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# **Computing Fluid Flow without Grid Generation**

W.H. Hui <sup>1</sup>and Z.N. Wu<sup>2</sup>

1. Department of Mathematics and Center for Scientific Computation, Hong Kong University of Science and Technology, Clear Water Bay, Hong Kong Phone: 852 2358 7415 Fax: 852 2358 1643

2. Department of Engineering Mechanics, Tsinghua University, Beijing, China

Corresponding author W.H. Hui

#### **Abstract**

It is shown that using the unified coordinates of Hui et al. [1-4], one can now compute fluid flow without prior grid generation. This represents a great saving of computing time.

#### 1. Introduction

After decades of intensive research on the shock-capturing method using Eulerian coordinates, two drawbacks remains: (i) slip lines are poorly resolved, and (ii) prior to flow field computation, it is necessary to generate a computation grid, which can be very time consuming.

Recently, a unified coordinate system was introduced by Hui et al. [1 - 4] which moves with velocity hq, q being the fluid velocity. By choosing h to preserve grid orthogonality, it resolves slip lines sharply, get the computation does not break down as the Lagrangian system does.

The fact that the unified coordinate system moves with velocity hq can be utilized to generate computational grid while the flow computation goes on. This is in direct contrast to the Eulerian computation, where a grid must be generated prior to flow computation, and this represents a great saving of computing time. It is noted that in typical aeronautical applications, computing the grid takes much longer time than computing the flow field itself.

### 2. The Unified Coordinates

Starting from Cartesian coordinates (x, y, z) and time t in the Eulerian description, we make a transformation to the unified coordinates ( $\lambda$ ,  $\xi$ ,  $\eta$ ,  $\zeta$ ),

$$\int dt = d\lambda \tag{1a}$$

$$dx = hud\lambda + Ad\xi + Ld\eta + Pd\zeta$$

$$dy = hvd\lambda + Bd\xi + Md\eta + Qd\zeta$$

$$dz = hvd\lambda + Cd\xi + Nd\eta + Rd\zeta$$
(1a)
$$dz = hvd\lambda + Cd\xi + Nd\eta + Rd\zeta$$
(1d)

$$dy = hvd\lambda + Bd\xi + Md\eta + Qd\zeta \tag{1c}$$

$$dz = hwd\lambda + Cd\xi + Nd\eta + Rd\zeta, \tag{1d}$$

where 
$$u$$
,  $v$ , and  $w$  are the  $x$ ,  $y$  and  $z$  components of fluid velocity  $q$ , respectively. Let
$$\frac{D_h}{Dt} \equiv \frac{\partial}{\partial t} + hu \frac{\partial}{\partial x} + hv \frac{\partial}{\partial y} + hw \frac{\partial}{\partial z} \tag{2}$$

denote the material derivative following the pseudo-particle, whose velocity is hq. Then, it is easy to show that

$$\frac{D_h \xi}{Dt} = 0, \qquad \frac{D_h \eta}{Dt} = 0, \qquad \frac{D_h \zeta}{Dt} = 0; \tag{3}$$

that is, coordinates  $(\xi, \eta, \zeta)$  are material functions of the pseudo-particles. computational cells move and deform with pseudo-particles, rather than with fluid particles as in Lagrangian coordinates. As a special case when h=1, the coordinates  $(\lambda, \xi, \eta)$  move with fluid velocity q and are thus Lagrangian coordinates. On the other hand when h=0,  $(\lambda, \xi, \eta)$  do not move and are thus are Eulerian coordinates.

Consider two-dimensional unsteady flow for which the Euler equations are

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$$\frac{\partial}{\partial t} \begin{pmatrix} \rho \\ \rho u \\ \rho v \\ \rho e \end{pmatrix} + \frac{\partial}{\partial x} \begin{pmatrix} \rho u \\ \rho u^{2} + p \\ \rho u v \\ \rho u \left( e + \frac{p}{\rho} \right) \end{pmatrix} + \frac{\partial}{\partial y} \begin{pmatrix} \rho v \\ \rho u v \\ \rho v^{2} + p \\ \rho v \left( e + \frac{p}{\rho} \right) \end{pmatrix} = 0, \tag{4}$$

where p and  $\rho$  are pressure and density, respectively, and

$$e = \frac{1}{2}(u^2 + v^2) + \frac{1}{\gamma - 1}\frac{p}{\rho}.$$

Under the transformation (1) we get

$$\frac{\partial \mathbf{E}}{\partial \lambda} + \frac{\partial \mathbf{F}}{\partial \xi} + \frac{\partial \mathbf{G}}{\partial \eta} = 0, \tag{5a}$$

where

$$\mathbf{E} = \begin{pmatrix} \rho \Delta \\ \rho \Delta u \\ \rho \Delta v \\ \rho \Delta e \\ A \\ B \\ L \\ M \end{pmatrix}, \quad \mathbf{F} = \begin{pmatrix} \rho(1-h)I \\ \rho(1-h)Iu + pM \\ \rho(1-h)Iv - pL \\ \rho(1-h)Ie + pI \\ -hu \\ -hv \\ 0 \end{pmatrix}, \quad \mathbf{G} = \begin{pmatrix} \rho(1-h)J \\ \rho(1-h)Ju - pB \\ \rho(1-h)Jv + pA \\ \rho(1-h)Je + pJ \\ 0 \\ 0 \\ -hu \\ -hv \end{pmatrix}, \quad (5b)$$

with

$$\Delta = AM - BL, \quad I = uM - vL, \qquad J = Av - Bu. \tag{6}$$

We note that the Euler equations (5) written in the unified coordinates are in conservation form, so any standard shock-capturing method, e.g. Godunov method, can be used to compute their solutions. The free function h is best chosen to preserve grid angles, hence grid orthogonality [1].

# 3. Computation Procedure

To compute a steady uniform flow past a given body,

- (1) Begin with a column of uniform orthogonal cells of the width  $\Delta x$ , where the uniform flow is given.
- Compute the solution to Eq. (5) by marching in  $\lambda$ , using the Godunov/MUSCL scheme. After one time step  $\Delta\lambda$ , the initial column of cells move to the right by  $h\mathbf{q}_{\infty}\Delta\lambda$  where  $\mathbf{q}_{\infty}$  is the velocity of the uniform free stream.
- (3) After several time steps when the initial column of cells has moved to the right by  $\Delta x$ , add one new column of cells on the left that is identical to the initial column.
- (4) Repeat the above process, until the columns of cells representing the given uniform flow meet a solid boundary, impose the boundary condition there.
- (5) Continue this process until the columns of cells cover the whole body surface, then we simultaneously add a new column of cells on the left while, at the same time, delete the right-most column of cells from our computation; this gives us a fixed window to watch the flow.
- (6) Continue this process until a steady state is judged to have been reached.

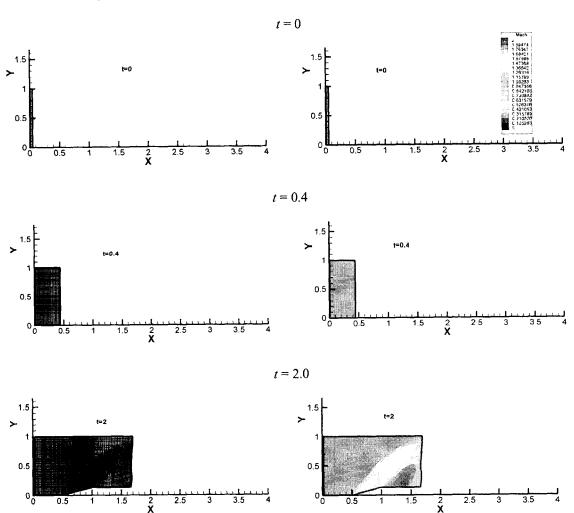
#### 4. An Example

An example of supersonic flow M=1.8, in a channel is shown in Fig. 1. It represents a Mach reflection on the upper boundary.

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# References

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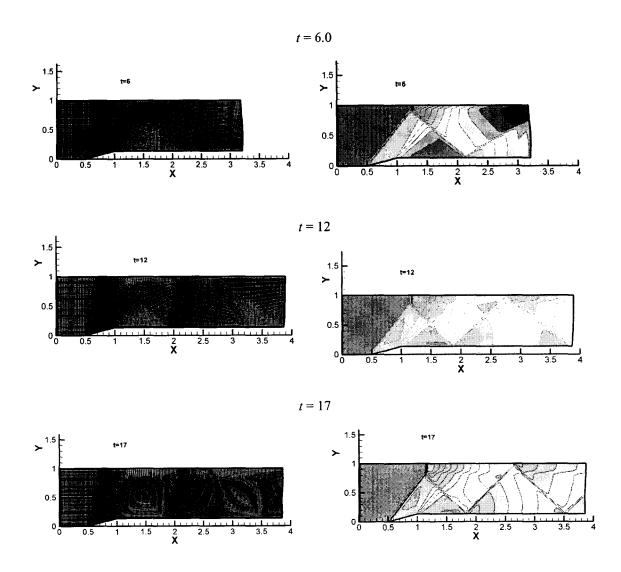


Fig. 1 Supersonic flow in a channel showing Mach reflection,  $M_{\infty} = 1.8$ .