

## Transient State Theory of Significant Liquid Structure Applied to Nitrogen Oxides

by

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### 액체 구조의 천이상태이론의 질소산화물들에 대한 적용

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#### 요 약

액체구조의 천이상태이론을 아산화질소( $N_2O$ )와 사산화질소( $N_2O_4$ )에 적용하여 이 액체들의 상태합을 유도하였다. 이상상태합들을 써서 각 액체의 몰부피, 증기압, 증발엔트로피, 임계점에서의 성질 등, 여러 가지 열역학적 양들을 계산한 결과 모두 실험치와 좋은 일치를 얻었다.

#### Abstract

The transient state theory of significant liquid structure is applied to nitrous oxide and nitrogen tetroxide. The partition functions for the two liquids are derived according to the transient state theory. The various thermodynamic properties; such as, molar volumes, vapor pressures, entropies of vaporization, and critical point properties agree well with the experimental values.

#### Introduction

The transient state theory of significant liquid structure developed by S. Chang et al has been applied to various liquids including binary mixtures successfully<sup>(1)-(3)</sup>. This work is the further application of the theory to nitrogen oxides,  $N_2O$  and  $N_2O_4$ .

Both  $N_2O$  and  $N_2O_4$  have anomalous physical properties in the liquid state.  $N_2O$  has a very short liquid range, an unusually high vapor pressure at the triple point, and an enormous entropy of fusion<sup>(4)</sup>. Although X-ray diffraction studies<sup>(5)</sup>, and other experimental works<sup>(6)-(8)</sup> reveal that  $N_2O_4$  molecules do not

dissociate in the solid state, they dissociate to  $NO_2$  in both gaseous and liquid states. It is also found that the degree of dissociation of  $N_2O_4$  is far less in the liquid state than in the gaseous state.  $N_2O_4$  molecules form symmetrical planer structures<sup>(5)</sup>.

#### Formulation of the Partition Function

##### A. Theoretical Considerations

According to the transient state theory of significant liquid structure<sup>(1)</sup>, the liquid possesses three kinds of degree of freedom, i. e. the solid-like, the transient, and the gas-like degrees of freedom. The proposed theory assumes that the transition of the degrees of freedom from the solid-like to gas-like takes place only through a transient state. Here, the

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transient state is such a state that molecules are in different energy state from solid-like molecules by acquiring strain energy due to the structural distortion. According to the theory, the number of holes introduced in a random fashion among  $N$  molecules, is assumed to be  $N(V-V_s)/V_s$ , where  $N$ ,  $V$ , and  $V_s$  are Avogadro's number, the molar volume of liquid, and the molar volume of solid-like molecules, respectively; then, only  $N(V_s/V)$  molecules must be bonded to each other.

Therefore, among  $N$  molecules,  $N(V-V_s)/V$  molecules have gas-like degree of freedom, and the remaining  $N(V_s/V)$  molecules are partitioned among the solid-like and the transient degrees of freedom in such a manner that  $\alpha N(V_s/V)$  and  $(1-\alpha)N(V_s/V)$  are the numbers of molecules possessing solidlike and transient degrees of freedom, respectively. Here,  $\alpha$  is a fractional number.

The strain energy, " $\epsilon$ ", which is the energy difference between solid-like and transient states, is proportional to the heat of sublimation,  $E_s$ , and inversely proportional to the number of vacant sites around a molecule (in other words, the number of positional-degeneracy,  $n(V-V_s)/V_s$ ; here,  $n=12V_s/V_t$ , where  $V_t$  is the molar volume of liquid at the triple point. Therefore,  $\epsilon = aE_s/n(X-1)$ , where  $X=V/V_s$ , and " $a$ " is a proportionality constant. Accordingly, the partition function for the liquid can be written as

$$F = \frac{(N_s + N_t)!}{N_s! N_t!} \cdot f_s^{N_s} \cdot f_t^{N_t} \cdot f_g^{N_g} \cdot \frac{1}{N_s!} \\ = \frac{[(V_s/V)N]!}{\left[\frac{V_s}{V} \alpha N\right]! \left[\frac{V_s}{V} (1-\alpha)N\right]!} \left[ \frac{e^{E_s/RT}}{(1-e^{-\theta_s/T})^s} b_s \right]^{\frac{V_s}{V} \alpha N} \\ \left( \frac{n \frac{V-V_s}{V_s} e^{(E_s-\epsilon N)/RT}}{(1-e^{-\theta_t/T})^s} b_t \right)^{\frac{V_s}{V} (1-\alpha)N} \\ \left[ \frac{(2\pi mkT)^{3/2} (V-V_s)}{h^3} b_r \right]^{\frac{V-V_s}{V} N} \frac{1}{\left[\frac{V-V_s}{V} N\right]!} \quad (1)$$

where " $\theta$ " is the Einstein's characteristic temperature;  $E_s$ , the sublimation energy of solid-like molecules. " $b$ " is the partition function for molecular rotational and vibrational degrees of freedom; here, subscripts  $s$ ,  $t$ , and  $g$  designate the states of solid-like, transient, and gas-like, respectively. A combinatorial factor,  $(N_s + N_t)! / (N_s! N_t!)$ , is used, because it is assumed that molecules of solid-like and transient are

mixed in a random fashion.

Einstein's oscillator model is applied to both the solid-like and the transient states, and the gas-like molecules are assumed to behave like an ideal gas.

### B. The Partition Function for $N_2O$

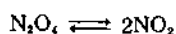
There are experimental evidences that a  $N_2O$  molecule has a linear structure and that the linear molecules of  $N_2O$  do not rotate freely in the solid state near the melting point<sup>(4),(9)</sup>. Therefore, it can be assumed that a  $N_2O$  molecule in the solid-like state or in the transient state has four vibrational degrees of freedom and its Einstein's oscillator has five degrees of freedom.

Accordingly, the partition function for liquid  $N_2O$  can be written as

$$F_{N_2O} = \frac{\left[\frac{V_s}{V} N\right]!}{\left[\frac{V_s}{V} \alpha N\right]! \left[\frac{V_s}{V} (1-\alpha)N\right]!} \\ \left[ \frac{e^{E_s/RT}}{(1-e^{-\theta_s/T})^s} \prod_{i=1}^4 \frac{1}{1-e^{-h\nu_i/kT}} \right]^{\frac{V_s}{V} \alpha N} \\ \left( \frac{n \frac{V-V_s}{V_s} e^{(E_s-\epsilon N)/RT}}{(1-e^{-\theta_t/T})^s} \prod_{i=1}^4 \frac{1}{1-e^{-h\nu_i/kT}} \right)^{\frac{V_s}{V} (1-\alpha)N} \\ \left( \frac{(2\pi mkT)^{3/2} (V-V_s)}{h^3} \frac{8\pi^3/kT}{h^2} \prod_{i=1}^4 \frac{1}{1-e^{-h\nu_i/kT}} \right)^{\frac{V-V_s}{V} N} \frac{1}{\left[\frac{V-V_s}{V} N\right]!} \quad (2)$$

### C. The Partition Function for $N_2O_4$

$N_2O_4$  molecules do not dissociate in the solid state. In the liquid state, they dissociate somewhat; however, the degree of dissociation for liquid  $N_2O_4$  is negligibly small compared with gaseous  $N_2O_4$ . Therefore, in formulating the partition function for  $N_2O_4$  liquid, the dissociation of gas-like molecules is considered only. In consideration of the dissociation of gas-like molecules, the following equilibrium can be assumed.



where  $z$  is the degree of dissociation. Therefore, the gas-like degrees of freedom is partitioned by  $(1-z) \cdot (V-V_s)/V$  for  $N_2O_4$  and  $2z(V-V_s)/V$  for  $NO_2$ .

The nitrogen dioxide molecule has two electronic degeneracies and two symmetry numbers, while  $N_2O_4$

molecule has four symmetry numbers only<sup>(5)</sup>. In the solid like and the transient states, the N<sub>2</sub>O<sub>4</sub> molecule has 12 vibrational degrees of freedom and its Einstein's oscillator has 6 degrees of freedom.<sup>(11),(12)</sup>

Accordingly, the partition function for N<sub>2</sub>O<sub>4</sub> can be written as

$$F_{N_2O_4} = \frac{\left[\frac{V_s}{V}N\right]_f}{\left[\frac{V_s}{V}\alpha N\right]_f \left[\frac{V_s}{V}(1-\alpha)N\right]_f} \left( \frac{e^{E_s/RT}}{(1-e^{-\theta_s/T})^6} \prod_{i=1}^{12} \frac{1}{1-e^{-h\nu_i/kT}} \right)^{\frac{V_s}{V}\alpha N} \left( \frac{V-V_s}{V_s} e^{(E_s-\epsilon_s N)/RT} \frac{1}{(1-e^{-\theta_s/T})^6} \prod_{i=1}^{12} \frac{1}{1-e^{-h\nu_i/kT}} \right)^{\frac{V_s}{V}(1-\alpha)N}$$

$$\left[ \frac{(2\pi mkT)^{3/2}(V-V_s)}{h^3} \frac{\pi^{1/2}(8\pi^2 kT)^{3/2}(IA'IB'IC')^{1/2}}{4h^3} \prod_{i=1}^{12} \frac{1}{1-e^{-h\nu_i/kT}} \right]^{\frac{V-V_s}{V}(1-\alpha)N} \left[ \frac{V-V_s}{V} \frac{1}{(1-\alpha)N} \right]_f$$

$$\left[ g \frac{(2\pi m'kT)^{3/2}(V-V_s)}{h^3} \frac{\pi^{1/2}(8\pi^2 kT)^{3/2}(IA'I_B'I_C')^{1/2}}{2h^3} e^{-D/RT} \prod_{i=1}^3 \frac{1}{1-e^{-h\nu_i/kT}} \right]^{\frac{V-V_s}{V}2\alpha N} \left[ \frac{V-V_s}{V} \frac{1}{2\alpha N} \right]_f \quad (3)$$

where *D* is dissociation energy at the ground state; *g*, the electronic degeneracy of NO<sub>2</sub>; *m'*, *I*A', *I*B', *I*C', and *ν*<sub>*i*</sub> are molecular mass, three moments of inertia and vibrational frequencies for NO<sub>2</sub> molecules, respectively.

**Determination of Parameters**

Since the free energy of a system becomes minimum at equilibrium, the following relationship can be obtained.

$$\alpha = \frac{f_s}{f_s + f_t} \quad (4)$$

Substituting equation (4) into equations (2) and (3), the following equations can be obtained.

$$F_{N_2O} = \left[ \frac{e^{E_s/RT}}{(1-e^{-\theta_s/T})^6} \{1 + \lambda(x-1)e^{-\alpha E_s/n(x-1)RT}\} \prod_{i=1}^6 \frac{1}{1-e^{-h\nu_i/kT}} \right]^{1N} \left[ \frac{(2\pi mkT)^{3/2}}{h^3} \frac{eV}{N} \frac{8\pi^2 kT}{h^3} \prod_{i=1}^6 \frac{1}{1-e^{-h\nu_i/kT}} \right]^{(1-\frac{1}{2})N}$$

$$\left[ \frac{f_s' e}{2\alpha N} \right]^{(1-\frac{1}{2})2\alpha N} \quad (5)$$

where  $\lambda = n \left( \frac{1-e^{-\theta_s/T}}{1-e^{-\theta_t/T}} \right)^6$

$$F_{N_2O_4} = \left[ \frac{e^{E_s/RT}}{(1-e^{-\theta_s/T})^6} \left\{ 1 + \lambda(x-1) e^{-\frac{\alpha E_s}{n(x-1)RT}} \right\} \prod_{i=1}^{12} \frac{1}{1-e^{-h\nu_i/kT}} \right]^{1N} \left[ \frac{f_s' e}{(1-\alpha)N} \right]^{(1-\frac{1}{2})(1-\alpha)N}$$

$$\left[ \frac{f_s' e}{2\alpha N} \right]^{(1-\frac{1}{2})2\alpha N} \quad (6)$$

where  $\lambda = n \left( \frac{1-e^{-\theta_s/T}}{1-e^{-\theta_t/T}} \right)^6$

$$f_s = \frac{(2\pi mkT)^{3/2} V}{h^3} \frac{\pi^{1/2}(8\pi^2 kT)^{3/2}(IA'IB'IC')^{1/2}}{4h^3} \prod_{i=1}^{12} \frac{1}{1-e^{-h\nu_i/kT}}$$

$$f_s' = g \frac{(2\pi m'kT)^{3/2} V}{h^3} \frac{\pi^{1/2}(8\pi^2 kT)^{3/2}(IA'I_B'I_C')^{1/2}}{2h^3} \prod_{i=1}^3 \frac{1}{1-e^{-h\nu_i/kT}} e^{-D/RT}$$

From equation (5), the parameters for N<sub>2</sub>O are determined at the triple point according to the method developed by S. Chang et al<sup>(1)</sup>.

From thermodynamic equilibrium condition,

$$\left( \frac{\partial A}{\partial x} \right)_{N, V, T} = -kT \left( \frac{\partial \ln F_{N_2O_4}}{\partial x} \right)_{N, V, T} = 0 \quad (7)$$

the following expression is obtained.

$$\frac{f_s'^2}{f_s} = \frac{(2\alpha)^2}{1-\alpha} N \quad \text{or} \quad \left( \frac{f_s'}{2\alpha} \right)^2 \frac{1}{N} = \frac{f_s}{1-\alpha} \quad (8)$$

Rewriting equation (8),

$$\ln \frac{(2\alpha)^2}{1-\alpha} = -\frac{2D}{RT} + 3 \ln T + \ln V + \sum_{i=1}^{12} \ln(1-e^{-h\nu_i/kT}) - 2 \sum_{i=1}^3 \ln(1-e^{-h\nu_i/kT}) + K \quad (9)$$

where

$$K = \ln \left\{ g^2 \frac{(2\pi k)^{3/2}}{h^3 N^{5/2}} \left( \frac{M'}{2} \right)^{3/2} \frac{\pi^{1/2} (8\pi^2 k)^{3/2}}{h^3} \frac{IA'I_B'I_C'}{(IA'IB'IC')^{1/2}} \right\}$$

Since, equation (9) holds for the vapor phase, the dissociation energy for gaseous N<sub>2</sub>O<sub>4</sub> can be calculated by the use of equation (9), substitution *V*<sub>g</sub> and *z*<sub>g</sub> for *V* and *z*, respectively. The value for *V*<sub>g</sub> is calculated from the expression, *V*<sub>g</sub> = (1 + *z*<sub>g</sub>)*RT*/*P* (the ideal gas equation); and the literature value<sup>(13)</sup> for *z*<sub>g</sub>, 0.08737, is used for the calculation. The dissociation energy thus obtained is 6593 cal./mole.

Introducing equation (8) into equation (6), we obtain

$$F_{N_2O_4} = \left[ \frac{e^{E_s/RT}}{(1-e^{-\theta_s/T})^6} \left\{ 1 + \lambda(x-1) e^{-\frac{\alpha E_s}{n(x-1)RT}} \right\} \prod_{i=1}^{12} \frac{1}{1-e^{-h\nu_i/kT}} \right]^{1N}$$

$$\prod_{i=1}^3 \left[ \frac{1}{1 - h_i v_i / RT} \right]^{1/2} \left[ f_{\epsilon} \frac{e^{\epsilon}}{1 - z} \right] \left( 1 - \frac{1}{z} \right)^N \quad (10)$$

Assigning appropriate value for  $E_s$  in equation (10), the parameters for  $N_2O_4$  are obtained according to the method developed by S. Chang and et al<sup>(1)</sup>.

The literature values used for parameter determinations are:

For  $N_2O$ :

$T_b$ , Boiling point 183.65° K<sup>14</sup>

$V_s$ , Molar volume of solid-like molecules  
28.18 cc/mole<sup>15</sup>

$V_l$ , Molar volume of liquid at b. p. 35.90 cc/mole<sup>14</sup>

$\Delta H_{vap}$ , Heat of vaporization 90.1 cal/gram<sup>15</sup>

$I$ , Moment of Inertia<sup>17</sup>  $66.0 \times 10^{-40}$  gr. -cm<sup>2</sup>

For  $N_2O_4$ :

$V_s$ , Molar volume of solid-like molecules  
47.09 cc/mole<sup>5</sup>

$V_t$ , Molar volume of liquid at triple pt.  
60.82 cc/mole<sup>18</sup>

$P_t$ , Vapor pressure at triple pt. 0.1839 atm.<sup>11</sup>

$T_t$ , Triple point temp. 261.95° K<sup>11</sup>

$I_A' I_B' I_C' = 1.44 \times 10^{-116}$  gr<sup>3</sup> -cm<sup>6</sup>

$I_A I_B I_C^* = 8.798 \times 10^{-114}$  gr<sup>3</sup> -cm<sup>6</sup>

\*This is calculated from the molecular structure<sup>5</sup>.

The parameters thus obtained are

For  $N_2O$

$\theta_s = 64.83^\circ K$

$\theta_l = 54.70^\circ K$

$E_s = 5478$  cal/mole

$a = 0.1725$

For  $N_2O_4$

$\theta_s = 60.92^\circ K$

$\theta_l = 45.80^\circ K$

$E_s = 1.060 \times 10^4$  cal/mole

$a = 0.2531$

## Calculation of Thermodynamic Properties

### A. Vapor Pressures and Molar Volumes

Using the expression,

$$A = -kT \ln F \quad (11)$$

the curve for Helmholtz free energy vs volume is plotted at a constant temperature as shown in Figure 1. The values for  $z$  appeared in the partition function for  $N_2O_4$ , equation (3), at constant temperature are calculated from equation (9) at various values of  $V$ .

Then, the negative slope of the common tangential line between the liquid region (at the vicinity of liquid minimum) and the gaseous region will give the vapor pressure at the given temperature. And the tangential point at the liquid region will give the molar volume at the temperature. Good agreements between calculated values and literature values are observed as shown in Tables 1 and 2.

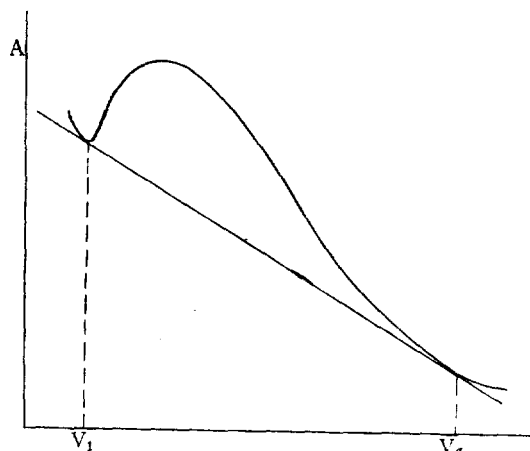


Figure 1. Plot for Helmholtz Free Energy vs Volume

Table 1. Molar Volume and Vapor Pressure for  $N_2O$

$T^\circ K$	V c. c. /mole			P atm.		
	Calc.	Obsd <sup>14</sup>	$\Delta\%$	Calc.	Obsd <sup>14</sup>	$\Delta\%$
182.25(T. P.)	35.71	(35.79)	-0.22	0.919	0.920	0.11
183.65(B. P.)	35.90	35.90	0.00	1.000	1.000	0.00
203.15	37.86	37.62	0.64	2.83	2.81	0.71
223.15	40.03	39.73	0.76	6.65	6.60	0.76
243.15	42.68	42.33	0.83	13.4	13.3	0.75
263.15	46.15	45.96	0.41	23.9	24.0	0.42

Table 2. Molar Volume and Vapor Pressure for  $N_2O_4$

$T^\circ K$	V c. c. /mole			P atm.		
	Calc.	Obsd <sup>18</sup>	$\Delta\%$	Calc.	Obsd <sup>11</sup>	$\Delta\%$
261.95(T. P.)	60.82	(60.82)	0.00	0.1845	0.1839	0.38
273.15	62.44	61.76	1.10	0.3413	0.3453	-1.12
283.15	63.62	62.64	1.56	0.5676	0.5822	-2.51
294.30(B. P.)	64.80	63.63	1.84	0.9660	1.000	-3.40
303.15	65.74	—	—	1.436	1.488 <sup>19</sup>	3.49
313.15	66.77	—	—	2.201	2.273 <sup>19</sup>	-3.17

### B. Entropies of Vaporization

The entropy is expressed as

$$S = k \ln F + kT(d \ln F / dT) \quad (12)$$

From the equation (12),  $S_g$ , the entropy at the gaseous state, and  $S_l$ , the entropy at the liquid state, can be calculated. Then, the entropy of vaporization can be obtained from the expression

$$\Delta S_{vap} = S_g - S_l \quad (13)$$

The calculated values are tabulated in Table 3.

**Table 3. Entropies of Vaporization,  $\Delta S_{vap}$ , cal/deg. For  $N_2O$**

$T^\circ K$	Calc.	Obsd. <sup>16</sup>	$\Delta\%$
182.25(T. P.)	21.8	(21.9)	-0.46
183.65(B. P.)	21.6	(21.6)	0.00
203.15	18.3	(18.1)	1.1
223.15	15.6	(15.2)	2.6
243.15	13.2	(12.7)	3.9
263.15	10.8	(10.6)	1.9

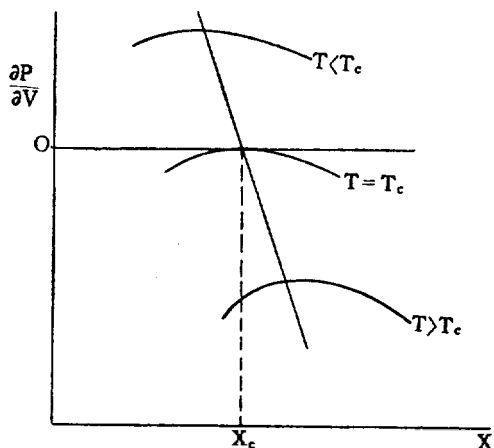
These values are obtained from the plot based on literature values.

For  $N_2O_4$  at boiling point, 294.30°K

Calc.	Obsd. <sup>12</sup>	$\Delta\%$
31.01	30.96	0.16

### C. Critical Point Properties

As shown in Figure 2, when values for  $(dP/dV)_T$  is plotted against  $X$  values; a maximum of the curve is found at  $(dP/dV)_T=0$  if  $T=T_c$ , whereas a maximum appears in the region of  $(dP/dV)_T>0$  if  $T<T_c$ , and in the region of  $(dP/dV)_T<0$  if  $T>T_c$ . Accordingly, the critical temperature is determined by plotting the calculated value of  $(dP/dV)_T$  against  $X$  at various temperatures to find the temperature at which the maximum appears at  $(dP/dV)_T=0$ . At this temperature the critical conditions,  $(dP/dV)_T=0$  and



**Figure 2. Isotherms of  $(dP/dV)_T$  Near the Critical Point**

$(d^2P/dV^2)_T=0$ , are automatically satisfied. The critical volume is determined from  $X_c$  at which  $(dP/dV)_T=0$ ,  $V_c$  being equal to  $X_c V_s$ . The critical pressure is calculated from equation (6) by using  $T_c$  and  $V_c$  obtained above. The calculated values for the critical point properties are shown in Table 4.

**Table 4. Critical Point Properties**

For  $N_2O_4$

	$T_c^\circ K$	$V_c$ c. c./mole	$P_c$ atm.
Calc.	326.20	104.3	93.2
Obsd. <sup>15</sup>	309.65	96.32	71.7
$\Delta\%$	5.3	8.3	30.0

For  $N_2O_4$

	$T_c^\circ K$	$V_c$ c. c./mole	$P_c$ atm.
Calc.	447.0	161.0	152.3
Obsd. <sup>20</sup>	431.4	165.3	99.96
$\Delta\%$	3.62	-2.60	52.4

### D. Degree of Dissociation

As explained in the previous section,  $W-A$ , the degree of dissociation of  $N_2O_4$  in gaseous state,  $z_g$ , can be calculated from equation (9), introducing the values of  $V_g$  for  $V$  in the expression at the given temperature. The degree of dissociation of  $N_2O_4$  in liquid state can be obtained by multiplying the value for  $z$ , the value calculated from equation (9) using the liquid volume for  $V$  in the expression, by  $(V-V_s)/V$ , the fraction of gas-like molecules in the liquid. The degrees of dissociation in gaseous and liquid states, thus calculated, are shown in Tables 5 and 6, respectively.

**Table 5. Degree of Dissociation in Gaseous Phase**

$T^\circ K$	Calculated ( $Z_g \times 10^2$ )	Observed <sup>13</sup> ( $Z_g \times 10^2$ )
291.95(T. P.)	8.698	8.737
273.15	11.201	11.000
283.15	13.771	13.179
294.30(B. P.)	16.998	15.888
303.15	19.673	—
313.15	23.101	—

### Discussion

As mentioned above, the difference between the boiling point and the triple point of  $N_2O$  is extremely

Table 6. Degree of Dissociation in Liquid Phase

T°K	Calculated ( $Z_1 \times 10^3$ )	Observed <sup>18</sup> ( $Z_1 \times 10^3$ )
261.95(T. P.)	0.50	0.18
273.15	0.87	0.36
283.15	1.42	0.66
294.30(B. P.)	2.39	1.19
303.15	3.54	—
313.15	5.29	—

small, 1.4 degree centigrade, and the vapor pressure of  $N_2O$  at the melting point is extremely high, 0.92 atm. When  $N_2O$  solid melts, the expansion of volume is unusually high, about 27% increase, and the entropy of fusion of  $N_2O$  is very high, 8.6 e.u. These unusual qualities of liquid  $N_2O$  are successfully verified by the theoretical calculations of liquid  $N_2O$  according to the transient state theory of the significant liquid structure. Besides having the similar unusual qualities to  $N_2O$ ,  $N_2O_4$  molecules dissociate in gaseous and liquid phases. However, the degree of dissociation in liquid phase is in the range of several hundredth of that in gaseous phase. It is experimentally proved that  $N_2O_4$  molecules do not dissociate in solid state. And from the fact that the energy difference between solid state and transient state is very small, about 1,000 cal./mole, compared with the dissociation energy of  $N_2O_4$  molecules, 13,186 cal./mole, it can be stated that the molecules in the transient state do not dissociate either. Accordingly, as it is done in this work, it is reasonable assumption that the molecules of  $N_2O_4$  do not dissociate in either transient or solid state.

As shown in the theoretical calculations, the abnormal liquid properties of  $N_2O_4$  are also successfully treated by the transient state theory of the significant liquid structure.

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