Sliding Mode Active Queue Management Algorithm

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Abstract: In this paper, a robust Sliding Mode Variable Structure (SMVS) controller is designed for Active Queue Management (AQM). This type of controller is insensitive to noise and variance of the parameters, thus it is suitable to time varying network systems. Simulation results conform the robust performance of SMVS controller against the disturbance. At the same time, a complete comparison between SMVS and PI controllers is made. The conclusion is that both transient and steady state performance of SMVS controller is better than that of PI one.

Keywords: Active queue management, robust control, sliding mode control

1. INTRODUCTION

Active Queue Management (AQM), as one class of packet dropping/marking mechanism in the router queue, has been recently proposed to support the end-to-end congestion control in the Internet [1]. It has been a very active research area in the Internet community. The goals of AQM are (1) reduce the average length of queue in routers and thereby decrease the end-to-end delay experimented by packets, and (2) ensure the network resources to be used efficiently by reducing the packet loss that occurs when queues overflow. AQM highlights the tradeoff between delay and throughput. By keeping the average queue size small, AQM will have the ability to provide greater capacity to accommodate nature-occurring burst without dropping packets, at the same time, reduce the delays seen by flow, this is very particularly important for real-time interactive applications. RED [2] was originally proposed to achieve fairness among sources with different burst attributes and to control queue length, which just meets the requirements of AQM. However, many subsequent studies verified that RED is unstable and too sensitive to parameter configuration, and tuning of RED has been proved to be a difficult job [3,4].

The variable structure controller is known to be robust to parameter uncertainty and external disturbance because of the sliding motion on a predefined hyperplane [5,6]. The most distinguishing property of variable structure control systems (VSCS) is that the closed loop system is completely insensitive to system uncertainties and external disturbances. A great deal of efforts has been put on establishing both theoretical VSCS concepts and practical applications [7,8,9,10].

The intuition and heuristic design is not always scientific and reasonable under any conditions. Of course, since Internet is a rather complex huge system, it is very difficult to have a full-scale and systematic comprehension, but importance has been considerably noted. The mathematical modeling of the Internet is the first step to have an in-depth understanding, and the algorithms designed based on the rational model should be more reliable than one original from intuition. In some of the references, the nonlinear dynamic model for TCP flow control has been utilized and some controllers like PI and Adaptive Virtual Queue Algorithm have been designed for that [11,12,13,14,15]. Although PI controller successfully related some limitations of RED, for instance, the queue length and dropping/marking probability are decoupled, whenever the queue length can be easily controlled to the desired value; the system has relatively high stability margin. The shortcomings

of PI controller are also obvious. The modification of probability excessively depends on buffer size. As a result, for small buffer the system exhibits sluggishness. Secondly, for small reference queue length, the system tends to performance poorly, which is unfavorable to achieve the goal of AQM because small queue length implies small queue waiting delay. Thirdly, the status of actual network is rapidly changeable, so we believe that it is problematic and unrealistic, at least inaccurate, to take the network as a linear and constant system just like the designing of PI controller. Affirmatively, the algorithm based on this assumption should have limited validity, such as inability against disturbance or noise. We need more robust controller to adapt complex and mutable network environment, which will be our motivation and aim in this study. In the paper, we will apply one of the advanced robust control theory, variable structure sliding mode control, to design the AQM controller, and expect it to have the perfect performance and be better suited for AQM than PI controller.

2. TCP FLOW CONTROL MODEL

In [11], a nonlinear dynamic model for TCP flow control has been developed based on fluid-flow theory. This model can be stated as follows

$$\begin{cases} \frac{dW(t)}{dt} = \frac{1}{R(t)} - \frac{W(t)W(t - R(t))}{2R(t)} p(t - R(t)) \\ \frac{dq(t)}{dt} = \frac{N(t)}{R(t)} W(t) - C(t) \end{cases}$$
(1)

The above nonlinear and time-varying system was approximated as a linear constant system by small-signal linearization about an operating point [16] (Fig. 1). In the block diagram, C(s) and G(s) are the controller and the plant, respectively. The meaning of parameters presented in Fig. 1 are as following

$$K(t) = \frac{\left[R(t)C(t)\right]^3}{\left[2N(t)\right]^2}, \quad T_1(t) = R(t), \quad T_2(t) = \frac{R^2(t)C(t)}{2N(t)}$$
 (2)

where

C(t): Link capacity (packets/sec) q_o : Queue reference value

N(t): Load factor, i.e., number of active sessions

R(t): Round-trip time (RTT), $R(t) = 2(q(t)/C(t) + T_p)$, T_p is the fixed propagation delay

p(t): Dropping/marking probability

q(t): Instantaneous queue

We believe that the AQM controller designed with the simplified and inaccurate linear constant model should not be optimal, because the actual network is very changeful, the state parameters are hardly kept at a constant value for a long time. Moreover, the equations (1) only take consideration into the fast retransmission and fast recovery, but ignore the timeout mechanism caused by lacking of enough duplicated ACK, which is very usual in burst and short-lived services. In addition to, there are many non-respective UDP flows besides TCP connections in networks; they are also not included in equations (1).

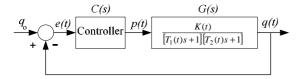


Fig. 1. Block diagram of AQM control system

3. SLIDING MODE CONTROL DESIGN

In this section, we will discuss of SMVS [5,6] controller design for AQM. Firstly, suppose that $x_1 = e$, $x_2 = de/dt$, so the plant depicted in Fig. 1 is described by a second order system as

$$\begin{cases} \frac{dx_1}{dt} = x_2 \\ \frac{dx_2}{dt} = -a_1(t)x_1 - a_2(t)x_2 - b(t) + F(t) \end{cases}$$
 (2)

$$a_{1 \min} = a_1 = a_{1 \max}, a_{2 \min} = a_2 = a_{2 \max}, 0 < b_{\min} = b = b_{\max}$$
 (3)

where

$$\begin{split} a_1(t) &= \frac{1}{T_1(t)T_2(t)}, a_2(t) = \frac{T_1(t) + T_2(t)}{T_1(t)T_2(t)}, b(t) = \frac{K(t)}{T_1(t)T_2(t)} \\ F(t) &= \frac{d^2}{dt^2} q_o + \frac{T_1(t) + T_2(t)}{T_1(t)T_2(t)} \frac{d}{dt} q_o + \frac{1}{T_1(t)T_2(t)} q_o \end{split}$$

F(t) is regarded as the system disturbance. For the convenience of implementation, the following control law is adopted

$$p = x_1.(5)$$

where

$$= \begin{cases} \alpha, & if & x_1 \sigma > 0 \\ \emptyset, & if & x_1 \sigma < 0 \end{cases}$$
 (6)

where σ is the switching function [5,6] as

$$\sigma = cx_1 + x_2 = 0$$
; $c > 0$ is csalar (7)

According to the existence condition for a sliding line:

$$\lim_{\sigma = 0} \sigma \frac{d\sigma}{dt} < 0$$
 [5], we have

$$\alpha = \max_{a_1, a_2, b} \left\{ \frac{1}{b(t)} \left[ca_2(t) - c^2 - a_1(t) \right] \right\}, \ \emptyset = \min_{a_1, a_2, b} \left\{ \frac{1}{b(t)} \left[ca_2(t) - c^2 - a_1(t) \right] \right\}$$
 (8)

Here, if conditions (8) are satisfied, the system must have a sliding regime on the switching line $\sigma=0$, but we are unable to determine if the system could hit this sliding line. The following theorem can answer this question

Theorem [5] A necessary and sufficient condition for hitting to occur in the system consisting with (2) and (5) is that the characteristic equation (9) has no non-negative real roots

$$p^{2} + a_{2 \min} p + a_{1 \min} + \inf_{t} \{ \alpha b(t) \} = 0$$
 (9)

The conservative condition that equation (9) has no non-negative roots is that it has complex roots, so

$$a_{2\min}^2 - 4(a_{1\min} + \inf_t {\alpha b(t)}) < 0$$
 (10)

Namely,

$$\alpha > \frac{a_{2 \min}^2 - 4a_{1 \min}}{4b_{\min}}$$
 (11)

For a variable-parameters and single-input system, the excellent performance could be reached if the conditions (11) and (8) would be satisfied, at the same time, the control law (5) should also be implemented. For the sliding parameter c, only requirement is to keep it more than zero [5]. Theoretically speaking, c should be relatively large since it is larger the transient process is shorter. However, for the network queue management system, c is limited. Taking p(t) into consideration, its meaningful value is in section [0,1], i.e., the control variable is limited. Therefore, we need to choose the combination of constant control and proportional control as new control law

$$p = \begin{cases} x_1, & |x_1| < M \\ x_1| > M \end{cases}$$
 (12)

where

$$= \begin{cases} M, & \sigma > 0 \\ m, & \sigma < 0 \end{cases}$$
 (13)

M and m denote the maximum and minimum of control variable, respectively, i.e., M=1 and m=0. The other parameters are same with (5). For the sake of convenience, suppose that $k=\alpha>0> \emptyset=-k$. Since the control variable is limited, the sliding mode regime in phase space will be restricted in a certain scope, so that the choice of sliding mode parameter c is also restricted, otherwise, the controller variable, queue length, would rush out of the sliding mode regime, and sharp overshoot and great oscillation will occur, which degrades the performance of router.

For the purpose of SMVS controller being suitable for most of dynamic systems, the varying scope of parameters in TCP/AQM system is assumed as following

$$N(t): 1-300, T_p = 0.02 \sec_{q_0}: 0-300 \, packets,$$

$$C(t): 1250 - 7500 \, packet / \sec$$

Therefore,

$$a_{2 \min} = 3.8501, a_{2 \max} = 1250, a_{1 \min} = 0.015, a_{1 \max} = 60000,$$

 $b_{\min} = 2604.2, b_{\max} = 28125000$

Let the sliding mode parameter c = 2. According to the existence condition (8), we have

With the reachable condition of sliding mode (11), we also have

$$\alpha > 0.0015$$

Thus, the controller parameters can be determined as

$$k = \alpha = - \text{ψ} = 0.96$$

So far, a novel AQM algorithm based sliding mode variable structure control theory is obtained.

4. SIMULATION RESULTS

The performance of the proposed controller is simulated using MATLAB. The network topology used for simulation, is depicted in Fig. 2. The only bottleneck link lies between node A and node B. the buffer size of node A is 300 packets, and default size of the packet is 500 bytes. Queue A is SMVS scheme, and the others are Drop Tail. All sources are classed into three groups. The first one includes N_1 greedy sustained

FTP application sources, the second one is composed of N_2 burst HTTP connections, each connection has 10 sessions, and the number of pages per session is 3. The thirds one has N_3 UDP sources, which follow the exponential service model, the idle and burst time are 10000msec and 1000msec, respectively, and the sending rate during "on" duration is 40kbps. We introduced short-lived HTTP flows and non-responsive UDP services into the router in order to generate a more realistic scenario, because it is very important for a perfect AQM scheme to achieve full bandwidth utilization in the presence of noise and disturbance introduced by these flows. The links between node A and all sources have the same capacity and propagation delay pair (L_1, τ_1) . The pair (L_2, τ_2) and (L_3, τ_3) define the parameter of links AB and BC, respectively.

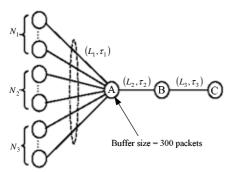


Fig. 2. The simulation network topology

In the first study, we will use the most general network configuration to testify whether the SMVS controller can reach the goals of AQM, and freely control the queue length to stabilize at the arbitrary expected value. Therefore, given that $(L_1,\tau_1)=(10Mbps,15ms)$, $(L_2,\tau_2)=(15Mbps,15ms)$, $(L_3,\tau_3)=(45Mbps,15ms)$. $N_1=270$, $N_2=N_3=0$. Let the expected queue length equal to 75 packets, the instantaneous queue length is depicted in Fig. 3. After a very short regulating process, the queue settles down its stable operating point. RED algorithm is unable to accurately control

the queue length to the desired value. The queue length varies with network loads. The load is heavier the queue length is longer. Attempting to control queue length through decreasing the interval between high and law thresholds, then it is likely to lead queue oscillation. Although PI controller could regulate the queue to the fixed point, the integrated performance needs to be improved, such as the transient process is too long and the fluctuation in steady state is great, for small queue length, which lows the link utilization. The queue evaluation of router A, controlled by PI controller (q_o =75packets), is plotted in Fig. 4. Evidently, PI controller takes the longer time to settle down the reference point. For the sake of clearness, the curves of probability are plotted in Fig. 5.

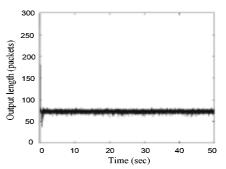


Fig. 3. Queue evaluation (SMVS)

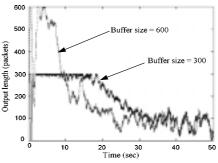


Fig. 4. Queue evaluation (PI)

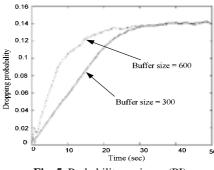


Fig. 5. Probability variance (PI)

We briefly analyze why PI controller is so sluggish. The control law for the PI controller is as follows

 $p(k) = (a-b)(q(k)-q_o) + b(q(k)-q(k-1)) + p(k-1)$ (14) The coefficients a and b are fixed at $1.822e^{-5}$ and $1.816e^{-5}$, respectively, the sampling frequency is 500Hz, the control variable p is accumulative. Because the parameter b is very small, and the sample interval is very short, the negative contribution to p made by the second item in the right can be omitted in initial process, then the positive contribution mainly come from the first item. Assume that q(k) is average value of buffer size and reference queue length in transient process, i.e., p(k) = (300+75)/2 = 188 packets, it is not difficult to calculate the lasting time that p increases from 0 to 0.14:

estimated regulating time
$$\frac{p_o}{(q(k)-q_o)\cdot(a-b)}\cdot\frac{1}{500} = 41.3 \text{ sec}$$

This result is close to the simulation. Considering the requirement of the steady state performance, it is impractical to increase the difference between a and b to speed up the response of PI controller. With the higher sampling frequency, the computation will be significantly exhausted. The only feasible way is to add the buffer size. In order to illustrate this ability, we redo the above simulation with 600 packets buffer size, which the results are also plotted in Figs. 4 and 5. Indeed, the large buffer is able to enhance the responsibility of PI controller, but this ability is limited, moreover it seems to be wasteful. Conversely, the SMVS controller has the ideal performance without any additional regulation mechanism. In order to evaluate the performance in steady state, we calculate the average and the standard deviation of the queue length in steady state. For the convenience of comparison, choose the queue length between 40 and 50 seconds as sample data. In this case, the standard deviation of PI controller (32.3336) is much larger than that of SMVS controller (2.5928). Fig. 6 presents the case of small reference queue length. Except q_o = 15, the other parameters are unchangeable.

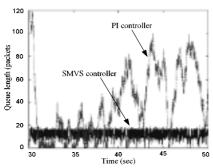


Fig. 6. Small expected queue $(q_o=15)$

In this section, Firstly, let $N_1 = 270$, $N_2 = 400$, $N_3 = 0$, the evaluation of queue size is shown in Fig. 7. As it can be seen, the proposed SMVS controller has better performance than that of PΙ one. Next, given that $N_1 = 270, N_2 = 0, N_3 = 50,$ we further investigate performance against the disturbance caused by the non-responsive UDP flows. Fig. 8 shows the results, obviously, the PI controller is very sensitive to this disturbance, while the SMVS controller operates in a relatively stable state. The queue fluctuation increases with introducing the UDP flows, but the variance is too much smaller comparing with PI one.

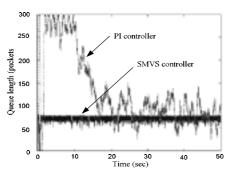


Fig. 7. Queue evaluation (FTP+HTTP)

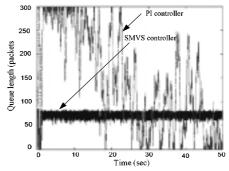


Fig. 8. Queue evaluation (FTP+UDP)

Finally, we evaluate the integrated performance of the SMVS controller using one relatively real scenario, i.e., the number of active flows is changeable, which has 270 FTP flows, 400 HTTP connections and 30 UDP flows. Figs. 9 and 10 show the evaluation of queue controlled by SMVS and PI controllers, respectively. It is clear that the integrated performance of SMVS controller, namely transient and steady state responses is superior to that of PI controller. The SMVS controller is always keeping the queue length at the reference value, even if the network loads abruptly change, but PI controller has the inferior adaptability. In other words, the former is more powerful, robust and adaptive than the later one, which is in the favor of achievement to the objectives of the AQM policy.

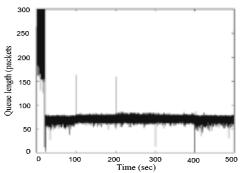


Fig. 9. Queue evaluation (SMVS)

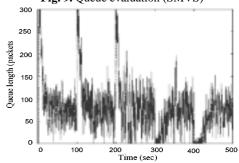


Fig. 10. Queue evaluation (PI)

5. CONCLUSIONS

In this paper, a robust sliding mode variable structure controller was designed for the objective of active queue management. For this purpose, a linearized model of the TCP flow [12,16] was considered. We applied a robust SMVS control strategy to this system because this advanced robust control methodology is insensitive to system dynamic parameters and is capable of being against disturbance and noise, which is very suitable for the mutable network environment. We took a complete comparison between

performance of the proposed SMVS and PI controllers under various scenarios. The conclusion was that the integrated performance of SMVS controller was superior to that of PI one. The SMVS controller was very responsive, stable and robust, especially for the small reference queue system, but its performance was inferior when active TCP sessions were relatively small. Thus, it will be very imperious to design the controller suitable for light load, and then integrate it with SMVS controller using adaptive control technology.

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