganese ferrites, magnesium-manganess ferrites, lithium manganese ferrites, and lithium nickel ferrites. If the cores are to be used as memory devices which are subjected to changes in temperature, the temperature coefficients of the coercive force force and "knee-current" are important properties. In order to make a memory

\*Present Address: The Korea Advanced Institute of Science Seoul, Korea : device operate satisfactorilly over a wide temperature range, changes in "knee-current" must be compensated by changing the amplitude of current pulses used to switch the cores. Therefore, cores with small temperature coefficients lead to improved performance and simpler memory design. The temperature coefficient of the "knee current", however, is increased by substitution of zinc and by most of the other elements which are introduced for various purposes<sup>1)2)</sup>.

Small temperature coefficient have been found in nickel-manganess-ferrous ferrite system<sup>3)4)</sup> and cobalt substituted lithium ferrite system<sup>5)</sup>. Memory cores made from the cobalt substituted lithium ferrite exhibit almost temperature independent "knee-current" in the temperature range from -50°C to 100°C, but also exhibit

larger magnetostrictive ringing voltages as well as larger disturbed noise. This ringing voltage is a source of noise in a high-speed core memory and is undesirable in practical application of large memory systems<sup>6)</sup>.

In this work it is shown how the disturbed noise of the cobalt substituted lithium ferrite memory cores can be decreased by the substitution of very small quantities of niobium pentoxide and the magnetostrictive ringing voltages can be decreased by the substitution of manganese,

# Experimental Procedure

A number of compositions in the system  $Z_{00,105}$   $Co_{0,025}$   $Li_{0.435-1/2x}$   $Ni_x$   $Fe_{2.435-\frac{1}{2}x-y}$   $Mn_y$   $Mn_y$   $O_4$  were studied. Zinc and cobalt were included in the formulation to obtain coercive force low enough for 18 mil (0.46mm) cores and to reduce temperature coefficient of  $I_k$  (knee current). Compositions with various content of vandium pentoxide (Fisher certified reagent) or biobium pentoxide (Alfa spec. grade) were also made. Each powder was prepared by mixing lithium carbonate (J. T. Baker), cobalt carbonate (J. T. Baker), manganese carbonate (J. T. Baker), nickel oxide (J. T. Baker), and iron oxide (Columbian Carbon Co.). This mixture was

treated by calcining, mixing again with ball mill, reacting at high temperature and ball mill grinding to produce a fine powder. Cores were prepared from this powder by tape method: the powder was mixed with a large quantity of a suitable binder and solvent by ball milling, coated on base film, dried and peeled off from the base film, and calendered into a strip of the desired thickness from which cores were cut out with the aid of a punch press. The cores sintered in a tube furnace in air atmosphere. The sintering temperature and the soak time were adjusted for each composition to obtain cores with optimum magnetic properties. For several batches, X-ray powder diffraction pattern were obtained and it showed to be a single spinel phase. The cores after sintering were, in size, approximately 0.46mm outside diameter, 0.28mm inside diameter and 0.11mm thick.

Measurements of memory-core characteristics were performed with a Computer Test Corporation 1700 core tester using a standard  $dV_1$  program ( $dV_1$  is the disturbed voltage output signal). (The definitions of symbols are given below Table I). The ringing noises per one hundred cores excited by nonswitching currents with amplitude of 800ma, risetime ( $t_R$ ), and fall time

Table 1 Memory-Core Characteristics of Li<sub>0.435-x/2</sub> Ni<sub>x</sub> Zn<sub>0.105</sub> Co<sub>0.025</sub> Fe<sub>2.435-x/2-y</sub> Mn<sup>9+</sup>, O<sub>4</sub>

#	x (Ni)	(Mn <sup>3+</sup> )	$dV_1 \pmod{mv}$	dV <sub>z</sub> (mv)	t <sub>s</sub> (nsec)	I, (ma)	C <sub>k</sub> (ma -25°C to 25°C	1/°C) 25°C to 25°C	$V_R+ \  m (mv)$	gain (mv/ma)
1	0.10	0.05	28	12	175	460	0.42	-0.20	5.0	. 24
2	0.10	0.10	46	8.3	195	470	0.0	-0.55	2.5	. 21
3	0.10	0.15	45	7.1	215	476	0.0	-0.64	1.5	. 21
4	0. 10	0.2	44	6.0	222	470	0.0	-0.86	0.5	. 21
5	0.10	0. 25	37	8.7	202	474	0.64	-0.52	0.0	. 22
6	0	0.15	36	9.0	195	474	0.50	-0.34	0.5	. 22
7	0.05	0.15	43	7.6	205	475	0.40	-0.36	1.0	. 21
8	0.10	0.15	54	7.1	215	475	0	-0.64	1.5	. 21
9	0. 15	0.15	44	6.8	213	480	0	-0.68	2.0	. 21
10*	0	0.12	47	4.2	233	495	0.40	-0.52	0.8	. 21
11*>	0	0.12	27	7.0	215	455	_	· -		

 $I_f = 720 \text{mA}$ ,  $I_b = 450 \text{mA}$ ,  $t_R = t_f = 50 \text{nsec}$ ,  $t_d = 300 \text{nsec}$ 

<sup>+:</sup> ringing voltage per one hundred cores

<sup>\*\*:</sup> with addition of 0.010 formula unit of V2O5

 $I_p$ : partial read or write current

 $dV_1$ : disturbed one lotvage ouptut

 $t_s$ : switching time of  $dV_1$ 

<sup>\*:</sup> with addition of 0.010 formula unit of Nb2O5

 $I_f$ : full read or write current

 $I_k$ : knee current

 $dV_z$ : disturbed zero voltage output

Ck: temperature coefficient of knee current

 $(t_f)$  equal to 50 nsec, and pulse width  $(t_d)$  adjusted to obtain maximum ringing noise were measured.

The microstructures were examined with a scanning electron microscope.

### Result

Memory-core-characteristics of compositions given by  $\text{Li}_{0.435-x/2} \text{ Ni}_x \text{ Zn}_{0.105} \text{ Co}_{0.025} \text{ Fe}_{2.535-x/2-y} \text{ Mn}_y \text{ O}_4$  are listed in Table 1. Samples here were sintered at 1038° C with varying soak time to be tested under the same drive-current conditions. The disturbed noise  $(dV_*)$ decreases with increasing manganese content. composition with Mn equal to 0.20 gives the greatest value of the signal to noise ratio dV1/dV2, which is a measure of the squareness of a core under the test condition. A further increase of manganese content causes a decrease of squareness and the sample with manganese equal to 0.25 shows marginal squareness for memory-core operation. The temperature coefficient of knee current  $C_{i}$ , however, increases with increasing manganese content. The disturbed noise  $dV_z$  decreases with increasing nickel content, and composition with Ni equal to 0.15 gives the best squareness. The ringing noise  $(V_R)$ , on the other hand, decreases sharply with increasing manganese content and increases with increasing nickel content. It can be seen here that material without nickel (composition #6) gives lower ringing noise but also give low value of signal to noise ratio.

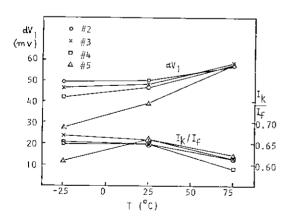


Figure 1 Memory core characteristics as a function of temperature for various manganes content.  $I_f$ =800mA,  $t_R$ = $t_f$ =50nsec,  $t_d$ =300nsec.

 $dV_{\rm I}/dV_{\rm z}$ . However, addition of small quantity of

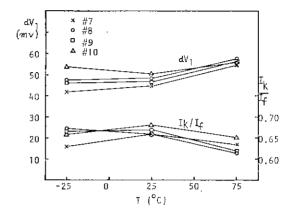


Figure 2 Memory core characteristics as a function of temperature for various nickel content.  $I_f = 800 \text{mA}, t_R = t_f = 50 \text{nsec}, t_d = 300 \text{nsec}.$ 

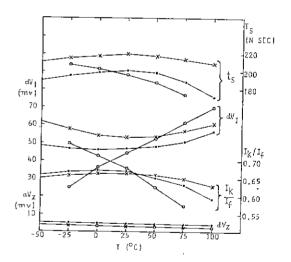


Figure 3 Memory core characteristics as a function of temperature for Li<sub>0.40</sub> Zn<sub>0.05</sub> Mn<sup>2+</sup><sub>0.07</sub> Ni<sub>0.08</sub> Mn<sup>3+</sup><sub>0.30</sub> Fe<sub>2.10</sub> O<sub>4</sub> Li<sub>0.385</sub> Zn<sub>0.105</sub> Ni<sub>0.10</sub> Co<sub>0.025</sub> Mn<sup>3+</sup><sub>0.15</sub> Fe<sub>2.235</sub> O<sub>4</sub> Li<sub>0.43</sub> Zn<sub>0.10</sub> Co<sub>0.027</sub> Mn<sup>2+</sup><sub>0.033</sub> Nb<sub>0.01</sub> Mn<sup>3+</sup><sub>0.12</sub> Fe<sub>2.28</sub> O<sub>4</sub>  $I_f$ =750mA,  $I_p$ =375mA,  $I_R$ = $t_f$ =50nsec,  $t_d$ =300nsec.

niobium pentoxide to this type of (composition # 10) gives extremely high value of  $dV_1/dV_z$ .

The disturbed voltage output signal  $dV_1$  and the disturb ratio  $I_k/I_f$  both as a function of temperature for various manganese and nickel content are shown in Figure 1 and Figure 2 respectively, It can be seen that the temperature dependence of  $dV_1$  is rather small with the exception of sample with manganese equal to 0.25.

The temperature dependence of  $dV_1$ ,  $dV_2$ , the disturb ratio  $I_k/I_f$ , and the switching time  $(t_i)$  are shown graphically in Figure 3 for lithium-manganese ferrite which is widely used today, and cobalt substituted lithium-manganese with and without addition of  $\mathrm{Nb}_2\mathrm{O}_5$ . It is seen here that  $I_k$  for the cobalt and niobium containing material is almost temperature independent (TIN\* core). The result is a very small temperature dependence of the  $dV_1$  and switching time  $t_i$ .

A typical microstructure of cobalt substituted lithium manganese ferrite is shown in Figure 4a, and those of lithium manganese ferrite with 0.01 formula unit of  $V_5O_5$ , and  $Nb_2$   $O_5$  are shown in Figure 4b and 4c respectively.

# Discussion

The material characteristis which cause the occurance of square hysteresis loops in polycrystalline magnetic ferrites have been described by wijn et al. follows (7). The preferred direction of magnetization in individual crystallites of cubic symmetry should be in the crystal (111) direction, a condition described by a negative value of the crystal anisotropy constant  $K_1$ . The crystal anisotropy must dominate the shape and stress anisotropies. This condition will be met if the magnetostriction coefficient in the preferred direction of magnetization  $\lambda_{111}$  is very small. A low porosity in the material is also a necessary candition for the occurance of square loops. The square-loop properties observed for compositions in the system NiFe<sub>2</sub>O<sub>4</sub>-Fe<sub>3</sub>O<sub>4</sub><sup>7)</sup>, NiFe<sub>2</sub>  $O_4$ -Fe<sub>3</sub>  $O_4$ -MnFe<sub>2</sub> $O_4$ <sup>3)</sup>, NiFe<sub>2</sub> $O_4$ -Mn<sub>3</sub> $O_4$  and Li<sub>0.5</sub>Fe<sub>2.5</sub>  $O_4$ -Mn<sub>3</sub> $O_4$ 8, and  $Li_{0.41-x/2}Co_xZn_{0.12}Ni_{0.06}Fe_{2.41-x/2}O_4$ 5) have been explained on the basis of these material characteristics. The value of  $K_1$  for lithium ferrite is negative,  $-9\times10^4 {\rm erg/cm^3}$  <sup>9)</sup>, and  $\lambda_{111}$  is small, values of  $-3.8\times10^{-6}$  <sup>10)</sup> and  $+2.7\times10^{-6}$  <sup>11)</sup> have been reported. The values of  $\lambda_{111}$  for nickel ferrite has been measured as  $-21.6\times10^{-6}$  at  $20^{\circ}{\rm C}^{12)}$ . An accurately measured value of  $\lambda_{111}$  for cobalt ferrite has not been reported but it appears to be large and positive, approximately  $+130\times10^{-6}$  <sup>13)</sup>. It was reported the presence of Mn<sup>3+</sup> in octahedral site in the lithium ferrite contributes to positive  $\lambda_{111}^{9)}$ . The greatest squareness was observed when the value of  ${\rm Co}^{2+}$  is 0.010 in iithium nickel zinc ferrite<sup>5)</sup>, and when the value of Mn<sup>3+</sup> is 0.30 in lithium nickel ferrite<sup>8)</sup>.

The data in Table 1 show that in the compositions containing cobalt a smaller quantity of substituted manganese is required to produce maximum squareness, y equal to 0.20. This was, at first, a surprising because the values of  $\lambda_{111}$  for cobalt is positive and was thought to be be sufficient to make \$\lambda\_{111} \approx 0\$ when the value of cobalt equal to 0.010, and thus any addition of Mn3+ would make  $\lambda_{111} > 0$  reducing the squareness. It has been found, however, that the effects of cobalt is diluted when zinc is present5)14). Thus we may speculate that effects of cobalt is also diluted when manganese is present. This diluting effect is also manifested in the temperature dependence of dV1 as can be seen in Figure 1, i.e, the temperature dependeness of  $dV_1$  with increasing manganese content are similar to those of  $dV_1$ with decreasing cobalt content with ro manganese<sup>5)</sup>.

The decrease of the ringing noise with increasing manganese content and the increase of the ringing noise with icreasing nickel content can be explained in terms of effective magnetostriction coefficient  $\lambda_{eff}$ , i.e the substitutions of manganese decrease  $\lambda_{eff}$  and the substitution of nickel increase  $\lambda_{eff}$ .  $^{6015}$ .

The extremely high value of the signal to noise ratio observed in Nb<sub>2</sub>O<sub>5</sub> substituted material (#10) appears to be related with higher density and uniform grain size whereas very poor properties observed in V<sub>2</sub>O<sub>5</sub> substituted material is related with lower density and non-uniformity in grain size, as shown in Figure 4A, B&C.

It should be pointed be pointed out that with substitution of V<sub>2</sub>O<sub>5</sub> a reasonably high value of signal to noise ratio can be obtained for large size and low drive cores as reported by others<sup>16</sup>,17<sup>18</sup>,18<sup>19</sup>.

<sup>\*</sup>Ampex trade name for temperature independent memory core.

# Acknowledement

The author wish to thank J. Orendain and E. Schwartz for their assistance.

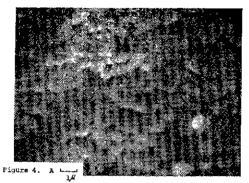






Figure 4 A typical microstructure of lithium manganese ferrite with and without "flux"

- a) no flux
- b) with 0.01 formula unit of  $V_2O_5$
- c) with 0.01 formula unit of  $Nb_2O_5$

#### Refernces

 A.P. Greifer, "Ferrite Memory Materials", IEEE. Transactions on Magnetics, vol. MAG-5, No. 4, p. 744, (1969)

- R. S. Weiss, "Square-Loop Ferrites", in Magnetic Properties of Materials, J. Smit, Ed., McGraw-Hill, New York, p. 205, (1971)
- H. B. Im and D. G. Wickham, "Square-Loop Properties of Materials in the System NiFe<sub>2</sub>O<sub>4</sub>-Fe<sub>3</sub> O<sub>4</sub>MnFe<sub>2</sub>O<sub>4</sub>", J. Appl. Phys., 35, p. 1442, (1964)
- T. Kawashima, "Temperature-Stable Low-Noise Ferrite Memory Cores", IEEE Transactions on Magnetics vol. MAG-5, p. 12, (1969)
- H. B. Im and D. G. Wickh5m, "Memory-Core Characteristics of Cobalt Substituted Lithium Ferrite", IEEE Transactions on Magnetics, vol. MAG-8, No. 4, p. 765, (1972)
- H. B. Im, "A Note on the Magnetostrictive Ringing in Core Memory Systems", IEEE Transactions on Magnetics, vol. MAG-10, No. 1, p. 93, (1974)
- H.P.J. Wijn, E.W. Gorter, C.J. Esveldt, and D. Geldermans, "Conditions for Square Hysteresis Loops in Ferrites", *Philips Tech. Rev.*, 16, p. 49, (1954)
- H.B. Im, "On the Conditions for Square Hysteresis Loops in Polycrystalline Ferrites and Their Application in Ni-Mn Ferrites and Li-Mn Ferrites", Ampex Restricted RB 65-20, (1965)
- G. F. Dionne, "Magnetic Anisotropy and Magnetostriction Constants of Substituted Lithium Ferrites at 300°K", J. Appl. Phys., 40, p. 4486, (1969)
- Yu. N. Kotyukov, Izv. Vyssh. Ucheb. Zaved. Fiz. 10, No. 8, p. 65, (1967)
- N. Tsuya and K. I. Arai, "Magnetostriction Contants of Cubic Ferrites Containing only Fe<sup>3+</sup> as Magnetic Ions", J. Appl. Phys., 42, p. 1637, (1971)
- A.B. Smith and R.V. Jones, "Magnetostriction in Nickel Ferrite and Nickel Cobalt Ferrite", J. Appl. Phys., 37, p. 1001, (1966)
- 13. R.S. Weiss, Loc. Cit., p. 216
- C. M. Van der Burgt, "Controlled Crystal Anisoropy and Controlled Temperature Dependence of the Permeability and Elasticity of Various Cobalt Subsituted Ferrites", *Philips Res. Repts.*, 12, p. 97, (1957)
- E. L. Boyd, "Magnetoelastic Resonances in Ferrite Memory Cores", J. Appl. Phys., 38, p. 2367,

Vol. 15, No. 2, 1978

(1967)

- D.G. Wickham and H.B. Im, U.S. Patent 3 300 411, (1966)
- 17. Kumada Masaharu, Japan Kokai 76 80 997, (1976)
- 18. L. M. Letyuk, "Formation of Microstructure and its Effects on the Properties of Lithium-Containing Rectangular Hysteresis-Loop Ferrites", Poroshkovaya

Metallurgia, 8, p. 59, (1975)

 L.M. Letyuk, S.S. Gorelik, E.A. Babich, and V.A. Nifontov, "Influence of Low-Melting Additives on Microsture Formation and Properties of Ferrites with Rectangular Hysteresis Loops", Izvestiva Akademii Nauk SSR, Neorganicheskie Materialy, 12, No. 11, p. 2023, (1976)