

Robust Optimal Control of Robot Manipulators with a Weighting Matrix Determination Algorithm

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Abstract: A robust optimal control design is proposed in this study for rigid robotic systems under the unknown load and the other uncertainties. The uncertainties are quadratically bounded for some positive definite matrix. Iterative method finding the Q weighting matrix is shown. Computer simulations have been done for a weight-lifting operation of a two-link manipulator and the result of the simulation shows that the proposed algorithm is very effective for a robust control of robotic systems.

Keywords: optimal control, uncertainties, weighting matrix, iterative method, robust control

1. INTRODUCTION

The motion control of a robot manipulator has received a great deal of attention in the past decade. Many approaches have been introduced to treat this control problem[1]. Because of the unknown load placed on the manipulator and the other uncertainties in the manipulator dynamics, adaptive control approaches and robust control approaches have been proposed to attenuate these uncertainties. Johansson[2] proposed explicit solutions to the Hamilton-Jacobi equation for optimal control of rigid body motion and designed adaptive control for self-optimization to solve the case of unknown or uncertain system parameters. Chen[3] proposed a mixed H_2/H_∞ control design for tracking of rigid robotic systems under parameter perturbations and external disturbances. And Lin[4] translated the robust control problem into the optimal control problem, where the uncertainties were reflected in the performance index.

This study has been done, based on Lin's work. The dynamics of a robot manipulator is to be written as the state space description by the definition of the state variables, control inputs and uncertainties. We define the uncertainties as the function of the state variables. To translate the robust control problem into the optimal control problem, we have to find a quadratically bounded matrix for the uncertainties. We simplify the problem to find the matrix by its definition as the product of a scalar and an identity matrix. And we define the state variables and the uncertainties as vectors on the finite time interval. Then we search the largest value of the square of the uncertainties divided by the square of the state variables on each time interval. The largest value is selected as the weighting value of the weighting matrix of the state variables in the cost function to be minimized. The optimal control inputs that minimize the cost function are obtained by solving the algebraic Riccati equation. And the control inputs are applied to the manipulator and the states of the system are changed. So the uncertainties are changed and we get the new largest value from the vectors of the uncertainties and state variables changed. The algorithm of searching the largest value includes the repeated routine stopped when the system gives us the same response.

We simulate the proposed algorithm for a weight-lifting operation of a two-link manipulator. We can see that the control is very robust with respect to the change of the load.

2. MANIPULATOR DYNAMICS

The dynamics of a robot manipulator is well understood

and is given by

$$\tau = M(q)\ddot{q} + C(q, \dot{q})\dot{q} + G(q) \quad (1)$$

The position coordinates q with associated velocities \dot{q} and accelerations \ddot{q} are controlled with the driving forces τ . The moment of inertia $M(q)$, the Coriolis, centripetal, and frictional forces $C(q, \dot{q})\dot{q}$, and the gravitational forces $G(q)$ all vary along the trajectories. For simplicity, we denote

$$N(q, \dot{q}) = C(q, \dot{q})\dot{q} + G(q). \quad (2)$$

There are uncertainties in $M(q)$ and $N(q, \dot{q})$ due to unknown load on the manipulator and unmodeled frictions. We assume the following bounds on the uncertainties:

- 1) There exists $M_o(q)$ such that $M(q) \leq M_o(q)$.
- 2) There exists $N_o(q, \dot{q})$ such that $\|N(q, \dot{q})\| \leq \|N_o(q, \dot{q})\|$.

From the dynamics of a robot manipulator, we have

$$\begin{aligned} \ddot{q} &= M^{-1}(\tau - N) \\ &= M^{-1}(\tau - N) - M^{-1}N_o + M^{-1}N_o \\ &= M^{-1}(\tau - N_o) + M^{-1}(N_o - N) \\ &= M^{-1}M_oM_o^{-1}(\tau - N_o) + M^{-1}M_oM_o^{-1}(N_o - N) \end{aligned} \quad (3)$$

where M, N are shorter notation of $M(q), N(q, \dot{q})$, and M_o, N_o are shorter notation of $M_o(q), N_o(q, \dot{q})$, respectively.

Let us define the control input u and the uncertainty w as

$$u = M_o^{-1}(\tau - N_o), \quad w = M_o^{-1}(N_o - N) \quad (4)$$

The joint accelerations \ddot{q} are given by

$$\ddot{q} = M^{-1}M_o u + M^{-1}M_o w \quad (5)$$

Define the state variables to be

$$x = \begin{bmatrix} \dot{q} \\ q \end{bmatrix} \quad (6)$$

Then, the state equation is given by

$$\dot{x} = Ax + Bu + Bw \quad (7)$$

where

$$A = \begin{bmatrix} 0 & 0 \\ I & 0 \end{bmatrix}, \quad B = M^{-1}M_o \begin{bmatrix} I \\ 0 \end{bmatrix}. \quad (8)$$

3. OPTIMAL CONTROL APPROACH

The robust control problem can be translated into the optimal control problem and if the solution to the optimal control problem exists, then it is a solution to the robust control problem[4].

Our goal is to solve the following robust control problem.

1) Robust Control Problem: Find a feedback control law such that the closed-loop system as $\dot{x} = Ax + Bu + Bw$, is globally asymptotically stable for all uncertainties w satisfying the condition that there exists a nonnegative function w_o such that $\|w\| \leq w_o$.

We would like to translate this robust control problem into the following optimal control problem.

2) Optimal Control Problem: For the following system as $\dot{x} = Ax + Bu$, find a feedback control law that minimizes the following cost function:

$$J = \frac{1}{2} \int_0^\infty (w_o^T w_o + x^T Qx + u^T Ru) dt \quad (9)$$

To translate the robust control problem into the optimal control problem, we need to assume that the uncertainty w satisfies the following condition:

$$w^T R w < x^T Q_w x \quad (10)$$

for some positive definite matrix Q_w .

Then the optimal control problem reduces to the following linear quadratic regulator(LQR) problem: For the system as $\dot{x} = Ax + Bu$, find a feedback control law that minimizes the following cost function:

$$J = \frac{1}{2} \int_0^\infty (x^T Q_w x + x^T Qx + u^T Ru) dt \quad (11)$$

The Hamiltonian is

$$H = \frac{1}{2} (x^T Q_w x + x^T Qx + u^T Ru) + J_x^{*T} (Ax + Bu) \quad (12)$$

where the minimum cost function J^* is

$$J^* = \min_u \left\{ \frac{1}{2} \int_0^\infty (x^T Q_w x + x^T Qx + u^T Ru) dt \right\} \quad (13)$$

The $u = u^*$ for which H has its minimum value is obtained from the partial derivatives with respect to u .

$$\frac{\partial H}{\partial u} = Ru + B^T J_x^* = 0, \quad J_x^{*T} B = -(u^*)^T R \quad (14)$$

The *Hamilton - Jacobi* equation gives us such that

$$H^* = \frac{1}{2} (x^T Q_w x + x^T Qx + (u^*)^T R (u^*)) + J_x^{*T} (Ax + Bu^*) = 0$$

and $J_x^{*T} (Ax + Bu^*) = -\frac{1}{2} (x^T Q_w x + x^T Qx + (u^*)^T R (u^*))$

Let us define the Lyapunov function candidate V as the minimum cost function J^*

$$V = J^* = \min_u \left\{ \frac{1}{2} \int_0^\infty (x^T Q_w x + x^T Qx + u^T Ru) dt \right\} \quad (15)$$

Solving Eq. (15) gives us the following Equations such as

$$V_x^T B = -(u^*)^T R \quad (16)$$

$$V_x^T (Ax + Bu^*) = -\frac{1}{2} (x^T Q_w x + x^T Qx + (u^*)^T R (u^*)) \quad (17)$$

To show $\dot{V} = dV / dt < 0$, we have

$$\begin{aligned} \dot{V} &= \frac{\partial V}{\partial x} \frac{dx}{dt} \\ &= V_x^T (Ax + Bu^* + Bw) \\ &= V_x^T (Ax + Bu^*) + V_x^T Bw \\ &= -\frac{1}{2} (x^T Q_w x + x^T Qx + (u^*)^T R (u^*)) - (u^*)^T R w \\ &= -\frac{1}{2} (x^T Q_w x - w^T R w) - \frac{1}{2} x^T Qx - \frac{1}{2} (u^* + w)^T R (u^* + w) \end{aligned} \quad (18)$$

By the assumption $x^T Q_w x - w^T R w > 0$ shown in Eq. (10), the Lyapunov function derivative is negative definite. Thus, the condition of the Lyapunov global asymptotic stability theorem is satisfied. The solution can be obtained by solving the following algebraic Riccati equation:

$$0 = Q_w + Q - PBR^{-1}B^T P + PA + A^T P \quad (19)$$

and the optimal control is given by

$$u^* = -R^{-1}B^T P x \quad (20)$$

4. CHOICE OF THE WEIGHTING MATRICES

We need to select the weighting matrices Q , R and Q_w to find the optimal control u^* . The weight matrix Q_w can be selected from the assumption of the uncertainties w .

Let us define $R = rI$ and $Q_w = q_w I$, then $w^T R w < x^T Q_w x$ is given by

$$\frac{\|w\|^2}{\|x\|^2} < \frac{q_w}{r} = \gamma \quad (21)$$

To get the weighting value γ that is satisfied the above condition in finite time interval $[0, N]$, let us define the state variables x and the uncertainties w as follows:

$$x_k = (x_k(0), x_k(1), \dots, x_k(N)) \quad (22)$$

$$w_k = (w_k(0), w_k(1), \dots, w_k(N)) \quad (23)$$

where the subscript k denotes the k th trial, the weighting value γ_k in the k th trial is given by the following l_∞ -norm such as

$$\gamma_k = \|\Gamma_k\|_\infty = \max_{0 \leq i \leq N} |\Gamma_k(i)| \quad (24)$$

where

$$\Gamma_k = (\Gamma_k(0), \Gamma_k(1), \dots, \Gamma_k(N)) \quad (25)$$

$$\Gamma_k(i) = \frac{\|w_k(i)\|^2}{\|x_k(i)\|^2}, \quad i = 0, \dots, N \quad (26)$$

To avoid $\|x_k(i)\|^2 = 0$, dummy variable δ is used as follows:

$$\Gamma_k'(i) = \frac{\|w_k(i)\|^2}{\|x_k(i)\|^2 + \delta}, \quad \delta \approx 0 \quad (27)$$

Now then, we have

$$\Gamma_k(i) = \frac{\|w_k(i)\|^2 \Gamma_k'}{\|w_k(i)\|^2 - \delta \Gamma_k'} \quad (28)$$

The computation to find the weighting value γ is repeated until the following convergence criterion is satisfied such as

$$\|\gamma_k - \gamma_{k-1}\| < \varepsilon \quad (29)$$

where ε is a given error requirement.

5. EXMAPLE

We illustrate the proposed optimal control approach by an example of a two-link robot manipulator in Fig. 1, with point masses m_1, m_2 (kg), lengths l_1, l_2 (m), angular positions q_1, q_2 (rad), and torques τ_1, τ_2 (Nm). The parameters for the equation of motion are

$$M(q) = \begin{pmatrix} (m_1 + m_2)l_1^2 & m_2l_1l_2(s_1s_2 + c_1c_2) \\ m_2l_1l_2(s_1s_2 + c_1c_2) & m_2l_2^2 \end{pmatrix}$$

$$C(q, \dot{q}) = m_2l_1l_2(c_1s_2 - s_1c_2) \begin{pmatrix} 0 & -\dot{q}_2 \\ +\dot{q}_1 & 0 \end{pmatrix}$$

$$G(q) = \begin{pmatrix} -(m_1 + m_2)l_1gs_1 \\ -m_2l_2gs_2 \end{pmatrix}$$

and the short-hand notations $c_1 = \cos(q_1), s_1 = \sin(q_1), c_2 = \cos(q_2), s_2 = \sin(q_2)$ are used.

For the convenience of simulation, the nominal parameters of the robotic system are given as $m_1 = 1(\text{kg}), m_2 = 10(\text{kg}), l_1 = 1(\text{m}), l_2 = 1(\text{m})$ and the initial values $q_1 = q_2 = \pi/2$ (rad), $\dot{q}_1 = \dot{q}_2 = 0$. The reference values are $q_r = 0, \dot{q}_r = 0$. $M(q)$ and $N(q, \dot{q})$ are the function of q

<i>k</i>	<i>t</i>	<i>gamma</i>	<i>gamma'</i>	<i>xx(5001)</i>	<i>xxSUM</i>	<i>JSUM</i>
000	0.000	00000.000000	00000.000000	00.000000	009836.282035	000025090.563501
001	2.894	35214.557504	17607.278752	00.000000	002475.407387	043729280.111337
002	0.000	00004.865442	08806.072097	00.000000	002478.113223	021920072.912788
003	0.000	00004.865442	04405.468770	00.000000	002482.352965	011005327.965142
004	0.000	00004.865442	02205.167106	00.000000	002489.043725	005540294.228730
005	0.000	00004.865442	01105.016274	00.000000	002499.909716	002802513.246557
006	0.000	00004.865442	00554.940858	00.000000	002518.140607	001430139.688169
007	0.058	00005.000576	00279.970717	00.000000	002549.343326	000741751.333341
008	0.334	00006.210467	00143.090592	00.000000	002602.273032	000397327.098876
009	0.331	00007.913236	00075.501914	00.000000	002687.932188	000225942.496634
010	0.341	00009.662743	00042.582328	00.000000	002812.639578	000141548.269939
011	0.500	00011.318062	00026.950195	00.000000	002961.734013	000100917.064449
012	0.517	00027.498686	00027.224440	00.000000	002957.832099	000101635.663050
013	0.516	00027.005438	00027.114939	00.000000	002959.381718	000101348.772558
014	0.516	00027.199120	00027.157030	00.000000	002958.784768	000101459.053461
015	0.516	00027.124580	00027.140805	00.000000	002959.014684	000101416.543630
016	0.516	00027.153300	00027.147052	00.000000	002958.926124	000101432.912580
017	0.516	00027.142239	00027.144646	00.000000	002958.960235	000101426.606936
018	0.516	00027.146500	00027.145573	00.000000	002958.947096	000101429.035614
019	0.516	00027.144859	00027.145216	00.000000	002958.952157	000101428.100129
020	0.516	00027.145491	00027.145353	00.000000	002958.950208	000101428.460454
021	0.516	00027.145247	00027.145300	00.000000	002958.950958	000101428.321665
022	0.516	00027.145341	00027.145321	00.000000	002958.950669	000101428.375123
023	0.516	00027.145305	00027.145313	00.000000	002958.950781	000101428.354532
024	0.516	00027.145319	00027.145316	00.000000	002958.950738	000101428.362463
025	0.516	00027.145313	00027.145315	00.000000	002958.950754	000101428.359408
026	0.516	00027.145315	00027.145315	00.000000	002958.950748	000101428.360585
027	0.516	00027.145315	00027.145315	00.000000	002958.950750	000101428.360132
028	0.516	00027.145315	00027.145315	00.000000	002958.950749	000101428.360306
029	0.516	00027.145315	00027.145315	00.000000	002958.950750	000101428.360239
030	0.516	00027.145315	00027.145315	00.000000	002958.950750	000101428.360265
031	0.516	00027.145315	00027.145315	00.000000	002958.950750	000101428.360255
032	0.516	00027.145315	00027.145315	00.000000	002958.950750	000101428.360259
033	0.516	00027.145315	00027.145315	00.000000	002958.950750	000101428.360257
034	0.516	00027.145315	00027.145315	00.000000	002958.950750	000101428.360258
035	0.516	00027.145315	00027.145315	00.000000	002958.950750	000101428.360258
036	0.516	00027.145315	00027.145315	00.000000	002958.950750	000101428.360258
037	0.516	00027.145315	00027.145315	00.000000	002958.950750	000101428.360258
038	0.516	00027.145315	00027.145315	00.000000	002958.950750	000101428.360258
039	0.516	00027.145315	00027.145315	00.000000	002958.950750	000101428.360258
040	0.516	00027.145315	00027.145315	00.000000	002958.950750	000101428.360258

Table. 1 The result of Iterative Method for $m_L = 0., \gamma'_k = (\gamma'_{k-1} + \gamma_k)/2$

and \dot{q} . So, they are changed each moment according to the motion of the manipulator and it is not easy to get the boundary. But in the regulator problem of weight-lifting operation, if it is assumed that the dynamics of the manipulator includes the uncertainty of the mass of the unknown load only, it is not difficult to calculate $M(q)$ and $N(q, \dot{q})$ when the mass of the unknown load is the maximum value. They are selected as $M_o(q)$ and $N_o(q, \dot{q})$ and used in simulations. If the maximum value is 10(kg), M_o, C_o, G_o are given by

$$M_o(q) = \begin{pmatrix} 21 & 20(s_1s_2 + c_1c_2) \\ 20(s_1s_2 + c_1c_2) & 20 \end{pmatrix}$$

$$C_o(q, \dot{q}) = 20(c_1s_2 - s_1c_2) \begin{pmatrix} 0 & -\dot{q}_2 \\ +\dot{q}_1 & 0 \end{pmatrix}$$

$$G_o(q) = \begin{pmatrix} -21gs_1 \\ -20gs_2 \end{pmatrix}$$

Iteration method is initialized by the weighting matrices $Q=I, R=I$ and the weighting value $\gamma=0$. To get the converged weighting value γ , we use $\gamma'_k = (\gamma'_{k-1} + \gamma_k)/2$ instead of γ_k for the k th trial. The result of iterative method for the mass of the load $m_L = 0$ is shown in Table 1. In the k th trial, the largest weighting value γ_k , γ , the very moment t , the squared value of the state variable on the final time interval $\|x_k(N)\|^2$, $xx(5001)$, the sum of the squared value of the state variable on the finite time interval $\sum_{i=0}^N \|x_k(i)\|^2$,

$xxSUM$, and the cost function $J, JSUM$ are listed in Table 1. Since the 34th trial, the largest weighting value γ and the very moment t converge to $\gamma = 27.145315, t = 0.516$ and the system is to be steady state.

The weighting matrix selected from the proposed iterative method $Q_w = 27.145315I$ and the weighting matrices $Q=I, R=I$ are used to solve the algebraic Riccati equation. The simulation results for $\gamma=0$ and $\gamma=27.145315$ are shown in Figs. 2-7. Fig. 2 shows the joint position q_1 , joint velocity \dot{q}_1 , applied torque τ_1 for $m_L = 0$. Fig. 3 shows the joint position q_2 , joint velocity \dot{q}_2 , applied torque τ_2 for $m_L = 0$. Figs. 4-5 are the results for $m_L = 5$ and Figs. 6-7 are the results for $m_L = 10$. From the figures, we can see that the control is very robust with respect to the change in the load.

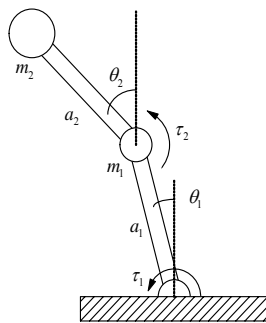


Fig. 1 A two-link manipulator with masses m_1 and m_2 .

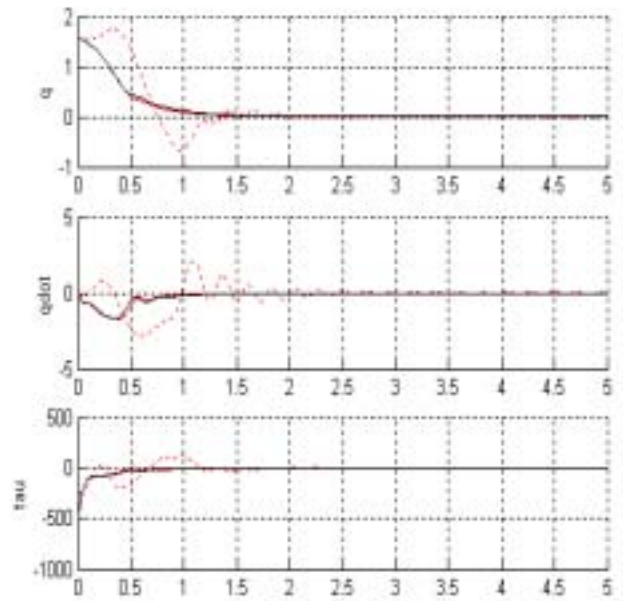


Fig. 2 Response for the mass of the load $m_L=0$ (kg).

Dotted line is the response for $\gamma=0$.

Solid line is the response for $\gamma=27.145315$.

Upper graph shows the joint position q_1 , middle graph shows the joint velocity \dot{q}_1 and lower graph shows the applied torque τ_1 , respectively. All graphs versus time(s).

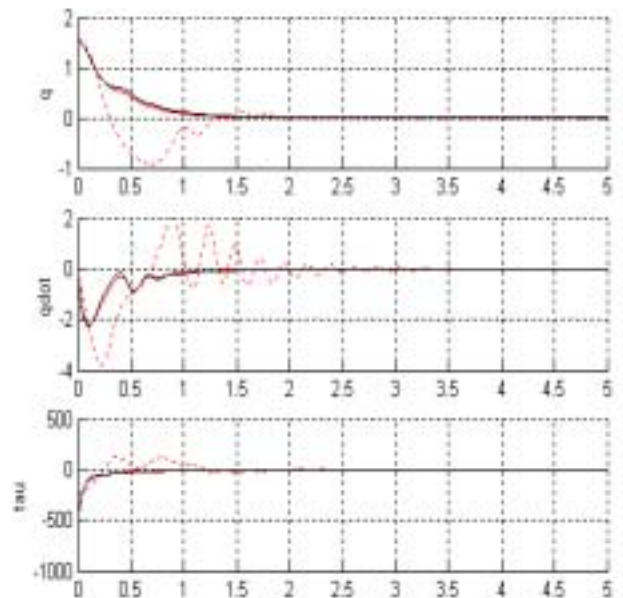


Fig. 3 Response for the mass of the load $m_L=0$ (kg).

Dotted line is the response for $\gamma=0$.

Solid line is the response for $\gamma=27.145315$.

Upper graph shows the joint position q_2 , middle graph shows the joint velocity \dot{q}_2 and lower graph shows the applied torque τ_2 , respectively. All graphs versus time(s).

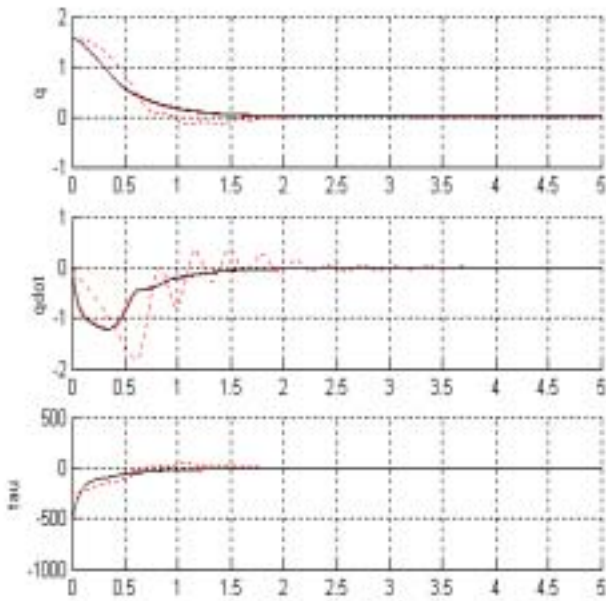


Fig. 4 Response for the mass of the load $m_L=5(\text{kg})$.
 Dotted line is the response for $\gamma=0$.
 Solid line is the response for $\gamma=27.145315$.
 Upper graph shows the joint position q_1 , middle graph shows the joint velocity \dot{q}_1 and lower graph shows the applied torque τ_1 , respectively. All graphs versus time(s).

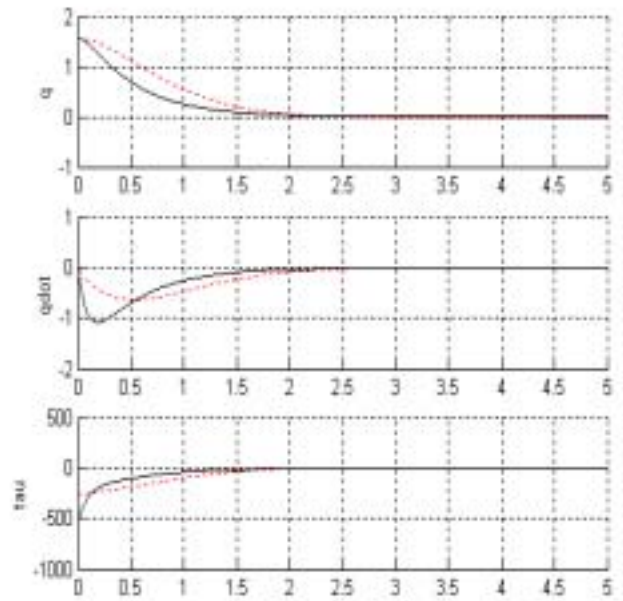


Fig. 6 Response for the mass of the load $m_L=10(\text{kg})$.
 Dotted line is the response for $\gamma=0$.
 Solid line is the response for $\gamma=27.145315$.
 Upper graph shows the joint position q_1 , middle graph shows the joint velocity \dot{q}_1 and lower graph shows the applied torque τ_1 , respectively. All graphs versus time(s).

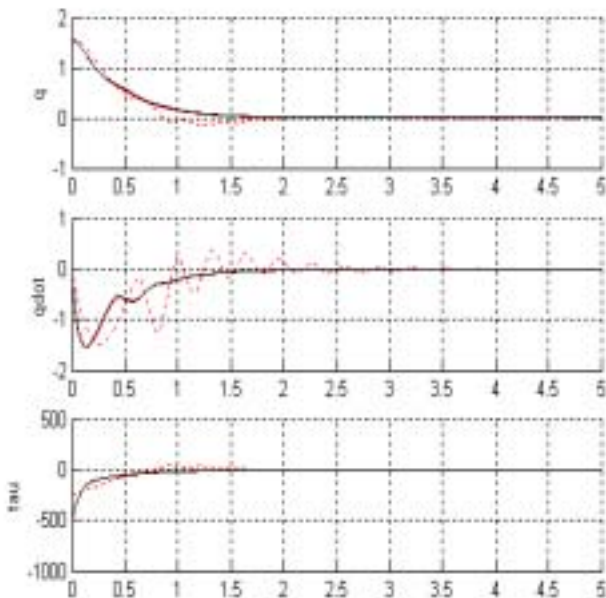


Fig. 5 Response for the mass of the load $m_L=5(\text{kg})$.
 Dotted line is the response for $\gamma=0$.
 Solid line is the response for $\gamma=27.145315$.
 Upper graph shows the joint position q_2 , middle graph shows the joint velocity \dot{q}_2 and lower graph shows the applied torque τ_2 , respectively. All graphs versus time(s).

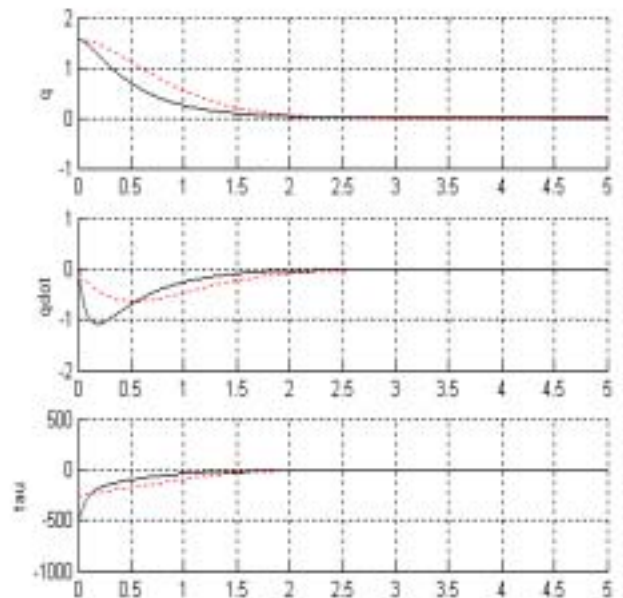


Fig. 7 Response for the mass of the load $m_L=10(\text{kg})$.
 Dotted line is the response for $\gamma=0$.
 Solid line is the response for $\gamma=27.145315$.
 Upper graph shows the joint position q_2 , middle graph shows the joint velocity \dot{q}_2 and lower graph shows the applied torque τ_2 , respectively. All graphs versus time(s).

6. CONCLUSION

We presented a robust optimal control of robot manipulators using the algorithm to choose the weighting matrix. The dynamics of a robot manipulator has been written as the state space description by the definition of the state variables, control inputs and uncertainties. To translate the robust control problem into the optimal control problem, we have to find a quadratically bounded matrix for the uncertainties. We simplified the problem to find the matrix by its definition as the product of a scalar and an identity matrix. We defined the state variables and the uncertainties as vectors on the finite time interval. We proposed an algorithm that searches the largest value of the uncertainties on the finite time interval iteratively. The weighting matrix selected by the proposed algorithm has been used in our simulations. Simulations have been done for a weight-lifting operation of a two-link manipulator and the result of the simulation shows that the proposed algorithm is very effective for a robust control of robotic systems.

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