

Solid-shell

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Welding analysis with linear solid-shell element

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Key Words : Solid-shell elements(), welding(), shear locking(), thickness locking()

Abstract

In the FE analysis of sheet metal forming, efficient results can be obtained by using shell elements rather than using solid elements. However, shell elements have some limitations to describe three-dimensional material laws. In the recent years, solid-shell element, which has only translational degree of freedom like solid element, has been presented. The assumed nature strain (ANS) and enhanced assumed strain (EAS) methods can be used to remove several solid-shell locking problems. In this paper, ANS method was used for diminish transverse shear locking and EAS method for thickness locking. Using the element, the steel pipe making process from flat plate analyzed effectively, which is including bending and welding.

3

1.

aspect ratio

solid shell
Shell

degenerated shell⁽¹⁾
shell

(transformation plasticity)

, solid

shell

transition

(2)

3

solid translational d.o.f.
solid-shell (3,4)

translational d.o.f. rotational d.o.f.
shell

shell

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3

shell

3

solid

solid-shell

solid-shell

2. Kinematics of Solid-shell

Solid-shell (1,2) shell (4,5)

$$X(\bullet, \xi, \prime) | \frac{1}{2} \Psi(12 \prime) X_u(\bullet, \xi) 2(14 \prime) X_l(\bullet, \xi) \beta \quad (1)$$

$$x(\bullet, \xi, \prime) | \frac{1}{2} \Psi(12 \prime) x_u(\bullet, \xi) 2(14 \prime) x_l(\bullet, \xi) \beta \quad (2)$$

$$X_u, X_l$$

$$\bullet 4 \xi$$

(1,2)

solid-shell

(in-plane)

(1,2)

$$F | \frac{\epsilon x}{\epsilon X} \quad (3)$$

$$E | \frac{1}{2} / F^T F 4 I 0 \quad (4)$$

3. Locking Effects

3.1 (Transverse shear locking)

shell solid

solid-shell

(Assumed Natural Strain)

shell ANS [6]

(5,6)

4

and Rifai⁽⁸⁾
Assumed Strain)

Simo
(Enhanced

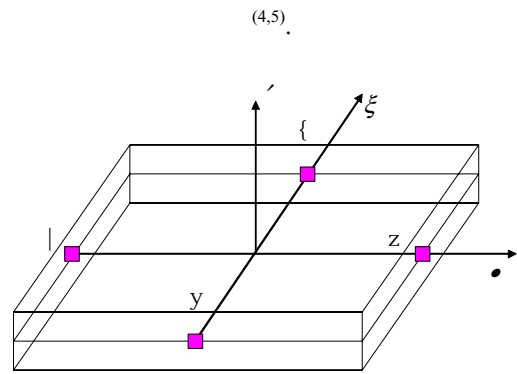


Fig. 1 ANS sampling points

$$E_{\xi'}^{ANS}(\bullet, \prime) | \frac{1}{2} (14 \bullet) E_{\xi'}^D 2 \frac{1}{2} (12 \bullet) E_{\xi'}^B \quad (5)$$

$$E_{\xi'}^{ANS}(\xi, \prime) | \frac{1}{2} (14 \xi) E_{\xi'}^A 2 \frac{1}{2} (12 \xi) E_{\xi'}^C \quad (6)$$

3.2 (Thickness locking)

$$E_{..}$$

0

Hook's law

$$E_{..}$$

solid-shell

$$E_{..}$$

$$E_{..}$$

(thickness locking)

$$E_{..}$$

(7)

(7)

$$u | \frac{1}{2} \begin{pmatrix} 12 \prime & 0 & 0 & 14 \prime & 0 & 0 & 0 \\ 0 & 12 \prime & 0 & 0 & 14 \prime & 0 & 0 \\ 0 & 0 & 12 \prime & 0 & 0 & 14 \prime & 14 \prime^2 \end{pmatrix} \begin{Bmatrix} u_u \\ u_l \\ \eta \end{Bmatrix} \quad (7)$$

Vu-Quoc⁽⁹⁾

(8)

(8)

$$E_{,r}^{EAS} = E_{,r}^C \frac{1}{2} \frac{1}{\det J} \left[1 \cdot \begin{matrix} \text{C}_1 \\ \text{C}_2 \\ \text{C}_3 \end{matrix} \right] \quad (8)$$

4.

Leblond⁽¹⁰⁾

(hyperelastoplastic)

(11)

$$\vartheta = [JU'43\zeta(\chi_4 \chi_0)U'''] I 2 s$$

$$s = dev[\vartheta] \quad (9)$$

Mises
(flow rule)

$$\frac{1}{3} tr[\bar{b}^e] \nu \sqrt{\frac{3}{2} \bar{\kappa}^p} \quad (10)$$

Mises

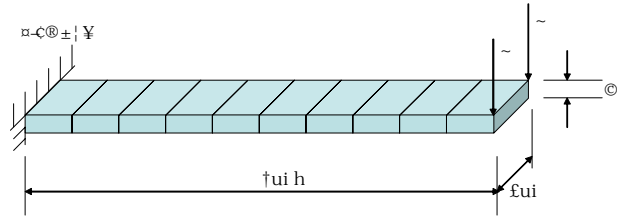


Fig. 2 10*1 Cantilever beam model

$h = 1, 0.1, 0.01$

$$E = 1.0 \Delta 10^7, \tau = 0.0 \quad (11)$$

ANS 8 solid-shell
8 solid
solid
shear locking solid-shell
(Fig. 3)

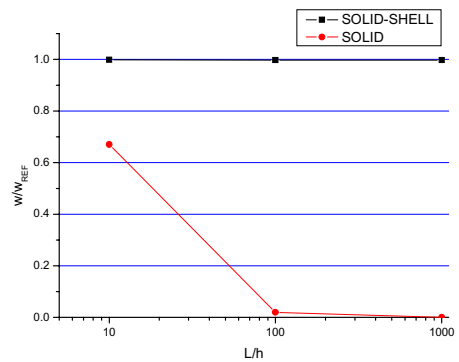


Fig. 3 ANS method in relieving shear locking

0.4 ANS

80%
EAS

Fig. 4

5. Numerical examples

5.1 (Cantilever beam bending problem)

Figure 2 10

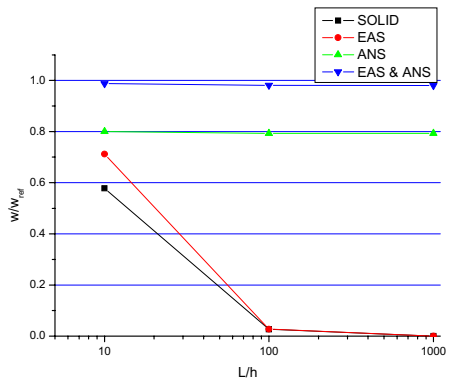


Fig. 4 ANS & EAS method in relieving thickness locking

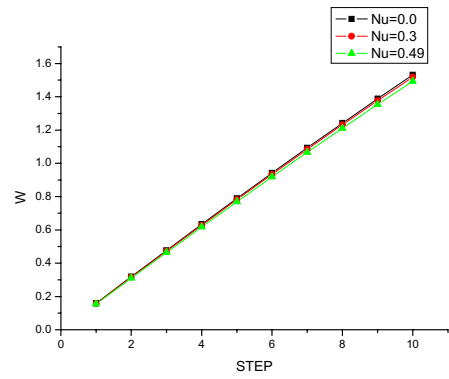


Fig. 6 Load deflection diagram with ANS & EAS method

($h \mid 0.1$)
 10
 EAS
 stiff
 Figure 6 EAS (8)
 640 shell ABAQUS
 (Fig. 7).
 locking

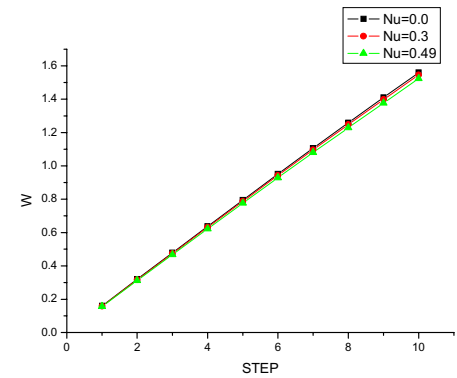


Fig. 7 Load deflection diagram with ABAQUS (S4R, 640 elements)

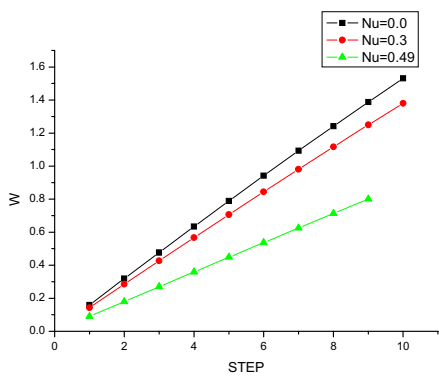


Fig. 5 Load deflection diagram with ANS method

5.2

107
 100*10*1

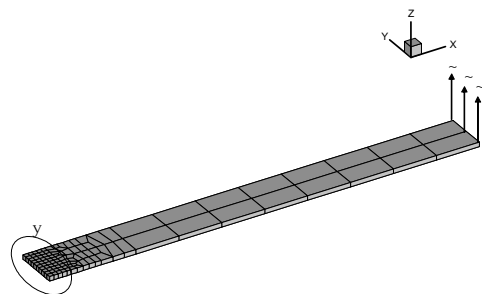


Fig. 8 Cantilever beam- bending and welding model

Figure 8 A POSCO Spiral seam

Z

Figures 9,10 (time=1sec)

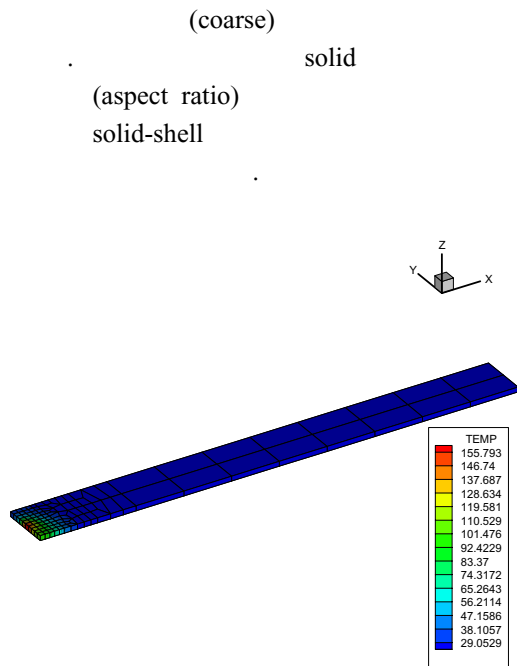


Fig. 9 Cantilever beam – Temperature plot at 1sec

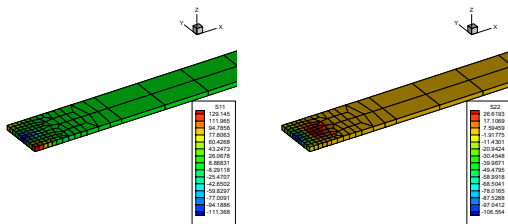


Fig. 10 Cantilever beam – stress plot at 1sec

6.

solid-shell

(EAS)

(ANS)

8

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