

## A Theoretical Study of Oxidation-Reduction Titration Curves\*

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### 산화·환원 적정곡선의 이론적 고찰

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### ABSTRACT

The variation of potential and completeness of reaction in an oxidation-reduction titration of  $Red_1$  ( $a Ox_1 + n_1 e \rightleftharpoons b Red_1$ ) by  $Ox_2$  ( $c Ox_2 + n_2 e \rightleftharpoons d Red_2$ ) is analyzed on the basis of general expressions. It is shown that the reaction deficiency as well as the rate of variation of the potential with titration fraction change in proportion to the  $[n_2(a-b) - n_1(c-d)]$  th power of the concentration of the reagents. In particular, at the equivalence point, the expression of the potential contains a concentration dependent term that is proportional to  $ac - bd$ . Thus, the equivalence-point potential varies with the concentration of the reagents unless  $ac = bd$  is satisfied.

It is also shown that the sharpness of the potentiometric end point is affected by exchanging titrand and titrant. The inflexion point of the potentiometric titration curve is shown to occur either prior to or after the equivalence point depending upon whether  $n_1c < n_2b$  or  $n_1c > n_2b$ , the deviation being the same order of magnitude as the relative deficiency at the equivalence point.

### INTRODUCTION

It has been pointed out that the equivalence-point potential in an oxidation-reduction titration deviates from the weighted average of the standard potentials and depends on the concentration

of the reagents, except for the cases where the coefficients in both half-reactions are homogeneous<sup>1),2)</sup>. Furthermore, some aspects of the titration curve for inhomogeneous cases have been elucidated in terms of numerical data computed for particular examples<sup>3)</sup>.

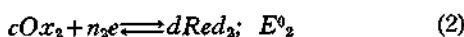
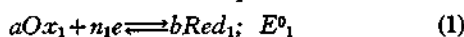
The present study is concerned with analyz-

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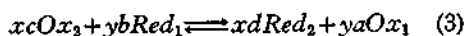
ing the variation of equivalence-point potential on a general basis and investigating the various features of the titration curve for general cases.

### BASIC EQUATIONS

Consider the titration of  $V_0$  liters of  $C_0$  molar solution of the reductant  $Red_1$  up to  $V$  liters of  $C$  molar solution of the oxidant  $Ox_2$ . Attention will not be paid to the influence of the hydrogen ion and/or other ligands that may be involved in the titration reaction, because it can be included in the standard formal potentials,  $E_0'$ s. Normally, it does not vary to an appreciable extent in the course of practical titrations. Let us assume that the potential throughout the titration is governed by the half-reactions of species 1 and 2:



Let the overall titrimetric reaction be



whence  $xn_2 = yn_1$  or  $n_1/n_2 = x/y$ .

It will be assumed that the potential of the solution is governed by the concentration expressions of the Nernst equation throughout the titration; namely, the activity coefficients of the species involved can be taken care of by the respective standard formal potentials and kept almost constant:

$$E = E_1^0 + \frac{1}{\varphi n_1} \ln \frac{[Ox_1]^a}{[Red_1]^b} \quad (4)$$

$$E = E_2^0 + \frac{1}{\varphi n_2} \ln \frac{[Ox_2]^c}{[Red_2]^d} \quad (5)$$

where  $\varphi = \frac{F}{RT} = 38.95$  volt at  $25^\circ\text{C}$ .

Letting the fraction of  $Red_1$  converted to  $Ox_1$  be  $\alpha$  at the equilibrium, the equilibrium concentrations of the chemical species involved in the titration reaction are written as the following:

$$[Red_1] = \frac{C_0 V_0 (1-\alpha)}{V_0 + V} \quad (6)$$

$$[Ox_1] = \frac{C_0 V_0 \alpha}{V_0 + V} \cdot \frac{a}{b} \quad (7)$$

$$[Red_2] = \frac{C_0 V_0 \alpha}{V_0 + V} \cdot \frac{n_1 d}{n_2 b} \quad (8)$$

$$[Ox_2] = \frac{CV - \frac{n_1 c}{n_2 b} \cdot C_0 V_0 \alpha}{V_0 + V} \quad (9)$$

Remembering that the titration fraction can be defined as

$$\phi = \frac{CVyb}{C_0 V_0 xc} = \frac{CVn_2 b}{C_0 V_0 n_1 c} \quad (10)$$

Eqs. (4) and (5) can be rewritten by use of Eqs. (6), (7), (8), (9) and (10) as

$$E = E_1^0 + \frac{1}{n_1 \varphi} \ln \frac{\alpha^a}{(1-\alpha)^b} + \frac{a}{n_1 \varphi} \ln \frac{a}{b} + \frac{a-b}{n_1 \varphi} \ln \frac{C_0 C}{C + \frac{n_2 b c_0 \alpha}{n_1 c} \phi} \quad (11)$$

and

$$E = E_2^0 + \frac{1}{n_2 \varphi} \ln \frac{(\phi - \alpha)^c}{\alpha^d} + \frac{1}{n_2 \varphi} \ln \left( \frac{n_2 b}{n_1 d} \right)^d \cdot \left( \frac{n_1 c}{n_2 b} \right)^c + \frac{c-d}{n_2 \varphi} \ln \frac{C_0 C}{C + \frac{n_2 b c_0 \alpha}{n_1 c} \phi} \quad (12)$$

Finally, multiplying Eq. (11) by  $n_1 c$  and (12) by  $n_2 b$  and adding results in

$$E = E_{eq}^0 + S + B + K(C^0, \phi, \rho) + \left[ \frac{ac-bd}{n_1 c + n_2 b} \ln \alpha + \frac{bc}{n_1 c + n_2 b} \ln \frac{\phi - \alpha}{1 - \alpha} \right] \cdot \frac{1}{\varphi} \quad (13)$$

where

$$S = \frac{1}{(n_1 c + n_2 b)} \cdot \frac{1}{\varphi} \left[ a c \ln a + (bd - bc - ac) \cdot \ln b + bc \ln c - db \ln d + b(d-c) \ln \frac{n_2}{n_1} \right] \quad (14)$$

$$B = \frac{(b-c)n_1 n_2 \Delta E_0}{(n_1 + n_2)(n_1 c + n_2 b)} \quad (\Delta E_0 = E_2^0 - E_1^0) \quad (15)$$

$$K(C_0, \phi, \rho) = \frac{ac-bd}{(n_1 c + n_2 b)} \ln f(C_0, \phi, \rho) \quad (16)$$

$$f(C_0, \phi, \rho) = \frac{C_0 V_0}{V + V_0} = \frac{C_0}{1 + \frac{n_2 b}{n_1 c} \phi \rho}; \rho = C_0 / C$$

and

$$E_{eq}^0 = \frac{n_1 E_1^0 + n_2 E_2^0}{n_1 + n_2} \quad (17)$$

It may be worthwhile to note that  $f(C_0, \phi, \rho) = C_0$  when  $V$  can be considered to be zero as in coulometric titration, whence  $\rho = 0$ . In the

following discussion, the subscripts eq, - and + will be used to designate the various regions of titration fraction; i.e., equivalence point, prior to and beyond the equivalence point, respectively. Eq. (13) is a generalized form of Eq. (15) in Bard and Simonsen's work<sup>2</sup>, which is concerned with equivalence point only. The concentration dependence of potential is represented by the terms  $K(C_0, \phi, \rho)$ ,  $\ln \alpha$  and  $\ln (\phi - \alpha)/(1 - \alpha)$ ;  $\alpha$  is a function of concentration and  $\phi$ . When  $ac = bd$  is satisfied, the effect of the former two terms vanishes. In particular, if  $a = b = c = d = 1$ , Eq. (13) is reduced to Eq. (12) of the previous work<sup>4</sup> on the cases of homogeneous reaction coefficients.

By defining the relative reaction deficiencies of  $Red_1$  as

$$\left. \begin{aligned} \vartheta_r &= \phi - \alpha \\ \vartheta'_r &= 1 - \alpha \end{aligned} \right\} \quad (18)$$

Eq. (13) can be rewritten as

$$E_- = E_{eq}^0 + S + B + K(C_0, \phi, \rho) + \frac{ac - bd}{(n_1c + n_2b)\varphi} \cdot \ln(\phi - \vartheta_r) + \frac{bc}{(n_1c + n_2b)\varphi} \ln \frac{\vartheta_r}{1 - \phi + \vartheta_r} \quad (19)$$

and

$$E_+ = E_{eq}^0 + S + B + K(C_0, \phi, \rho) + \frac{ac - bd}{(n_1c + n_2b)\varphi} \ln(1 - \vartheta'_r) + \frac{bc}{(n_1c + n_2b)\varphi} \ln \frac{\phi - 1 + \vartheta'_r}{\vartheta'_r} \quad (19')$$

which represent the potential as functions of titration fraction with a parameter  $\vartheta_r$  or  $\vartheta'_r$ .

The magnitude and rate of variation of the reaction deficiencies in relation to titration fraction can be elucidated on the basis of the equilibrium constant expression

$$A = \exp(n_1n_2\varphi \Delta E_0) = F \cdot G \cdot \frac{\alpha^{a n_2 + d n_1}}{(1 - \alpha)^{n_2} (\phi - \alpha)^{n_1}} \quad (20)$$

where

$$\begin{aligned} \Delta E_0 &= E_2^0 - E_1^0 \\ F &= [f(C_0, \phi, \rho)]^{n_2(a-b) - n_1(c-d)} \end{aligned} \quad (21)$$

and

$$G = a^{n_2a} b^{n_1(c-d) - n_2c} c^{-n_1c} d^{n_1d} (n_2/n_1)^{n_1(c-d)}$$

In principle, Eq. (20) can be used in tabulating the relationships between  $\alpha$  and  $\phi$  or  $\vartheta$  and  $\phi$  for any given practical case, and in turn evaluation of potential at any desired titration fraction can be made, although the procedure may be quite cumbersome. On the other hand, an exact explicit expression of  $\alpha$  or  $\vartheta$  for general cases as a function of  $\phi$  can not be obtained in a simple form. The values of  $\vartheta$  obtained from Eq. (20) in the similar way as Bishop's method<sup>3</sup>, which amounts to the use of an equation corresponding to Eq. (20) to compute the absolute reaction deficiency, may be substituted into Eqs. (19) or (19') instead of the Nernst expression (11) or (12). In fact, when  $1 - \phi \gg \vartheta$ , the Nernst expression (11) can be approximated by

$$E_- = E_1^0 + \frac{1}{n_1\varphi} \ln \frac{\phi^0}{(1 - \phi)^b} + \frac{a}{n_1\varphi} \ln \frac{a}{b} + \frac{a - b}{n_1\varphi} \ln f(C_0, \phi, \rho) + D \quad (22)$$

where

$$D = \frac{(a - b)\phi - a}{n_1\varphi(1 - \phi)} \vartheta_r \quad (22')$$

Thus, when  $D$  is negligible, the only concentration dependent term is the fourth in the right-hand side of Eq. (22). It becomes independent of  $C$  when  $a = b$ , the half reaction of the titrand being homogeneous in coefficient. For example, if ferrous iron is titrated with dichromate, the titration curve for  $\phi$  smaller than and not close to unity will be independent of concentration of reagents whereas titration of thiosulfate with iodine will result in the shifting of titration curve downwards by 2.303 RT/2F volts for every ten-fold dilution.

For the particular point,  $\phi = \frac{1}{2}$ ,

$$E_{\frac{1}{2}} = E_1^0 - \frac{a - b}{n_1\varphi} \ln 2 + \frac{a}{n_1\varphi} \ln \frac{a}{b} + \frac{a - b}{n_1\varphi} \cdot \ln f(C_0, \frac{1}{2}, \varphi) + D_{\frac{1}{2}} \quad (22'')$$

The titration fraction where the potential is equal to  $E_1^0$  satisfies

$$1n \frac{(1-\phi+\vartheta_r)^b}{(\phi-\vartheta_r)^a} = a1n \frac{a}{b} + (a-b)1nf(C_0, \phi, \rho) \quad (23)$$

and where the potential is equal to  $E^{\vartheta_2}$

$$1n \frac{(1-\vartheta'_r)^d}{(\phi-1+\vartheta'_r)^c} = 1n \left( \frac{n_2 b}{n_1 d} \right)^d \cdot \left( \frac{n_1 c}{n_2 b} \right)^c + (c-d)1nf(C_0, \phi, \rho) \quad (24)$$

respectively, in view of Eqs. (11) and (12). Therefore, if the reaction is practically quantitative throughout the titration, the  $E^{\vartheta_1}$  point will shift towards and the  $E^{\vartheta_2}$  point away from the equivalence point as the concentration decreases, for the cases where both  $a-b$  and  $c-d$  are positive and, vice versa. It is clear now that the main contribution to the influence on the titration curve comes from the concentration function  $f(C_0, \phi, \rho)$  as long as the reaction is practically quantitative. It is obviously due to the fact that the potential depends on the reaction quotient whereas the titration fraction defines the concentration ratio; in other words, the position of the chemical equilibrium is determined by both the concentrations and concentration ratio unless the half reactions are homogeneous in coefficient. Eqs. (19) and (19') represent one of the expressions that indicate the effect of concentration of reagents and the quantitiveness of titration reaction on the potential at given titration fraction.

It may be worthwhile to note that  $f(C^0, \phi, \rho) = C_0$  when  $V$  can be considered to be zero as in coulometric titration whence  $\rho=0$ .

Unless there exists a particular relationship between the coefficients, the following equations are more convenient than Eqs. (19) and (19') for computing the potential in terms of reaction deficiency, which are obtained by substituting Eq. (20) into (19) and (19'):

$$E_- = E^{\vartheta_2} + S + \frac{1}{n_2 \varphi} \left[ \frac{1nG}{b} + (c-d)1nf(C_0, \phi, \rho) + c1n\vartheta_r - d1n(\phi - \vartheta_r) \right] \quad (19'')$$

and

$$E_+ = E^{\vartheta_1} + S + \frac{1}{n_1 \varphi} \left[ \frac{1nG}{c} + (a-b)1nf(C_0, \phi, \rho) - b1n\vartheta'_r + a1n(1 - \vartheta'_r) \right] \quad (19''')$$

## EQUIVALENCE-POINT POTENTIAL

Letting  $\phi=1$  in Eq. (13), the equivalence-point potential  $E_{eq}$  is obtained as

$$E_{eq} = E^{\lambda_{eq}} + S + B + K_{eq} + \frac{ac-bd}{(n_1c+n_2b)\varphi} 1n\alpha_{eq} \quad (25)$$

or in an approximate form

$$E_{eq} = E^{\lambda_{eq}} + S + B + K_{eq} - \frac{ac-bd}{n_1c+n_2b} \cdot \frac{\vartheta_{eq}}{\varphi} \quad (25')$$

if the reaction is practically quantitative at the equivalence point.

In particular cases where  $ac=bd$ , Eq. (25) reduces to

$$E_{eq} = E^{\lambda_{eq}} + S + B \quad (25'')$$

and all the concentration dependent terms vanish. Such a condition will be satisfied in many cases including the particular cases of  $a=b=c=d$  and  $a=d \neq b=c$ . It is note worthy that there can be many cases where the equivalence-point potential is independent of the concentrations of reagents even when the coefficients of the half reactions are inhomogeneous, although there may be deviation from  $E^{\lambda_{eq}}$  by a constant amount depending on relationship between the coefficients.

The general forms of each term appearing in Eq. (25) for several particular cases are listed in Table I. Whenever there is concentration dependence, i.e.,  $ac \neq bd$ , the equivalence-point potential shifts by  $\frac{bd-ac}{n_1c+n_2b} \cdot \frac{2.303}{\varphi}$  volts with every ten-fold dilution of the reagents. For example, in the titration of ferrous iron with dichromate where  $a=b=c=1$ ,  $d=2$ ,  $n_1=1$  and  $n_2=6$ , it amounts to 8.5 mv and in the titration of thiosulfate with  $I_7$ , where  $a=1$ ,  $b=2$ ,  $c=1$ ,  $d=3$ , and  $n_1=n_2=2$ , it amounts to 49.3mv. Thus, potentiometric titration up to a preassigned potential will be practical

only if  $ac=bd$  is satisfied. The numerical example studied elsewhere<sup>2</sup> is compared with the figures obtained by using Eq. (25) neglecting the last term ( $<10^{-2}$  mv) in Table 2.

As pointed out by Eq. (22'),  $E_{\frac{1}{2}}$  also depends on the concentration of reagents. Thus, it will be useful to elucidate the concentration dependence of  $E_{eq} - E_{\frac{1}{2}}$ ,  $E_{\frac{2}{3}} - E_{eq}$  and  $E_{\frac{2}{3}} - E_{\frac{1}{2}}$

TABLE 1. Terms representing shift of equivalence-point potential from  $E_{eq}^0$  in several particular cases

Concentration	independent terms	Concentration	dependent terms
S	B	$K_{eq}$	other
$a=b=c=d$	0	0	0
$a=d \neq b=c$	$-\frac{(a-b)}{(n_1-n_2)\phi} - 1n \frac{n_2}{n_1}$	0	0
$\frac{a=b=c=d^*}{ac=bd}$	$\frac{0}{(n_1c+n_2b)\phi} + \frac{1}{b} \left[ c1n \frac{a^n}{b^a} + b1n \frac{c^c}{d^d} + b(d-c)1n \frac{n_2}{n_1} \right]$	$\frac{(b-c)n_1n_2 \Delta E_0}{(n_1+n_2)(n_1c+n_2b)}$	0
$a=b=c \neq d$	$\frac{1}{(n_1+n_2)\phi} \left[ d1n \frac{a}{d} + (d-a)1n \frac{n_2}{n_1} \right]$	0	$\frac{(a-d)}{(n_1+n_2)\phi} - 1n \alpha_{eq}$
$a \neq b=c=d$	$\frac{a}{(n_1+n_2)\phi} - 1n \frac{a}{b}$		
$b=c \neq a=d$	$\frac{1}{\phi(n_1+n_2)} \left[ a1n \frac{a}{b} + d1n \frac{c}{d} + (d-c)1n \frac{n_2}{n_1} \right]$		

\* For the chemical reactions of well-known types,  $a=b$  will mean  $a=b=1$  and  $c=d$  will mean  $c=d=1$ ; thus  $b=c$  so that  $B=0$ .

In view of Eqs. (25), (22'') and the similar equation for  $E_{\frac{2}{3}}$  derived from Eq. (12), the following expressions are obtained.

$$E_{eq} - E_{\frac{1}{2}} = X(\rho) - \frac{b[n_2(a-b) - n_1(c-d)]}{n_1(n_1c + n_2b)\phi} - 1n C_0 + \Delta \quad (26)$$

$$E_{\frac{2}{3}} - E_{eq} = Y(\rho) - \frac{c[n_2(a-b) - n_1(c-d)]}{n_2(n_1c + n_2b)\phi} - 1n C_0 + \Delta' \quad (26')$$

$$E_{\frac{2}{3}} - E_{\frac{1}{2}} = Z(\rho) - \frac{n_2(a-b) - n_1(c-d)}{n_1n_2\phi} - 1n C_0 + \Delta'' \quad (26'')$$

where  $X$ ,  $Y$  and  $Z$  are constants determined by  $a$ ,  $b$ ,  $c$ ,  $d$ ,  $n_1$ ,  $n_2$  and  $\rho$ , and  $\Delta'$ ,  $\Delta''$ , and  $\Delta'''$  are small terms of the order of magnitude of the reaction deficiencies at  $\phi=1$ ,  $\phi=\frac{1}{2}$  and  $\phi=\frac{2}{3}$ , respectively. It is noteworthy that dilution of reagents not only results in a shift of titration curve as a whole but also widening the spacing between the two branches. Such an effect will affect the steepness of the titration curve in the vicinity of equivalence point, depending upon the sign and magnitude of  $[n_2(a-b) - n_1(c-d)] / (n_1n_2\phi)$ .

TABLE 2. Comparison of computed data.

$C_0=C=0.05M$ ;  $n_1=n_2=2$ ,  $a=2$ ,  $b=c=1$ ,  $d=3$ ;  $\Delta E_0=100$  mv;  $30^\circ C$ . ( $=38.26$  Volt<sup>-1</sup>),  $n_2(a-b) - n_1(c-d)=6$ .

(a) Potentials

Dilution factor	$(E_{eq} - E_{\frac{1}{2}})^*$	Differences Eq. (25')	$(E_{eq} - E_{\frac{1}{2}})^*$	Differences Eq. (26)
1	61.598 mv	+15.0 mv	$\frac{2.303}{4\phi}$	+45.00 mv $\frac{3 \times 2.303}{4\phi}$
0.1	76.592	+15.0	141.876	+45.00 45.0 mv
0.01	91.591		186.874	

## (b) Reaction deficiency

Dilution factor	$\delta_{eq}^*$	$\vartheta_{eq}$ from Eq. (28)	$\delta_{eq}$ computed**
1	$2.2075 \times 10^{-5}$	$8.83 \times 10^{-4}$	$2.23 \times 10^{-5}$
0.1	$6.9963 \times 10^{-5}$	$2.83 \times 10^{-5}$	$7.01 \times 10^{-5}$
0.01	$2.2126 \times 10^{-10}$	$8.93 \times 10^{-7}$	$2.23 \times 10^{-10}$

\* Reference 2.

\*\*  $\vartheta$  is multiplied by the expected concentration at the equivalence point.

## REACTION DEFICIENCIES

The knowledge of the relative reaction deficiency at the equivalence point is quite valuable because it will be the maximum value for the given system, and hence it will provide a criterion in making various approximations.

At the equivalence point, Eq. (20) can be written as

$$\frac{A}{F(1)G} = \frac{(1-\vartheta_{eq})an_2 + dn_1}{\vartheta_{eq}n_2b + n_1c} \quad (27)$$

with

$$F(1) = \left[ \frac{C_0}{1 + \frac{n_2b}{n_1c}\rho} \right]^{n_2(a-b) + n_1(c-d)}$$

Therefore, if  $\vartheta \ll 1$  can be assumed, the relative reaction deficiency at the equivalence point can be approximated by

$$\vartheta_{eq} = \left[ \frac{F(1)G}{A} \right]^{1/(n_2b + n_1c)} \quad (28)$$

and the absolute reaction deficiency at the equivalence point is given by

$$\delta_{eq} = \left[ \frac{G}{A} \cdot \left\{ \frac{C_0(1-\vartheta_{eq})}{1 + \frac{n_2b}{n_1c}\rho} \right\}^{an_2 + dn_1} \right]^{\frac{1}{n_2b + n_1c}} \\ = \left( 1 + \frac{n_2b}{n_1c} \right)^{-1} \cdot C_0 \vartheta_{eq} \quad (28')$$

Consequently, dilution of reagents will cause a decrease in relative reaction deficiency at the equivalence point if  $n_2(a-b) - n_1(c-d)$  is positive, and vice versa. If  $a=b$  and  $c=d$ , there will be no concentration effect on the relative reaction deficiency. The concentration dependence of reaction deficiencies is illustrated in Table 2.

The magnitude of the last term in Eq. (25')

can be estimated by Eq. (28).

If  $\vartheta_{eq}$  is proven to be negligible in comparison to unity, Eq. (20) can be converted to

$$1n\vartheta_r = -\frac{n_2\varphi\Delta E_0}{c} + \frac{1}{n_1c} 1nG + \frac{1}{n_1c} \cdot$$

$$1n \frac{an_2 + dn_1}{(1-\varphi)^{n_2b}} + \frac{n_2(a-b) - n_1(c-d)}{n_1c} \cdot$$

$$1nf(C_0, \phi, \rho) \quad (29)$$

for the range prior to the equivalence point where  $\vartheta_r \ll \phi$  and  $\vartheta_r \ll 1 - \phi$ , and

$$1n \vartheta'_r = -\frac{n_1\varphi\Delta E_0}{b} + \frac{1}{n_2b} 1nG + \frac{n_2(a-b) - n_1}{n_2b} \cdot$$

$$\frac{(c-d)}{n_2b} 1nf(C_0, \phi, \rho) - \frac{n_1c}{n_2b} 1n(\phi-1) \quad (29')$$

beyond the equivalence point where  $\phi - 1 > \vartheta'_r$ , is satisfied. It is interesting to note that relative reaction deficiency decreases as dilution increases if  $n_2(a-b) - n_1(c-d)$  is positive everywhere including the equivalence point. The concentration dependence of reaction deficiency is greater in the regions removed from equivalence point than at the equivalence point by a factor of  $\frac{n_1c + n_2b}{n_1c}$  or  $\frac{n_1c + n_2b}{n_2b}$ , as comparison of Eqs. (29) and (29') with Eq. (28) shows.

In the extreme vicinity of equivalence point, the relative reaction deficiency can not be neglected in comparison to  $1 - \phi$  or  $\phi - 1$  so that the approximate equations (29) and (29') do not apply. The procedure developed in the previous work<sup>4</sup> introducing a parameter  $f$  by  $1 - \phi = f\vartheta_r$  for  $\phi < 1$  and  $\phi - 1 = f\vartheta'_r$  for  $\phi > 1$  facilitates the calculation of reaction deficiency. Thus, from Eq. (20)

$$1n\vartheta_r = 1n\vartheta_{eq} + \frac{1}{n_2b + n_1c} \cdot \left[ (an_2 + dn_1) 1n(\phi -$$

$$\vartheta_r) - n_2 b \ln(f+1) + \ln \frac{F(\phi)}{F(1)} \quad (31)$$

and

$$\ln \vartheta'_r = \ln \vartheta_{eq} + \frac{1}{n_2 b + n_1 c} \cdot \left[ (a n_2 + d n_1) \ln(1 - \vartheta'_r) - n_1 c \ln(f+1) + \ln \frac{F(\phi)}{F(1)} \right] \quad (31')$$

Normally, relative reaction deficiencies will be negligible in comparison to  $\phi$  or unity, thus allowing approximation of  $f$  from Eq. (31) or (31') in conjunction with Eq. (30), and in turn reaction deficiencies. Namely,

$$\frac{1 - \phi}{\vartheta_{eq}} \approx f(f+1)^{-n_2 b / (n_2 b + n_1 c)} \quad (32)$$

or

$$\frac{\phi - 1}{\vartheta_{eq}} \approx f(f+1)^{-n_1 c / (n_2 b + n_1 c)} \quad (32)$$

is solved for  $f$ , and in turn  $f$  is used for calculating relative reaction deficiency by means of Eq. (30).

It should be noted that the procedure of calculating reaction deficiency given here has nothing to do with Nernst expression but based on the equilibrium constant expression. Therefore, it applies to any type of chemical equilibrium.

In order to have further information on reaction deficiency, it is desirable to compute its differential coefficient with respect to titration fraction. Differentiation of Eq. (20) after changing variable with respect to  $\phi$  gives

$$\frac{d\vartheta_r}{d\phi} = 1 - \frac{n_2 b \rho [n_2(a-b) - n_1(c-d)] + \frac{n_1 c}{\vartheta_r}}{n_1 c + n_2 b \phi \rho} + \frac{n_1 c}{\vartheta_r} \quad (33)$$

and

$$\frac{d\vartheta'_r}{d\phi} = - \frac{n_2 b \rho [n_2(a-b) - n_1(c-d)] + \frac{n_1 c}{\phi - 1 + \vartheta'_r}}{n_1 c + n_2 b \phi \rho} + \frac{n_1 c}{\vartheta'_r} + \frac{a n_2 + d n_1}{\phi - 1 + \vartheta'_r} \quad (33')$$

It is easily shown that at equivalence point

$$\frac{d\vartheta_r}{d\phi} - \frac{d\vartheta'_r}{d\phi} = 1$$

and, if  $\vartheta_{eq}$  is small enough,

$$\frac{d\vartheta_r}{d\phi} \approx \frac{n_2 b}{n_2 b + n_1 c} \quad \text{and} \quad \frac{d\vartheta'_r}{d\phi} \approx \frac{-n_1 c}{n_2 b + n_1 c}$$

which show no concentration dependence since the concentration dependent terms in the numerators of Eqs. (33) and (33') are negligible compared to the inverse of relative reaction deficiency if the reaction is practically quantitative. In such cases, Eqs. (33) and (33') can be approximated as

$$\frac{d\vartheta_r}{d\phi} \approx \frac{n_2 b \vartheta_r}{n_2 b \vartheta_r + n_1 c (1 - \phi + \vartheta'_r)} \quad (34)$$

and

$$\frac{d\vartheta'_r}{d\phi} \approx \frac{-n_1 c \vartheta'_r}{n_1 c \vartheta'_r + n_2 b (\phi - 1 + \vartheta'_r)} \quad (34')$$

in the extreme vicinity of equivalence point, and

$$\frac{n_1 c}{\vartheta_r} \cdot \frac{d\vartheta_r}{d\phi} \approx \frac{a n_2 + d n_1}{\phi} + \frac{n_2 b}{1 - \phi} - \frac{n_2 b [n_2(a-b) - n_1(c-d)] \rho}{(n_1 c + n_2 b \phi \rho)} \quad (35)$$

for  $\phi < 1$ , and

$$\frac{1}{\vartheta'_r} \cdot \frac{d\vartheta'_r}{d\phi} \approx - \frac{n_1 c}{n_2 b (\phi - 1)} - \frac{[n_2(a-b) - n_1(c-d)] \rho}{n_1 c + n_2 b \phi \rho} \quad (35')$$

for  $\phi > 1$ . It should be noted that the rate of change of the relative reaction deficiency in the extreme vicinity of equivalence point is of the order of unity and that in the region removed from equivalence point is the same order as the relative reaction deficiency. Furthermore, Eq. (35) indicates that reaction deficiency prior to equivalence point decreases with increasing  $\phi$  if  $n_2(a-b) - n_1(c-d)$  is positive, and vice versa. However, it increases with  $\phi$  without regard to the sign of  $n_2(a-b) - n_1(c-d)$  in the extreme vicinity of equivalence point. Therefore, reaction deficiency should pass through a minimum if the latter is positive. More detailed features can be seen by differentiating Eq. (29) with respect to  $\phi$ ; of course the result applies where Eq. (29) is valid. Thus, the root of Eq. (35) will give the position of the minimum  $\vartheta_r$ . It should be noted that, if  $\rho = 0$  or in

the case of internal generation of  $Ox_2$  by electrolysis,  $\frac{d\vartheta_r}{d\phi}$  will be always positive prior to the equivalence point regardless of the sign of  $n_2(a-b) - n_1(c-d)$ . On the other hand, Eq. (35') indicates that  $\vartheta_r'$  will go through a maximum in the region  $\phi > 1$ .

The rate of variation of relation deficiency with respect to titration fraction depends on concentration of reagents implicitly through relative reaction deficiency itself.

Although  $\frac{d\vartheta}{d\phi}$  is at most of the order of unity, relative rate of variation  $\frac{1}{\vartheta} \cdot \frac{d\vartheta}{d\phi}$  will be very large when the reaction is practically complete. The completeness of reaction can be judged by computing  $\vartheta_{eq}$  by using Eq. (28).

Differentiation of Eqs. (34) and (34') gives

$$\frac{d^2\vartheta_r}{d\phi^2} = \frac{n_2b n_1c(n_2b+n_1c)(1-\phi+\vartheta_r)\vartheta_r}{[n_2b\vartheta_r+n_1c(1-\phi+\vartheta)]^3} \quad (36)$$

and

$$\frac{d^2\vartheta_r'}{d\phi^2} = \frac{n_2b n_1c(n_2b+n_1c)(\phi-1+\vartheta_r')\vartheta_r'}{[n_1c\vartheta_r'+n_2b(\phi-1+\vartheta_r')]^3} \quad (36')$$

respectively, which are both positive and of the order of  $\frac{1}{\vartheta}$  whereas differentiation of Eqs. (35) and (35') shows that  $\frac{d^2\vartheta}{d\phi^2}$  are of the order of  $\vartheta$  at the regions removed appreciably from the equivalence point. Thus, it is evident that the variation of  $\frac{d\vartheta}{d\phi}$  is mostly concentrated around the equivalence point.

It should be noted that results on the study of relative reaction deficiency as a function of titration fraction given above apply to any chemical equilibrium, they are obtained from Eq. (20) only.

## VARIATION OF POTENTIAL WITH TITRATION FRACTION

Differentiation of Eqs. (19) and (19') gives

$$\frac{dE_-}{d\phi} = \frac{1}{(n_2b+n_1c)\varphi} \cdot \left[ -(ac-bd) \frac{n_2b\rho}{n_1c+n_2b\phi\rho} + (ac-bd) \frac{1}{\phi-\vartheta_r} \left(1-\frac{d\vartheta_r}{d\phi}\right) + bc \frac{1}{\vartheta_r} \cdot \frac{d\vartheta_r}{d\phi} \right]$$

$$- \frac{bc}{1-\phi+\vartheta_r} \left(\frac{d\vartheta_r}{d\phi} - 1\right) \quad (37)$$

and

$$\frac{dE_+}{d\phi} = \frac{1}{(n_2b+n_1c)\phi} \cdot \left[ -(ac-bd) \frac{n_2b\rho}{n_1c+n_2b\phi\rho} - (ac-bd) \frac{1}{1-\vartheta_r'} \cdot \frac{d\vartheta_r'}{d\phi} - \frac{bc}{\vartheta_r'} \cdot \frac{d\vartheta_r'}{d\phi} + \frac{bc}{\phi-1+\vartheta_r'} \left(1+\frac{d\vartheta_r'}{d\phi}\right) \right] \quad (37')$$

respectively. Those equations are convenient at the equivalence point only if  $ac=bd$ . Otherwise, the following equations obtained by differentiating Eqs. (19'') and (19''') may be more convenient:

$$\frac{dE_-}{d\phi} = \frac{b(d-c)\rho}{(n_1c+n_2b\phi\rho)\varphi} + \frac{c}{n_2\varphi} \cdot \frac{1}{\vartheta_r} \cdot \frac{d\vartheta_r}{d\phi} + \frac{d}{n_2\varphi} \cdot \frac{1}{\phi-\vartheta_r} \left(\frac{d\vartheta_r}{d\phi} - 1\right) \quad (38)$$

and

$$\frac{dE_+}{d\phi} = \frac{n_2b(b-a)\rho}{n_1(n_1c+n_2b\phi\rho)\varphi} - \frac{b}{n_1\varphi} \cdot \frac{1}{\vartheta_r'} \cdot \frac{d\vartheta_r'}{d\phi} - \frac{a}{n_1\varphi} \cdot \frac{1}{1-\vartheta_r'} \cdot \frac{d\vartheta_r'}{d\phi} \quad (38')$$

At the equivalence point, both types of equations give

$$\left(\frac{dE}{d\phi}\right)_{eq} = \frac{bc}{\vartheta_{eq}} \cdot \frac{1}{n_1c+n_2b} \cdot \frac{1}{\varphi} \quad (39)$$

if  $\vartheta_{eq}$  can be neglected in comparison to unity.

$$\text{More explicitly } = \left(\frac{dE}{d\phi}\right)_{eq} = \frac{n_2(a-b) - n_1(c-d)}{n_1c+n_2b} \cdot \left[ \frac{A}{G} \frac{1}{n_1c+n_2b} \cdot \left[ \frac{n_1c+n_2b\rho}{n_1c} \frac{C_o}{C_o} \right] + \frac{bc}{(n_1c+n_2b)\varphi} \right] \quad (39')$$

Therefore, the steepness of titration curve at the equivalence point will depend on the concentration of reagents unless  $n_2(a-b) - n_1(c-d)$  vanishes, which is in accordance with the qualitative anticipation from Eq. (26'). It is remarkable that, in view of Eq. (39'), if  $a=b$  and  $c=d$ , even when  $\Delta E_o$  is not large enough so that reaction deficiency at normal concentration is not sufficiently small, sharpness of potentiometric end point can be made greater by using more dilute solutions of reagents. In practice, however, response of indicating electrode bec-



comes slower with dilution of reagents and sets the limits on the effectiveness of dilution.

Differentiation of Eq.(38) and(38') gives

$$n_2\varphi \frac{d^2E_-}{d\phi^2} = \frac{(n_2b\rho)^2(d-c)}{(n_1c+n_2b\phi\rho)^2} + c \frac{\left[ \vartheta_r \frac{d^2\vartheta_r}{d\phi^2} - \left( \frac{d\vartheta_r}{d\phi} \right)^2 \right]}{\vartheta_r^3} + d \frac{\left[ (\phi-\vartheta_r) \frac{d^2\vartheta_r}{d\phi^2} + \left( \frac{d\vartheta_r}{d\phi} - 1 \right)^2 \right]}{(\phi-\vartheta_r)^2} \quad (40)$$

and

$$n_1\varphi \frac{d^2E_+}{d\phi^2} = \frac{(n_2b\rho)^2(b-a)}{(n_1c+n_2b\phi\rho)^2} - b \frac{\left[ \vartheta_r' \frac{d^2\vartheta_r'}{d\phi^2} - \left( \frac{d\vartheta_r'}{d\phi} \right)^2 \right]}{\vartheta_r'^3} - a \frac{\left[ (1-\vartheta_r') \frac{d^2\vartheta_r'}{d\phi^2} - \left( \frac{d\vartheta_r'}{d\phi} \right)^2 \right]}{(1-\vartheta_r')^2} \quad (40')$$

respectively. Substitution of values for  $\frac{d\vartheta}{d\phi}$  given by Eq. (33) and for  $\frac{d^2\vartheta}{d\phi^2}$  computed from Eq. (36) into Eqs. (40) results in

$$\varphi \left( \frac{d^2E}{d\phi^2} \right)_{eq} = \frac{(n_2b\rho)^2(d-c)}{n_2(n_1c+n_2b\rho)^2} + \frac{n_1c-n_2b}{(n_2b+n_1c)^2} \cdot \frac{bc}{\vartheta_{eq}^2} + \frac{n_1bcd}{(n_2b+n_1c)^2\vartheta_{eq}} \quad (41)$$

and, similarly, using Eq. (33'), (36') and (40')

$$\varphi \left( \frac{d^2E_1}{d\phi^2} \right)_{eq} = \frac{(n_2b\rho)^2(b-a)}{n_1(n_1c+n_2b\rho)^2} + \frac{n_1c-n_2b}{(n_2b+n_1c)^2} \cdot \frac{bc}{\vartheta_{eq}^2} + \frac{n_2abc}{(n_2b+n_1c)^2\vartheta_{eq}} \quad (41')$$

respectively; note that Eq. (40) and (40') are exact but Eqs. (41) and (41') are approximate formulas. (40') are exact but show that the major term is the same and its sign is determined by the term  $n_1c - n_2b$ .

In homogeneous case, where  $a=b=c=d=1$ , it was already noted that the inflexion point of potentiometric titration is located either beyond or prior to the equivalence point depending upon  $n_1 > n_2$  or  $n_1 \leq n_2$ . (see Eq. (54') of reference 4.) The abovementioned results show that the inflexion point is located prior to the equivalence point if  $n_1c > n_2b$  and beyond the later if  $n_1c < n_2b$ . As pointed out at the end of the last section,  $\frac{d\vartheta}{d\phi}$  varies mostly in the vicinity of the equivalence point. In view of Eqs. (38) and (38'),  $\frac{dE}{d\phi}$  varies mostly in the same

region, accordingly. Therefore, the approximate location of the inflexion point of the potentiometric titration curve can be obtained by substituting Eqs.(34) or (34') into the second terms of [Eqs. (41) or (41')] and putting the latter terms equal to zero. The results of such approximation are

$$1 - \phi + \frac{n_2^2b^2 - n_1^2c^2}{n_1^2c^2}, \text{ if } n_1c < n_2b \quad (42)$$

and

$$\phi - 1 = \frac{n_1^2c^2 - n_2^2b^2}{n_2^2b^2}, \text{ if } n_1c > n_2b \quad (42')$$

respectively. Thus, the deviation of the inflexion point from the equivalence point is the same order of magnitude as  $\vartheta_{eq}$ . Utilizing Eqs. (32) and (42), the deviation for the case where  $n_1c < n_2b$  is obtained as

$$1 - \phi = \left[ \frac{(n_1c)^{2(n_2b-1)} \cdot (n_2^2b^2 - n_1^2c^2)}{(n_2b)^{2n_2b}} \right]^{\frac{1}{n_2b + n_2c}} \cdot \vartheta_{eq} \quad (42'')$$

which will be normally very close to  $\vartheta_{eq}$ . In view of Eqs. (42'') and (28), the deviation of the inflexion point from the equivalent point depends on the  $\Delta E^0$  value as well as concentration of the reagent as long as  $n_2(a-b) - n_1(c-d)$  does not vanish.

## EFFECT OF EXCHANGING TITRANT AND TITRAND

For a given titration reaction represented by Eq. (3), if  $V^0$  liters of  $C_0$  molar solution of  $Ox_2$  is titrated with  $V$  liters of  $C$  molar solution of  $Red_1$ , assuming the fraction of  $Ox_2$  converted to  $Red_2$  to be  $\alpha'$ , the following equations are obtained:

$$E = E^0_1 + \frac{1}{n_1\varphi} 1n \frac{\alpha'^a}{(\phi' - \alpha')^b} + \frac{1}{n_1\varphi} 1n \left( \frac{n_2d}{n_1c} \right)^c \cdot \left( \frac{n_1c}{n_2b} \right)^d + \frac{a-b}{n_1\varphi} 1nf(C_0, \phi', \rho) \quad (43)$$

$$E = E^0_2 + \frac{1}{n_2\varphi} 1n \frac{(1-\alpha')^c}{\alpha'^d} + \frac{1}{n_2\varphi} 1n \frac{c}{d} + \frac{c-d}{n_2\varphi} 1nf(C_0, \phi', \rho) \quad (44)$$

$$E = E^0_{eq} + S' + B + K(C_0, \phi', \rho) + \frac{ac-bd}{(n_2b+n_1c)\varphi}$$

$$1n\alpha' + \frac{bc}{(n_2b+n_1c)\varphi} 1n \frac{1-\alpha'}{\phi' - \alpha'} \quad (45)$$

where

$$\phi' = \frac{CV n_1c}{C_0 V_0 n_2b}$$

$$S' = \frac{1}{(n_2b+n_1c)\varphi} \left[ -bc 1nb + (ac+bd-bc)1nc \right. \\ \left. + (ac-bd)1nd - c(a-b)1n \frac{n_2}{n_1} \right]$$

The equilibrium constant is represented by

$$A = \frac{\alpha'^{n_2} \alpha_2^{n_1}}{(1-\alpha')^{n_1} (\phi' - \alpha')^{n_2}} \cdot F \cdot G'$$

where

$$G' = a^{n_2} \cdot b^{-n_2} \cdot c^{n_2b-n_1c} \cdot d^{n_1c} \cdot \left( \frac{n_2}{n_1} \right)^{n_2(a-b)} \quad (46)$$

In particular, at the equivalence point, the following equations are satisfied:

$$E'_{eq} = E^h_{eq} + S' + B + K_{eq} + \frac{ac-bd}{(n_2b+n_1c)\varphi} 1n\alpha'_{eq} \quad (47)$$

$$\vartheta'_{eq} = 1 - \alpha'_{eq} \approx \left[ \frac{F(1) \cdot G'}{A} \right]^{\frac{1}{n_2b+n_1c}} \quad (48)$$

$$\left( \frac{d\vartheta'}{d\phi'} \right)_{eq} \approx \frac{n_1c}{n_2b+n_1c} \quad (49)$$

$$\left( \frac{dE}{d\phi'} \right)_{eq} = \frac{1}{(n_2b+n_1c)\varphi} \left[ \frac{dK}{d\phi'} + \frac{ac-bd}{1-\vartheta'} \right. \\ \left. \left( 1 - \frac{d\vartheta'}{d\phi'} \right) - \frac{bc}{\vartheta'} \right]_{eq} \approx \frac{bc}{(n_2b+n_1c)\varphi} \cdot \frac{1}{\vartheta'_{eq}} \cdot \\ \approx \frac{bc}{(n_2b+n_1c)\varphi} \cdot \left[ \frac{A}{F(1) \cdot G'} \right]^{\frac{1}{n_2b+n_1c}} \quad (50)$$

From Eqs. (50) and (30)

$$\left( \frac{dE}{d\phi'} \right)_{eq} \approx \left[ \frac{G'}{A} \right]^{\frac{1}{n_2b+n_1c}} \approx \left[ \frac{n_2b}{n_1c} \right]^{\frac{n_2(a-b)-n_1(c-d)}{n_2b+n_1c}} \quad (51)$$

and from Eqs. (49) and (33)

$$\left( \frac{d\vartheta'}{d\phi'} \right)_{eq} \approx \frac{n_2b}{n_1c} \quad (52)$$

are obtained. It should be noted that  $n_2b/n_1c$  is the ratio of the coefficients of the titrands in the overall chemical equation (3).

Eqs. (51) and (52) indicate that the steepness of the potentiometric titration curves at the equivalence point takes different values when the titrand and titrant are exchanged in a

given pair of reagents. In the potentiometric titration, the change of steepness depends on both the ratio  $n_2b/n_1c$  and the sign and magnitude of  $n_2(a-b) - n_1(c-d)$ . On the other hand, in spectrophotometric or amperometric titration, where the reaction deficiency is followed, it depends only on the ratio  $n_2b/n_1c$ .

Eqs. (45), (48) and (50) indicate that the concentration dependence of the titration curves is in the same direction as the reverse titration and determined by the sign of  $n_2(a-b) - n_1(c-d)$

## EFFECT OF BUFFERING ACTION ON AN REAGENT

In practical titrations, it is possible to have buffering action on one or more reagents involved in the oxidation-reduction reaction. For example, in the titrations involving iodine solution the iodide concentration does not change appreciably. In such cases, the coefficient of the buffered reagent in the half reaction can be considered to be zero and the effects of the buffering reagents is included in the formal potential  $E$ . When a gaseous product or precipitate that dissolves sparingly in the solution is formed in the titration, the same will hold. Thus, the concentration dependence of the potential curve as well as the steepness of the curve at the equivalence point will be affected by buffering action on any reaction component by affecting the numerical values of  $(ac-bd)$ ,  $n_2(a-b) - n_1(c-d)$ ,  $G$ ,  $F$ , and relative reaction deficiency.

## LITERATURES CITED

1. A. J. Bard and S.H. Simonsen, *J. Chem. Ed.* **37**, 364(1960)
2. E. Bishop, *Anal. Chim. Acta* **27**, 253(1962)
3. E. Bishop, *ibid.*, **26**, 397(1962)
4. Q. Won Choi, *J. Korean Chem. Soc.*, **11**, 159(1967)