

PE19) Treatment of Hydrogen Sulfide in Waste Gas Stream by Polyurethane Biotrickling Filter

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1. INTRODUCTION

Hydrogen sulfide is nuisance odor smelling like a rotten egg, released to the atmosphere as a by-product of industrial process including sour gas flaring, wastewater treatment and pulp and paper manufacturing. The biological removal of hydrogen sulfide has been studied by a number of researchers, Seongyup Kim, Marc A.Deshusses (2005) suggested that trickling rate was significant effect on high gas velocity, and addition of some sulfur containing substrates, such as thiosulfate had an improved effect on removal of hydrogen sulfide. Investigation of microbial diversity in system is important, due to changing operational parameters, such as pH. At the neutral pH the mixed cultures grown had intrinsically effective. While in some studies suggested that even at low pH removal of hydrogen sulfide is less affected due to acidophilic characteristic of inoculates. Yaomin Jin et al., (2005) studied the autotrophic degradation of sulfide in biotrickling filter signifying influence of CO₂, pH and flow pattern on the removal of hydrogen sulfide. They suggested that neutral pH was effective for the autotrophic degradation with an elimination capacity of 31.12g H₂S/m³h; removal efficiency 97%. Complete removal of hydrogen sulfide were at 11s EBRT. David Gabriel, Marc A.Deshusses (2003) studied hydrogen sulfide removal in converted biotrickling filter, and suggested that even at low EBRT as 1.6 95% of H₂S were removed for sustained inlet as 30 ppm. 90% removal observed at 2.2s with 60ppm of inlet concentration.

In the present study a biotrickling filter was packed with polyurethane foam as support used to treat H₂S-polluted air, and to determine the operating parameters that optimize the performance of system.

2. MATERIALS AND METHODS

2.1 Experimental set-up

Two identical laboratory set-ups were applied for the removal of hydrogen sulfide. Both of columns were inoculated sulfur oxidizing bacteria. One reactor was running with deionized water, the other one were operated with secondary effluent water from waste water treatment plant (Yong-in city, Korea). Biotrickling filter construction and operating conditions are shown in Table 1 and Figure 1. H₂S was introduced by reaction of HCl and solution of Na₂S. H₂S concentrations ranging from 0 to 200 ppm were obtained by changing the Na₂S concentration and/or the dripping rate.

2.2 Microorganisms and cultivation

Sulfide oxidizing bacteria were enriched in initially autoclaved thiosulfate media at 150rpm 28°C. The composition of the liquid medium used was (in g/L): KH₂PO₄, 2; K₂HPO₄, 2; NH₄Cl, 0.4; MgCl₂·6H₂O, 0.2; FeSO₄·7H₂O, 0.01; Na₂S₂O₃·5H₂O, 8 and yeast 1. Autoclaved polyurethane foams were introduced to the flask with enriched microorganisms and also incubated at same condition. After 7 days of incubation foams were transferred to columns and drained liquid media for 24hours.

Table 1. Operating condition

Design	
Bed height and internal diameter	30×10 cm ²
Bed volume	3L
Packing	Polyurethane foam (90% porous)
Recycle liquid volume	2L
Gas/liquid flow	Counter current
pH control	Manual addition of 0.3M NaOH; 1M HCL
Operation	
Gas flow rate (EBRT)	5~8L h ⁻¹ (36~10s)
Mass loading	6~43 g m ⁻³ h ⁻¹
H ₂ S inlet concentration	Variable, up to 200 ppmv
Recycle liquid pH	7.0
Recycle liquid rate	250 ml/in
Nutrient addition	250ml/day

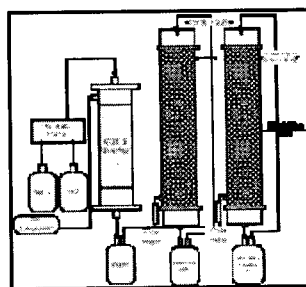


Fig. 1. Biotrickling filter.

2.3 Analytical methods

H₂S were measured by Gastec and multiRae portable gas analyzer; t⁰ were determined by thermometer and pH by pH meter. Pressure drop were measured by digital manometer. Sulfide concentration in liquid determined by methylene blue method using s auto analyzer AA3 (Bran Luebbe, Germany) and CFU by serial dilution method. Sulfate ions measured by ion chromatography (Waters).

3. RESULTS AND DISCUSSIONS

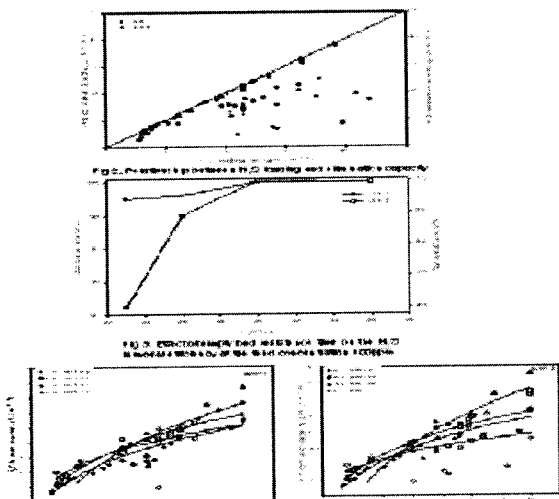


Fig. 4. Estimation capacity as a function of inlet concentration of the different gas flow rates

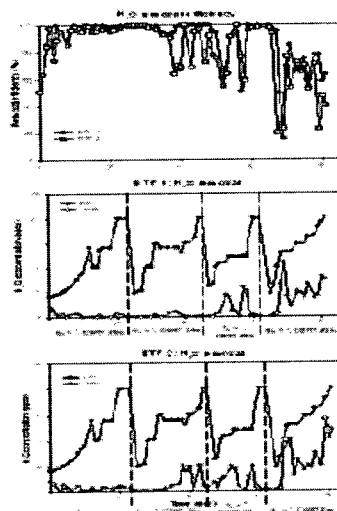


Fig. 5. H₂S removal efficiency in biotrickling filter

3.1 Gas analyses

At the start up in both systems inlet concentrations were maintained near 50ppm. After 7 days of start up removal efficiency in both reactors were 100%. When the concentration increased to 100 ppm, removal efficiency in both reactors maintained above 98%. For BTF 1, the removal efficiency was higher than BTF 2 even at the high concentration as 200ppm. With the increasing gas flow rate the removal efficiency were stable at a low concentrations but at high concentrations it decreased to 60%. In BTF 2 the nutrient addition were stopped after 20 days and only replaced

trickling water with 500ml/day secondary effluent water. At day 35, the removal efficiency decreased to 62%, which can be explained that nutrients which were fed previously all consumed by microorganisms. Although the secondary effluent water has buffering effect but it's needs also constant nutrient addition.

3.2 H₂S removal efficiency

Increasing H₂S concentrations were fed to the biotrickling filter to establish operating criteria necessary to scale-up the biotrickling filter, the relationship between the inlet loading of H₂S and the elimination capacity was estimated. The results are reported in Fig. 2. The elimination capacity is defined as the amount of pollutant degraded per unit of time, normalized to the volume of packed bed. As shown in Fig. 2, the critical loading (i.e complete removal capacity) was determined as 32.88 g H₂Sm⁻³ reactor h⁻¹ with 100% removal efficiency for each biotrickling filters.

3.3 Effect of EBRT/ gas flow rate on the removal of H₂S

The effect of empty bed residence time were studied at gas feed concentration 100 ppm, with a different gas flow rate. The removal efficiency reached above 95% removal at 36s (EBRT). When it decreased to 23s the removal efficiency was still high at low inlet concentrations (~100ppm) but at a high inlet concentration removal efficiency decreased to 60% and 20% for BTF 1 and BTF 2, respectively. The reduction in removal efficiency can be explained by the slow diffusion of gas into liquid phase. After sometime the removal efficiency increases again, which means the microorganisms adapts to the new environment. The optimum EBRT for both reactors obtained at 26s .

In Fig. 4, the measured trickling filter's elimination capacity is plotted for different inlet H₂S concentrations at a constant liquid flow rate of 250ml/min and at gas flow rates of 5, 6, 7 and 8L min⁻¹ corresponding to EBRT of 36, 30, 26 and 23 s. From this figure, it can be observed that the elimination capacity increased when increasing the gas flow rate over all the concentration range studied. At 7L min⁻¹ a maximum elimination capacity of 38.36 g H₂ Sm⁻³ h⁻¹ for BTF 1 and 37.78 g H₂S m⁻³h⁻¹ for BTF 2 was obtained.

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