

# Passivation of Al<sub>2</sub>O<sub>3</sub>-based Refractories by Air Plasma Spray Coatings of Y<sub>2</sub>O<sub>3</sub>

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## 1. Introduction

As the starting process of pyroprocessing, head-end process deals with the conversion of spent fuel into suitable feed form of uranium oxides for following electrolytic reduction process. Depending on its physical form, the fabrication process of feed materials may (or may not) include high temperature treatment. Voloxidation and sintering correspond to the high temperature processes in the preparation of porous pellet, which is one of the promising feed materials [1-3]. During the heat treatment at high enough, radioactive fission products such as Cesium (Cs) and Iodine (I) are released from the spent fuel of uranium oxides. Considering that the fission products are extremely harmful to human body, their emission to atmosphere must be strictly minimized by capturing them using appropriate filters. In other words, the released off gas should be collected at the filters connected to a furnace where the heat treatment of the spent fuel takes place.

The off-gas escapes from the spent fuel and move to the filters along with atmospheric gas flow in heating furnace, contacting inner surfaces of the refractory materials in the furnace. Most of the refractories usually contain alumina (Al<sub>2</sub>O<sub>3</sub>) and silica (SiO<sub>2</sub>) due to their excellent heat tolerance. However, those likely to form mullite (Al<sub>6</sub>Si<sub>2</sub>O<sub>13</sub>) phase during heating. The mullite is well known material for capturing the Cs vapor by the formation of pollucite (CsAlSi<sub>2</sub>O<sub>6</sub>) phase. Considering this, the use of those general refractories would be a critical problem. Apart from developing 'brand-new' refractory materials, which is extremely challenging, the coatings of inert materials on the surface of refractories can be a possible detour to suppress the reaction with CS. The present study explores the possible way to prevent the capture reaction of Cs with refractories by Air Plasma Spray (APS) coating of pure Y<sub>2</sub>O<sub>3</sub>. Both confirmation on the material and optimization of the coating process in this study

would provide the applicability of this material and method for successful head-end process, especially for capturing the off-gas in pyroprocessing.

## 2. Experimental

The commercial insulating fire bricks with a composition of 99.3Al<sub>2</sub>O<sub>3</sub>-0.4SiO<sub>2</sub>-0.1Fe<sub>2</sub>O<sub>3</sub> (wt. %) and high purity Y<sub>2</sub>O<sub>3</sub> powder (> 99.9 %) were prepared for the substrate and coating material for APS coating in this experiment. The confirmation on the reactivity of the Y<sub>2</sub>O<sub>3</sub> with Cs using Cs<sub>2</sub>CO<sub>3</sub> powder, which is decomposes into Cs<sub>2</sub>O and CO<sub>2</sub> after melting at about 610°C. The spray coating was conducted with the same conditions except the thickness of Y<sub>2</sub>O<sub>3</sub> coating layer then optimized the thickness of coating layer as 500 μm. To enhance adhesion without delamination, the coated samples were heat-treated at 1520°C for 10 h in air atmosphere with heating and cooling rate of 2°C/min. For the reaction experiment between Cs and refractory material, Cs<sub>2</sub>CO<sub>3</sub> powder was used as Cs source. 0.05 g of Cs<sub>2</sub>CO<sub>3</sub> powder was dispersed on the surface of coated layer and heat treated at 1450°C for 1 h in 4% H<sub>2</sub>-Ar flow (0.1 liter/min). The characterization was conducted by SEM/EDS and XRD before and after the heat treatment.

## 3. Results and Discussion

Fig. 1 shows the physical properties of the commercial insulating brick. It consists of pure Al<sub>2</sub>O<sub>3</sub> particles ranging from few to few tens of microns as shown in the SEM and SEM/EDS results. Their particle shapes varied from rounded to elongated. The XRD pattern indicates its single phase of Al<sub>2</sub>O<sub>3</sub>. To exclude the possibility of mullite phase is the reason why the brick of high purity without Si was used in this experiment.

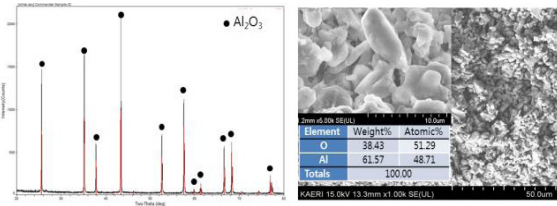


Fig. 1. XRD (left) and SEM/EDS results of the brick.

Fig. 2 shows SEM micrographs of the cross section and the surface of  $Y_2O_3$  coated samples after heat treatment at  $1520^\circ C$  for 10 h in air. Clear distinction was made by different porosity in the observations. It is noting that the substrate brick was overspread with coated  $Y_2O_3$  layer. From the micrograph showing the surface of the coated layer, well-organized small  $Y_2O_3$  grains were observed. Severe roughness with many pores was also observed at the surface which is largely due to the original surface roughness of the surface of brick substrate. However, it did not mean the exposure of the substrate brick to atmosphere.

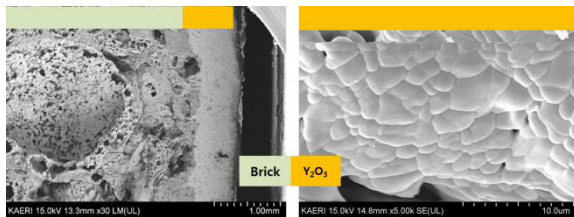


Fig. 2. SEM micrographs showing a cross section (left) and surface (right) of the APS coated samples.

The spatial chemical composition across the interface was observed by SEM/EDS line scan as shown in Fig. 3. It shows other distinction of the substrate and coated layer than the morphology shown in Fig. 2. The brick substrate and coated layer were divided by its composition with other major cation element, Al and Y, respectively. In the line scan result, some of Al was also observed at the coated  $Y_2O_3$  layer. In contrast, from the spot analysis indicated that the coated layer was homogeneous  $Y_2O_3$  single phase, indicating the inactivation of the coated layer based on that there was no reaction between the  $Y_2O_3$  and  $Cs_2CO_3$  powder.

Fig. 4 shows the photographs of cube-shaped samples before and after heat treatment at  $1450^\circ C$  for 1 h in 4%  $H_2$ -Ar, which is similar with real sintering process of the porous pellet fabrication.

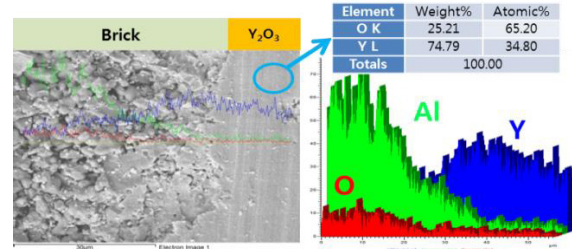


Fig. 3. SEM/EDS line scan result of across the interface between brick and coated  $Y_2O_3$  layer.

The heat treatment was accompanied by addition of  $Cs_2CO_3$  powder on the surface of the coated  $Y_2O_3$  layer. After the heat treatment, the coated layer was  $Y_2O_3$  single phase as shown in the XRD pattern as it was before the heat treatment. This clearly indicates that there would be no chemical reaction of the coated  $Y_2O_3$  layer with Cs.

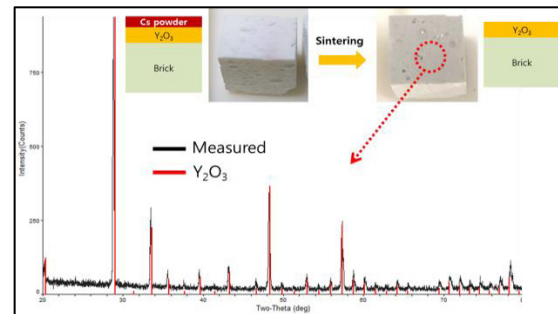


Fig. 4. Photographs of the samples before and after heat treatment (inset) and XRD pattern of the coated  $Y_2O_3$  layer after heat treatment.

## 4. Conclusions

The coated  $Y_2O_3$  layer on a commercial fire brick maintained its physical/chemical integrity with the presence of Cs during high temperature heat treatment. This provides the applicability of the APS coating of  $Y_2O_3$  to the refractories for off-gas treatment system in pyroprocessing.

## REFERENCES

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- [2] S.-C. Jeon, J.-W. Lee, J.-H. Lee, S.-J. Kang, K.-Y. Lee, Y.-Z. Cho, D.-H. Ahn, and K.-C. Song, "Fabrication of  $UO_2$  Porous Pellets on a Scale of 30 kg-U/Batch at the PRIDE Facility," Adv. Mater. Sci. Eng., 2015 (2015) 1-8.