

# Fluids in Computer Animation

임인성 교수

서강대학교 공과대학 컴퓨터학과

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최근 컴퓨터 애니메이션 분야에서는 계산 유체 역학 분야의 기법을 적용하여 다양한 유체 애니메이션 효과를 생성하려는 시도가 활발히 진행되고 있다. 본 강연에서는 연기와 가스, 그리고 물 등의 유체에 대하여 애니메이션 제작 분야에서 제안되고 적용되고 있는 유체 기법에 대하여 설명한 후, 본 서강대학교 컴퓨터 그래픽스 연구실에서 수행하고 있는 유체 애니메이션 관련 연구에 대하여 간략히 알아본다.

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강연자 전자메일  
ihm@sogang.ac.kr

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서강대학교 공과대학 컴퓨터학과  
임인성

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## Physically Based Fluids in Computer Animation



$$\nabla \cdot \mathbf{u} = 0$$

$$\frac{\partial \mathbf{u}}{\partial t} = -(\mathbf{u} \cdot \nabla) \mathbf{u} + \nu \nabla^2 (\nabla \mathbf{u}) - \frac{1}{\rho} \nabla p + \mathbf{f}$$

...

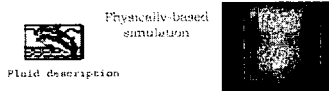
$$\phi_t + \mathbf{u} \cdot \nabla \phi = 0$$

$$\phi_t + \text{sgn}(\phi)(|P_{\nabla \psi} \cdot \nabla \phi| - 1) = 0$$

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## Two Major Tasks in Fluid Animation

- ❖ How are such natural phenomena as water, smoke, fire, flame, and explosion simulated numerically?



- ❖ How are the simulated results visualized realistically?



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## Important Issues in Fluid Animation

- ❖ Which one is more important in the physically based fluid animation?

Preciseness — Cost & Complexity  
Controllability

- Preciseness and Realism
  - Physically-convincing motion must be generated.
- Cost & Complexity
  - 5min x 60sec/min x 30fr/sec x 10min/fr = 90,000min = 62.5days
- Controllability
  - Animation is all about control!
- Applicability to animation production is crucial.

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- ❖ Is it possible to have a fully-interactive real-time physically-based fluid animation?

- The current programmable GPUs on PCs will be powerful and flexible enough to make this possible.

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## Physically Based Simulation of Smoke and Gas



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## Recent Works on Gas and Smoke Simulations



- J. Stam, "Turbulent Wind Field for Gaseous Phenomena," *ACM SIGGRAPH '93*, pp. 369-376, 1993.



- J. Stam, and E. Fiume. "Depiction of Fire and Other Gaseous Phenomena Using Diffusion Process," *ACM SIGGRAPH '95*, pp. 129-136, 1995.



- N. Foster, and D. Metaxas. "Modeling the motion of a hot, turbulent gas," *ACM SIGGRAPH '97*, pp. 181-188, 1997.



- J. Stam, "Stable Fluids," *ACM SIGGRAPH '99*, pp. 121-128, 1999.



- J. Stam, "Interacting with smoke and fire in real time," *CACM*, Vol. 43, pp. 76-83, 2000.



- R. Fedkiw, and J. Stam, and H. Jensen. "Visual Simulation of Smoke," *ACM SIGGRAPH '01*, pp. 15-22, 2001.

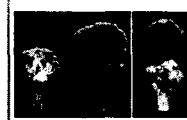


- J. Stam, "A simple fluid solver based on the FFT," *Journal of Graphics Tools*, Vol. 6, pp. 43-52, 2001.

- J. Stam, "Real-Time Fluid Dynamics for Games," *Proceedings of Game Developer Conference*, 2003.



- A. Treuille, A. McNamara, Z. Popovic, and J. Stam. "Keyframe Control of Smoke Animation," *ACM Transactions on Graphics (ACM SIGGRAPH '03)*, Vol. 22, No. 3, pp. 716-723, 2003.



- N. Rasmussen, D. Nguyen, W. Geiger, and R. Fedkiw, "Smoke simulation for large scale phenomena," *ACM Transactions on Graphics (ACM SIGGRAPH '03)*, Vol. 22, No. 3, pp. 703-707, 2003.



- X. Wei, Y. Zhao, Z. Fan, W. Li, S. Yoakum-Stover, and A. Kaufman "Blowing in the wind," *ACM Siggraph/Eurographics Symposium on Computer Animation '03*, pp. 75-85, 2003.

## Basic Equations in [Stam99]



### ❖ The incompressible Navier-Stokes equations

For the velocity  $\mathbf{u} = (u, v, w)$ ,

- Conservation of mass

$$\nabla \cdot \mathbf{u} = 0$$

- Conservation of momentum

$$\frac{\partial \mathbf{u}}{\partial t} = \underbrace{-(\mathbf{u} \cdot \nabla) \mathbf{u}}_{\text{advection}} + \underbrace{\nu \nabla \cdot (\nabla \mathbf{u})}_{\text{diffusion}} - \underbrace{\frac{1}{\rho} \nabla p}_{\text{pressure}} + \underbrace{\mathbf{f}}_{\text{external force}}$$

### ❖ Helmholtz-Hodge decomposition

$$\mathbf{w} = \mathbf{u} + \nabla q, \text{ where } \nabla \cdot \mathbf{u} = 0$$

and  $q$  is a scalar field.

- "Any vector field is the sum of a mass conserving field and a gradient field."

### ❖ Projection operator $\mathbf{P}$

$$\nabla \cdot \mathbf{w} = \nabla^2 q \rightarrow \mathbf{u} = \mathbf{P} \mathbf{w} = \mathbf{w} - \nabla q$$

### ❖ The combined Navier-Stokes equations

- Using the fact that  $\mathbf{P} \mathbf{u} = \mathbf{u}$  and  $\mathbf{P} \nabla p = 0$ , the following equation is obtained:

$$\frac{\partial \mathbf{u}}{\partial t} = \mathbf{P} (-(\mathbf{u} \cdot \nabla) \mathbf{u} + \nu \nabla \cdot (\nabla \mathbf{u}) + \mathbf{f})$$

## Updating the Velocity Field $\mathbf{u}$



### ❖ The general procedure

$$u(x, t) \quad \frac{\partial u}{\partial t} = P(-(\mathbf{u} \cdot \nabla)\mathbf{u} + \nu \nabla \cdot (\nabla \mathbf{u}) + \mathbf{f}) \quad u(x, t + \Delta t)$$

$$\mathbf{w}_0(\mathbf{x}) \xrightarrow{\text{add force}} \mathbf{w}_1(\mathbf{x}) \xrightarrow{\text{advect}} \mathbf{w}_2(\mathbf{x}) \xrightarrow{\text{diffuse}} \mathbf{w}_3(\mathbf{x}) \xrightarrow{\text{project}} \mathbf{w}_4(\mathbf{x})$$

### 1. The *add force* step: $\mathbf{f}$

$$\mathbf{w}_1(\mathbf{x}) = \mathbf{w}_0(\mathbf{x}) + \Delta t \mathbf{f}(\mathbf{x}, t)$$

### 2. The *advect* step: $-(\mathbf{w}_1 \cdot \nabla) \mathbf{w}_1$

- Use the method of characteristics for the effect of advection: a semi-Lagrangian scheme

$$\mathbf{w}_2(\mathbf{x}) = \mathbf{w}_1(\mathbf{p}(\mathbf{x}, -\Delta t))$$

where  $\mathbf{p}(\mathbf{x}, t)$  is the characteristics of the vector field.

- Implementation:

- Build a particle tracer and linear (or cubic) interpolator.



### 3. The *diffuse* step: $\nabla \cdot (\nu \nabla \mathbf{w}_2)$

- Use an implicit method for the effect of viscosity.

$$(\mathbf{I} - \nu \Delta t \nabla^2) \mathbf{w}_3(\mathbf{x}) = \mathbf{w}_2(\mathbf{x}),$$

where  $\mathbf{I}$  is the identity operator.

- Implementation:

- Use the linear solver POIS3D from FISHPAK after discretization.

### 4. The *project* step: $P(\mathbf{w}_3)$

- Apply the projection operator to make the velocity field divergent-free.

$$\nabla^2 q = \nabla \cdot \mathbf{w}_3 \rightarrow \mathbf{w}_4 = \mathbf{w}_3 - \nabla q$$

- Implementation:

- Use the linear solver POIS3D from FISHPAK after discretization.

## Moving Substances through the Fluid



- A non-reactive substance is advected by the fluid while diffusing at the same time.
- The following equation can be used to evolve density, temperature, texture coordinates, etc.

$$\frac{\partial a}{\partial t} = -\mathbf{u} \cdot \nabla a + \kappa_a \nabla^2 a - \alpha_a a + S_a$$

where  $\kappa_a$  is a diffusion constant,  $\alpha_a$  is a dissipation rate, and  $S_a$  is a source term.

- Dissipation term

$$(1 + \Delta t \alpha_a) a(\mathbf{x}, t + \Delta t) = a(\mathbf{x}, t)$$

## Summary of [Stam99]



- Based on the full Navier-Stokes equations
- Based on an 'unconditionally' stable computational model
  - Semi-Lagrangian integration scheme
- Easy to implement
- Appropriate for gas and smoke
- Suffer from too much 'numerical dissipation'
  - The flow tends to dampen too rapidly.
  - [FedkiwStamJensen01] attempted to solve this problem.

## Basic Equations in [FedkiwStamJensen01]

### ❖ The incompressible Euler equations

"Gases are modeled as inviscid, incompressible, constant density fluids."

$$\nabla \cdot \mathbf{u} = 0$$

$$\frac{\partial \mathbf{u}}{\partial t} = -(\mathbf{u} \cdot \nabla) \mathbf{u} - \nabla p + \mathbf{f}$$

### ❖ The equations for the evolution of the temperature $T$ and the smoke's density $\rho$

$$\frac{\partial T}{\partial t} = -(\mathbf{u} \cdot \nabla) T$$

$$\frac{\partial \rho}{\partial t} = -(\mathbf{u} \cdot \nabla) \rho$$

## Updating the Velocity Field $\mathbf{u}$

### 1. The *add force* step: $\mathbf{f}$

- Update the velocity field for the effect of forces.

$$\mathbf{f} = \mathbf{f}_{user} + \mathbf{f}_{buoy} + \mathbf{f}_{conf}$$

- $\mathbf{f}_{user}$ : user-defined force (for any purpose)
- $\mathbf{f}_{buoy}$ : gravity and buoyancy forces

$$\mathbf{f}_{buoy} = -\alpha \rho \mathbf{z} + \beta (T - T_{amb}) \mathbf{z}, \text{ where } \mathbf{z} = (0, 0, 1)$$

$\mathbf{f}_{conf}$ : vorticity confinement force

- Use a vorticity confinement method by Steinhoff and Underhill.
- Inject the energy lost due to numerical dissipation back into the fluid using a forcing term.

- Reduce the numerical dissipation inherent in semi-Lagrangian schemes.

$$\boldsymbol{\omega} = \nabla \times \mathbf{u} \rightarrow \mathbf{N} = \frac{\boldsymbol{\omega}}{|\boldsymbol{\omega}|} (\eta = \nabla \cdot |\boldsymbol{\omega}|) \rightarrow \mathbf{f}_{conf} = c h (\mathbf{N} \times \boldsymbol{\omega})$$

- Implementation: simple

### 2. The *advect* step: $-(\mathbf{u} \cdot \nabla) \mathbf{u}$

- Use the method of characteristics for the effect of advection: a semi-Lagrangian scheme
- Implementation:
  - Build a particle tracer and linear interpolator.
  - Same as [Stam99]

### 3. The *project* step: $\mathbf{P}(\mathbf{w}_3)$

- Apply the projection operator to make the velocity field divergent-free.
- Same as [Stam99]

$$\nabla^2 p = \frac{1}{\Delta t} \nabla \cdot \mathbf{u}^*$$

$$\mathbf{u} = \mathbf{u}^* - \Delta t \nabla p$$

- Implementation:
  - Impose free Neumann boundary conditions at the occupied voxels.
  - Use the conjugate gradient method with an incomplete Choleski pre-conditioner.

## Moving Substances through the Fluid

### ❖ Use the semi-Lagrangian scheme.

$$\frac{\partial T}{\partial t} = -(\mathbf{u} \cdot \nabla) T$$

$$\frac{\partial \rho}{\partial t} = -(\mathbf{u} \cdot \nabla) \rho$$

## Updating the Velocity Field in [stam03]

### ❖ The general procedure

$$\frac{\partial \mathbf{u}}{\partial t} = \mathbf{P}(-(\mathbf{u} \cdot \nabla) \mathbf{u} + \nu \nabla \cdot (\nabla \mathbf{u}) + \mathbf{f}) \quad \mathbf{u}(\mathbf{x}, t + \Delta t)$$

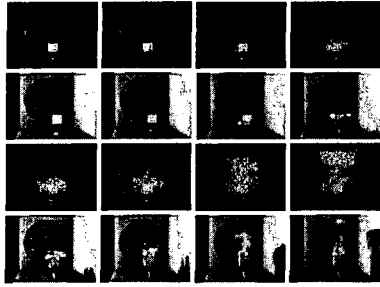
$$\mathbf{w}_0(\mathbf{x}) \xrightarrow{\text{add force}} \mathbf{w}_1(\mathbf{x}) \xrightarrow{\text{diffuse}} \mathbf{w}_2(\mathbf{x}) \xrightarrow{\text{project}} \mathbf{w}(\mathbf{x}) \xrightarrow{\text{advect}} \mathbf{w}_3(\mathbf{x}) \xrightarrow{\text{compress}} \mathbf{w}_4(\mathbf{x})$$

- The basic integration method is same as in [stam99].
- The Gauss-Seidel method is used for solving the linear system instead of FFT.
  - 20 iterations are enough for the projection operator.

## What are we doing with gas and smoke?



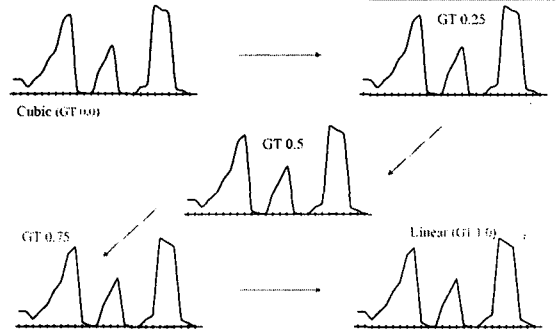
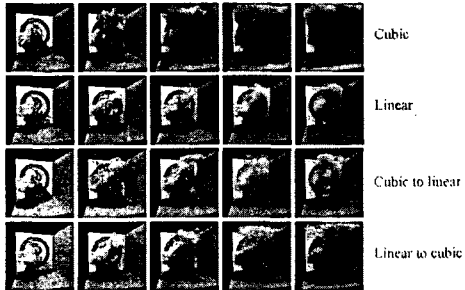
- Development of a stable simulation engine with intuitive user controls



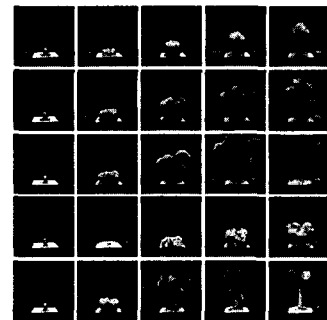
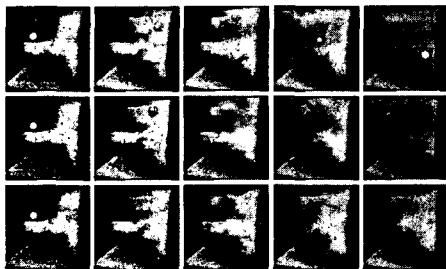
- Application to the animation production



- Design of a controllable monotonic cubic interpolation filter

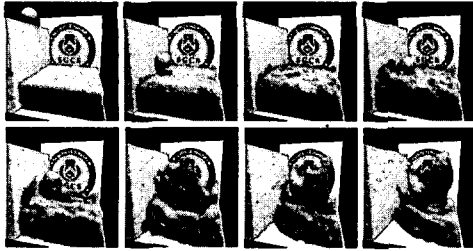


- Animation of chemically reactive fluids



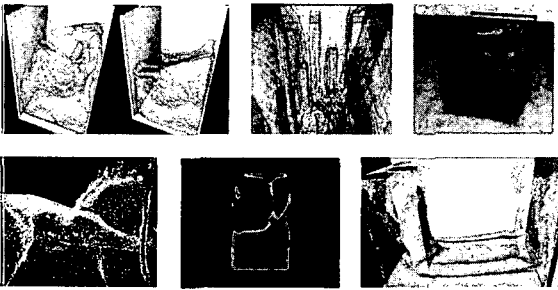


### Effective interaction of moving objects with fluids



- Adaptive and parallel computation of large scale simulations for HD-level animations
- Real-time simulation on programmable graphics processors

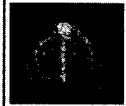
### Physically Based Simulation of Water



### Recent Works on Water Simulation



- N. Foster, and D. Metaxas, "Realistic animation of liquids," *Graphical Models and Image Processing* 58, pp. 471-483, 1996.



- N. Foster, and D. Metaxas, "Controlling fluid animation," *Computer Graphics International '97*, pp. 178-188, 1997.



- N. Foster, and R. Fedkiw, "Practical animation of liquids," *ACM SIGGRAPH '01*, pp. 15-22, 2001.





- D. Enright, R. Fedkiw, J. Ferziger, and I. Mitchell, "A hybrid particle level set method for improved interface capturing," *J. Comp. Phys.* 183, pp. 83-116, 2002.




- D. Enright, S. Marschner, and R. Fedkiw, "Animation and rendering of complex water surfaces," *ACM Transactions on Graphics (ACM SIGGRAPH '02)*, Vol. 21, No. 3, pp. 736-744, 2002.



- C. Chiu, J. Chuang, C. Lin, and J. Yu, "Modeling Highly Deformable Fluid," <http://cg.mwww.csie.nctu.edu.tw/images/jwchiu/ModelingLiquid.pdf>, 2002.





▪ R. Fedkiw, "Simulating Natural Phenomena for Computer Graphics." *Geometric Level Set Methods in Imaging, Vision and Graphics*, edited by S. Osher and N. Paragios, pp. 461-479, Springer Verlag, New York, 2003.



### Cell Properties

- ❖ LIQUID
  - This cell is one that is fully filled with liquid. It is used for the calculation of pressure.
- ❖ EMPTY
  - This cell is one in which no liquid exists at all.
- ❖ SURFACE
  - This cell is one that exists between the LIQUID and the EMPTY cell.
- ❖ BOUNDARY
  - This cell is one that is contained in a solid object. It can be wall, obstacle, and other object that water can't flow in. Velocity of this cell is not governed by Navier-Stokes equation.




### Basic Algorithm in [FosterFedkiw01]

For each time step {


- Update the velocity field by solving the Navier-Stokes equations.
- Update the position of the liquid volume using the new velocity field.

}

$$\nabla \cdot \mathbf{u} = 0$$

$$\frac{\partial \mathbf{u}}{\partial t} = -(\mathbf{u} \cdot \nabla) \mathbf{u} + \nu \nabla \cdot (\nabla \mathbf{u}) - \frac{1}{\rho} \nabla p + \mathbf{f}$$


- ❖ How do we track the dynamically evolving surface of a volume of liquid?
  - Use a hybrid surface model based on particles and level set
  - Both the Lagrangian and the Eulerian approach




### Representing the Water Surface

- ❖ Particle versus level set for dynamically evolving surfaces
  - Particle: a Lagrangian approach
    - Easy to move around in the velocity field.
    - Tricky to handle topological changes.
    - Hard to extract a smooth polygonal representation of the liquid surface.

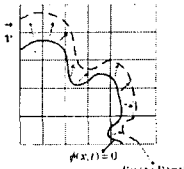

$$\frac{dx_p}{dt} = \mathbf{u}_x$$

- Level set: an Eulerian approach
  - Easily produce smooth surfaces.
  - Relatively easy to handle topological changes.
  - Suffer from severe volume loss in under-resolved regions.

$$\phi_t + \mathbf{u} \cdot \nabla \phi = 0$$


### Level Set Method

- ❖ Traces the interface of moving surfaces using a signed distance function.
- ❖ Signed distance function  $\phi = \phi(x, y, z, t)$ 
  - The shortest distance from a point to the interface
  - The sign indicates whether a point is inside, on, or outside of the surfaces.
- ❖ The evolution of the interface is described by the following simple convection equation:
 
$$\phi_t + \mathbf{u} \cdot \nabla \phi = 0$$

- ❖ How do we define  $\mathbf{u}$  in order to create desired visual effects?
- ❖ How do we discretize the equation temporarily and spatially in a stable manner?
  - It is convenient to make the signed distance function to the interface so that  $|\nabla \phi| = 1$ .
    - Reinitialize the function near the interface.
 
$$\phi_\tau + \frac{\phi}{\sqrt{\phi^2 + |\nabla \phi|^2 \Delta x}} (|\nabla \phi| - 1) = 0$$
 where  $\tau$  is the fictitious time and  $\phi_\tau$  is amount to adjust value  $\phi$ .
  - Use a fifth-order accurate Hamilton-Jacobi WENO method to approximate the spatial derivatives.
  - Use a third-order accurate TVD Runge-Kutta method for the temporal integration.

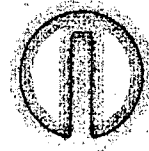


## Particle Level Set Method [Enright et al.02]



- ❖ A hybrid front tracking technique to model the surface interface that uses marker particles combined with a dynamic implicit surface level set.
- ❖ Based on the hybrid method proposed in [FosterFedkiw01].
- ❖ The particles are used to correct errors in moving the level set surfaces.

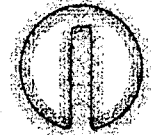
## Example of Particle Level Set Method



Initial placement of particles



After one revolution of particles and level sets



After error correction

## Algorithm of Particle Level Set Method

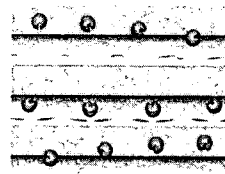


Place both positive and negative particles near the interface.

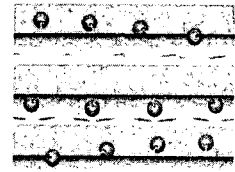
For each time step {

- 1 Update the velocity field by solving the Navier-Stokes equations.
- 2 Evolve both the particles and the level set functions forward in time.
- 3 Correct errors in the level set function using particles.
- 4 Apply re-initialization, correcting errors in the level set function using particles.
- 5 Adjust the particle radii.
- 6 Perform particle reseeding, if necessary.

## Comparison of the Old and the New Schemes

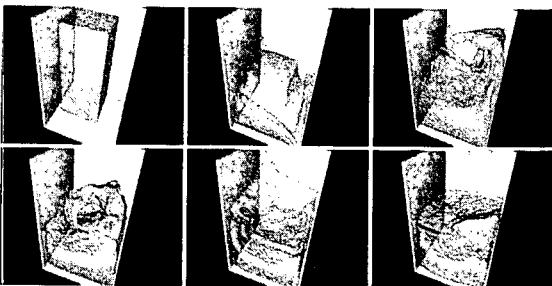


Level-set-only method

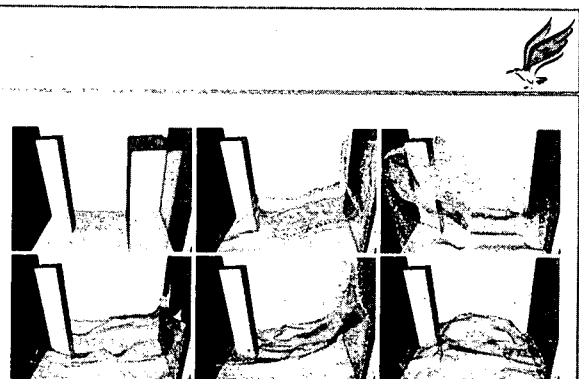


Particle level set method

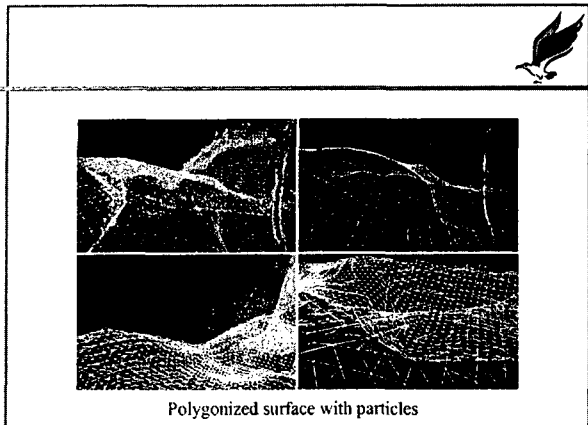
## Implementation Results



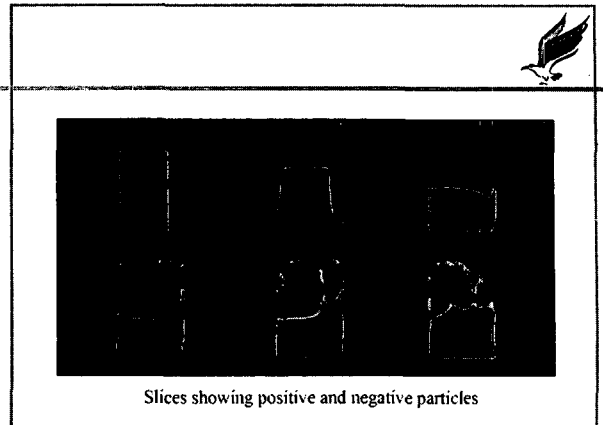
Particle-only method without smoothing



Particle level set method with smoothing



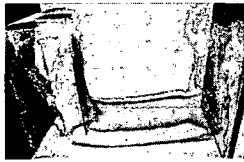
Polygonized surface with particles



Slices showing positive and negative particles

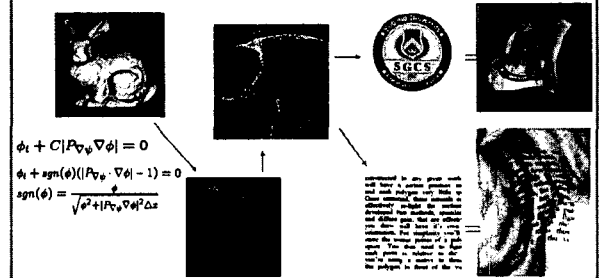
### What are we doing with water and level set?

- Development of a stable simulation engine with intuitive user controls





### Local parameterization of polygonal objects using projection level set

- Local parameterization of polygonal objects using projection level set



### Physically Based Simulation of Fire, Flame, and Explosion

### Recent Works on Fire and Flame Simulation

- 
 P. Beaudoin, S. Paquet, and P. Poulin, "Realistic and controllable fire simulation," *Graphics Interface 2001*, pp. 159 - 166, 2001.
- 
 X. Wei, W. Li, K. Mueller, and A. Kaufman, "Simulating fire with texture splats", *IEEE Visualization 2002*, pp. 227-234, 2002.



- D. Nguyen, R. Fedkiw, and H. Jensen. "Physically based modeling and animation of fire." *ACM Transactions on Graphics (ACM SIGGRAPH '02)*, Vol. 21, No. 3, pp. 721-728, 2002.



- A. Lamorlette, and N. Foster. "Structural modeling of flames for a production environment." *ACM Transactions on Graphics (ACM SIGGRAPH '02)*, Vol. 21, No. 3, pp. 729-735, 2002.



- S. Hasinoff, and K. Kutulakos. "Photo-consistent 3D fire by flame-sheet decomposition". *IEEE International Conf. on Computer Vision*, pp. 1184-1191, 2003.

## Recent Works on Explosion Simulation



- M. Neff, and E. Fiume. "A visual model for blast waves and fracture," *Graphics Interface '99*, pp. 193-202, 1999.

- O. Mazarak, C. Martins, and J. Amanatides. "Animating exploding objects." *Graphics Interface '99*, pp. 211-218, 1999.



- G. Yngve, J. O'Brien, and J. Hodgins. "Animating explosions," *ACM SIGGRAPH '00*, pp. 29-36, 2000.



- B. Bashforth, and Y.-H. Yang. "Physics-based explosion modeling," *Graphical Models*, Vol. 63, No. 1, pp. 21-44, 2001.



- B. Feldman, J. O'Brien, and O. Arikan. "Animating suspended particle explosions," *ACM Transactions on Graphics (ACM SIGGRAPH '03)*, Vol. 22, No. 3, pp. 708-715, 2003.



- N. Rasmussen, D. Nguyen, W. Geiger, and R. Fedkiw. "Smoke simulation for large scale phenomena." *ACM Transactions on Graphics (ACM SIGGRAPH '03)*, Vol. 22, No. 3, pp. 703-707, 2003.