

모델 불확실성과 외란이 있는 이동 로봇을 위한 적응 슬라이딩 모드 제어

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Adaptive Sliding Mode Control for Nonholonomic Mobile Robots with Model Uncertainty and External Disturbance

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Abstract - This paper proposes an adaptive sliding mode control method for trajectory tracking of nonholonomic mobile robots with model uncertainties and external disturbances. The kinematic model represented by polar coordinates are considered to design a robust control system. Wavelet neural networks (WNNs) are employed to approximate arbitrary model uncertainties in dynamics of the mobile robot. From the Lyapunov stability theory, we derive tuning algorithms for all weights of WNNs and prove that all signals of an adaptive closed-loop system are uniformly ultimately bounded.

1. Introduction

The control of a mobile robot with nonholonomic constraints has attracted much attention because it is useful in many applications such as transportation, exploration, military issue, and so on. The robust control problem out of them has been steadily considered for mobile robots with uncertainties and external disturbances.

The sliding mode control (SMC) technique, in particular, has been used for a robust control of uncertain mobile robots because of its fast response, good transient performance, and robustness with regard to parameter variations [1],[2],[3]. Recently, Yang and Kim [4] applied the SMC technique to the trajectory tracking problem of nonholonomic mobile robots in polar coordinates. Chwa proposed a position controller and a heading direction controller using the SMC technique for nonholonomic mobile robots in [5]. Though he considered the mobile robot with kinematics in polar coordinates as treated in [4], he overcame constraints on the heading angle of the mobile robot and the angle coordinate in [4]. However, in [4] and [5], the model uncertainties were not treated and only external disturbances in the dynamics of the system were done. These points motivate us to design an upgraded controller capable of overcoming model uncertainties and external disturbances of mobile robots. Accordingly, we propose an adaptive SMC (ASMC) system using neural networks for trajectory tracking of nonholonomic mobile robots with model uncertainties and external disturbances. In the proposed control system, the sliding surfaces presented in [5] are used. In this paper, we prove from the Lyapunov stability theory that all signals of the adaptive closed-loop system using the WNN are uniformly ultimately bounded. Adaptation laws for all weights of WNNs are derived from this procedure.

2. Model of Mobile Robots With Nonholonomic Constraints

2.1 Dynamics of Mobile Robots With Model Uncertainty

The dynamic equation of the mobile robot system with nonholonomic constraints can be described by Euler-Lagrange formulation [4] as

$$M(q)\ddot{q} + V(q, \dot{q})\dot{q} + G(q) = B(q)\tau - A^T(q)\lambda, \quad (1)$$

where $M(q) \in R^{n \times 1}$ is a symmetric, positive definite inertia matrix, $V(q, \dot{q}) \in R^{n \times n}$ is the centripetal and Coriolis matrix, $G(q) \in R^{n \times 1}$ is the gravitational vector, $B(q) \in R^{n \times r}$ is an input transformation matrix, $\tau \in R^{r \times 1}$ is a control input vector, and $\lambda \in R^{m \times 1}$ is a vector of constraint forces. By using $\ddot{q} = S\dot{z} + \dot{S}z$, we can rewrite the dynamic equation as

$$H(q)\dot{z} + F(q, z) = \tau, \quad (2)$$

where $H(q) = (S^T(q)B(q))^{-1}S^T(q)M(q)S(q)$,

$$F(q, z) = (S^T(q)B(q))^{-1}S^T(q)(M(q)\dot{S}(q) + V(q, \dot{q})S(q))z.$$

If model uncertainties and external disturbances influence the mobile robot, the actual dynamics equation of the mobile robot can be rewritten as

$$[H_0(q) + \text{TRIANGLE}H(q)]\dot{z} + [F_0(q, z) + \text{TRIANGLE}F(q, z)] + \tau_d = \tau \quad (3)$$

where $H_0(q)$ and $F_0(q, z)$ denote known smooth nominal functions, $\text{TRIANGLE}H(q)$ and $\text{TRIANGLE}F(q, z)$ denote unknown internal uncertainties including parametric and nonparametric uncertainties, τ_d denotes external disturbances, and $\tau = [\tau_l \ \tau_r]^T$ is a torque vector applied to the left and right driving wheels. To divide nominal values and uncertainties, (3) is represented as

$$H_0(q)\dot{z} + F_0(q, z) + \Gamma(q, z) + \tau_d = \tau, \quad (4)$$

where $\Gamma(q, z) = \text{TRIANGLE}H(q)\dot{z} + \text{TRIANGLE}F(q, z)$ denotes the uncertainty term.

Assumption 1 : The matrix $H_0(q)$ is bounded and invertible.

Assumption 2: $\tau_d = H_0 f$, $f = [f_1 \ f_2]^T$, $|f_i| \leq f_{mi}$, $i = 1, 2$.

2.2 Kinematics of Mobile Robots

It is assumed that the driving wheels of the mobile robot purely roll and do not slip [4]. This nonholonomic constraint can be expressed as $x_c \sin \theta_c - y_c \cos \theta_c = 0$. Then, the kinematic equation $\dot{q}_c = S(q)z$ can be described by

$$\begin{bmatrix} \dot{x}_c \\ \dot{y}_c \\ \dot{\theta}_c \end{bmatrix} = \begin{bmatrix} \cos \theta_c & 0 \\ \sin \theta_c & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} v_c \\ w_c \end{bmatrix}, \quad (5)$$

where x_c and y_c are position variables, θ_c is a heading direction angle. In addition, the kinematic equation in polar coordinates is derived as follows:

$$\begin{bmatrix} \dot{\rho}_c \\ \dot{\phi}_c \\ \dot{\theta}_c \end{bmatrix} = \begin{bmatrix} v_c \cos(\phi_c - \theta_c) \\ -\frac{v_c}{\rho_c} \sin(\phi_c - \theta_c) \\ w_c \end{bmatrix}, \quad (6)$$

where $\rho_c = \sqrt{x_c^2 + y_c^2}$ and $\phi_c = \tan^{-1}(y_c/x_c)$.

3. Adaptive Sliding Mode Control

The objective of trajectory tracking control problem is to design a robust adaptive controller so that the mobile robot can track the reference trajectory $q_r = [\rho_r \ \phi_r \ \theta_r]^T$ represented in polar coordinates as follows:

$$\begin{bmatrix} \dot{\rho}_r \\ \dot{\phi}_r \\ \dot{\theta}_r \end{bmatrix} = \begin{bmatrix} v_r \cos(\phi_r - \theta_r) \\ -\frac{v_r}{\rho_r} \sin(\phi_r - \theta_r) \\ w_r \end{bmatrix}, \quad (7)$$

where $z_r = [v_r \ w_r]^T$; ρ_r, ϕ_r and θ_r are piecewise smooth and time-varying functions.

We use the sliding surface $S = [s_1 \ s_2]^T$ expressed as follows [5]:

$$S = M(\rho_c, \phi_c, \theta_c) \begin{bmatrix} s_\rho + k_0 \text{sgn}(\rho_c) s_\theta \text{RIGHT} s_\phi + \frac{k_0}{\rho_c} \text{sgn}(\phi_c) s_\theta \text{RIGHT} s_\theta \\ \end{bmatrix}, \quad (8)$$

where $k_0 > 1$, $s_\rho = \dot{\rho}_c + k_1 \rho_c$, $s_\phi = \dot{\phi}_c + k_2 \phi_c$, $s_\theta = \dot{\theta}_c + k_3 \theta_c$, in which $\rho_e = \rho_c - \rho_r$, $\phi_e = \phi_c - \phi_r$, and $\theta_e = \theta_c - \theta_r$, k_1, k_2 , and k_3 are positive constants, and

$$M(\rho_c, \phi_c, \theta_c) = \begin{bmatrix} \cos(\phi_c - \theta_c) & -\rho_c \sin(\phi_c - \theta_c) & 0 \\ \sin(\phi_c - \theta_c) & \rho_c \cos(\phi_c - \theta_c) & 1 \end{bmatrix}, \quad (9)$$

By using the computed-torque method, we can choose a torque control input composed of the nominal values $H_0(q)$ and $F_0(q, z)$ as

$$\tau = H_0(q) \dot{z}_r + F_0(q, z) + H_0(q) u, \quad (10)$$

where $u = [u_1 \ u_2]^T$ is a control law. Substituting (10) into (4), we have

$$\dot{z} - g(\bar{x}) + f = \dot{z}_r + u, \quad (11)$$

where $g(\bar{x}) = -H_0^{-1}(q) \Gamma(q, z)$ and $\bar{x} = [q^T \ z^T]^T$.

In this paper, we propose the control law u using the WNNs which stabilizes the sliding surface (8) as

$$u = -\hat{g}(\bar{x}) \hat{W} - Qs - P \text{sgn}(s) + \Psi(q, q), \quad (12)$$

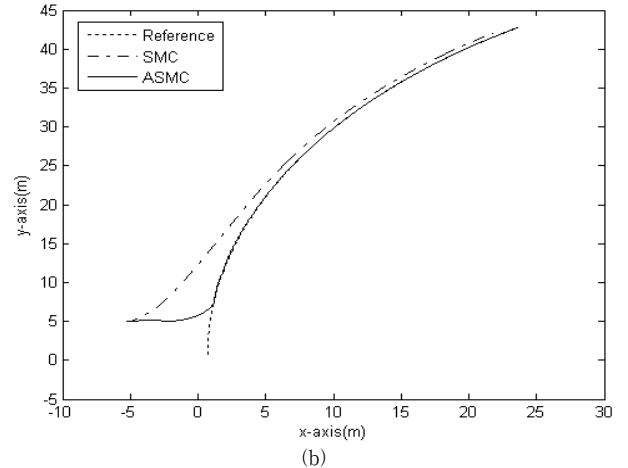
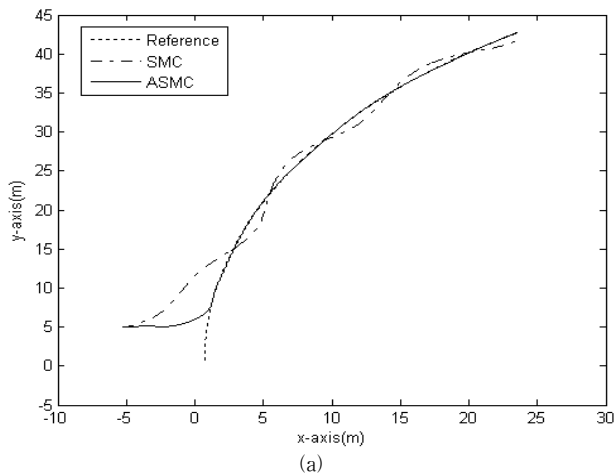
where $\hat{g}(\cdot) = [\hat{g}_1 \ \hat{g}_2]^T$ is an approximation of the uncertainty term $g(\bar{x})$, $Q = \text{diag}[q_1, q_2] > 0$, $P = \text{diag}[f_{m1}, f_{m2}] > 0$.

4. Simulations

In this section, simulations for the tracking control of the wheeled-mobile robot are implemented to demonstrate the validity of the proposed control method. In addition, we compare the performance of the proposed control approach with that of the SMC approach presented in [5] to verify the robustness of the ASMC system using WNNs. Table 1 shows the uncertain system parameters of the mobile robot with model uncertainties where it is assumed that the nominal values are only known. The radius and width for the mobile robot are chosen as $r=0.05\text{m}$ and $R=0.25\text{m}$. In addition, the constant external disturbance and the time-varying external disturbance given by $\tau_d = [0.5 \ 2]^T$ and $\tau_d = [2\cos(2t) \ 2\sin(2t)]^T$, respectively, are assumed to influence the nonholonomic mobile robot model. The initial locations for the mobile robot and the reference trajectory are given by $[\rho_r, \phi_r, \theta_r] = [1, \pi/4, 1.46]$ and $[\rho_c, \phi_c, \theta_c] = [7.3, 2.38, -0.38]$. To generate a curve, the reference velocity $[v_r \ w_r] = [5 \ -0.1]$ is chosen. The controller parameters for the WNN-based ASMC system and the SMC system are chosen as $k_0 = 1.1$, $k_1 = k_2 = 2$, $k_3 = 0.002$, $q_1 = q_2 = 1$, $p_1 = p_2 = 2.5$, $\sigma = 0.1$, and $\lambda_1 = \lambda_2 = 0.003$.

<Table 1> Simulation parameters for mobile robot

Condition	Nominal	Actual
mass $m(\text{kg})$	8	12
inertia $I(\text{kg}\cdot\text{m}^2)$	5	2.5



<Fig. 1> Trajectory tracking result of the proposed controller. (a) x-y plot under the constant external disturbance. (b) x-y plot under the time varying external disturbance.

Fig. 1 compares the tracking results of the proposed control system and the SMC system which represents a curve. In Fig. 1 (a) and (b), the control results under the constant external disturbances and the time-varying external disturbances are shown respectively. In Fig. 1, note that the performance of the proposed approach is better than that of the SMC approach proposed in [5] under the effects of the model uncertainties, and the constant or the time-varying external disturbances.

5. Conclusion

In this paper, the adaptive sliding mode controller for a nonholonomic wheeled mobile robot with model uncertainties and external disturbances has been proposed. To approximate the uncertainty terms, the WNNs have been employed and all their weights have been trained online by tuning laws derived from the Lyapunov stability theory. In addition, we have proved that all signals in the adaptive closed-loop system are uniformly ultimately bounded. Finally, from the simulation results for the mobile robot, it have been shown that the proposed controller has better tracking performance than the previous SMC approach based on kinematics in polar coordinates under the model uncertainties and the external disturbances.

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