

MBWR을 이용한 LNG 혼합물 Flash 공정 모사

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LNG Mixture Flash Process Modeling for MBWR

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1. 서론

본 연구에서는 BRMR(Bishinoi & Robinson Mixing Rules)를 적용한 MBWR 상태방정식(Modified Benedict-Webb-Rubin Equation of State)을 사용해서 기·액 상평형 물성 예측에 필요한 Flash 과정에 관하여 발표하고자 한다.

2. 이론

1) MBWR 상태방정식

Benedict-Webb-Rubin 상태방정식은 8개의 상수로 이루어져 있다.

$$P = \rho RT + (B_o RT - A_o - \frac{C_o}{T^2})\rho^2 + (bRT - a)\rho^3$$

$$aa\rho^6 + \frac{c\rho^3}{T^2}(1 + \gamma\rho^2)\exp(-\gamma\rho^2) \quad (2.4-1)$$

그 후 Starling et al. 은 BWR 상태방정식의 온도의존성에 대한 수정을 위해 상수 C_o 와, 임계영역에서 물성예측의 개선을 위해 상수 a 를 아래의 식과 같이 전개하였다.

$$C_o^* = C_{o1} - \frac{C_{o2}}{T} + \frac{C_{o3}}{T^2} \quad (2.4-2)$$

$$a^* = a_1 + \frac{a_2}{T} \quad (2.4-3)$$

그리고 등온의 enthalpy 분석으로 부터 얻어진 C_o^* 와 a^* 를 BWR식에 대입하여 다음의 MBWR 상태 방정식을 구했다.

$$\begin{aligned}
 P = & \rho RT + (B_o RT - A_o - \frac{C_o}{T^2} + \frac{D_o}{T^3} - \frac{E_o}{T^4})\rho^2 \\
 & + (bRT - a - \frac{d}{T})\rho^3 + a(a + \frac{d}{T})\rho^6 \\
 & + \frac{c\rho^3}{T^2}(1 + \gamma\rho^2)\exp(-\gamma\rho^2) \quad (2.4-4)
 \end{aligned}$$

11개의 순수물질 parameter는 다음 식으로 계산된다. (Han&Starling Correlation)

$$\begin{aligned}
 \rho_{ci} B_{oi} &= A_1 + B_1 \omega_i \\
 (\rho_{ci} A_{oi})/(R T_{ci}) &= A_2 + B_2 \omega_i \\
 (\rho_{ci}^2 C_{oi})/(R T_{ci}^3) &= A_3 + B_3 \omega_i \\
 \rho_{ci}^2 \gamma_i &= A_4 + B_4 \omega_i \\
 \rho_{ci}^2 b_i &= A_5 + B_5 \omega_i \\
 (\rho_{ci}^2 a_i)/(R T_{ci}^3) &= A_6 + B_6 \omega_i \\
 \rho_{ci}^3 \alpha_i &= A_7 + B_7 \omega_i \\
 (\rho_{ci}^2 c_i)/(R T_{ci}^3) &= A_8 + B_8 \omega_i \\
 (\rho_{ci} D_{oi})/(R T_{ci}^4) &= A_9 + B_9 \omega_i \\
 (\rho_{ci}^2 d_i)/(R T_{ci}^2) &= A_{10} + B_{10} \omega_i \\
 (\rho_{ci} E_{oi})/(R T_{ci}^5) &= A_{11} + B_{11} \omega_i \exp(-3.8 \omega_i)
 \end{aligned}$$

The Bishinoi-Robinson Mixing Rules

$$\begin{aligned}
 B_{oi} &= \sum_{i=1}^n x_i B_{oi} \\
 A_o &= \sum_{i=1}^n \sum_{j=1}^n x_i x_j A_{oi}^{\frac{1}{2}} A_{oj}^{\frac{1}{2}} (1 - k_{ij})^3 \\
 C_o &= \sum_{i=1}^n \sum_{j=1}^n x_i x_j C_{oi}^{\frac{1}{2}} C_{oj}^{\frac{1}{2}} (1 - k_{ij})^3 \\
 \gamma &= \left[\sum_{i=1}^n x_i \gamma_i^{\frac{1}{2}} \right]^2 \\
 b &= \left[\sum_{i=1}^n x_i b_i^{\frac{1}{3}} \right]^3 \\
 a &= \left[\sum_{i=1}^n x_i a_i^{\frac{1}{3}} \right]^3 \\
 \alpha &= \left[\sum_{i=1}^n x_i \alpha_i^{\frac{1}{3}} \right]^3 \\
 c &= \left[\sum_{i=1}^n x_i c_i^{\frac{1}{3}} \right]^3 \\
 D_o &= \sum_{i=1}^n \sum_{j=1}^n x_i x_j D_{oi}^{\frac{1}{2}} D_{oj}^{\frac{1}{2}} (1 - k_{ij})^4 \\
 d &= \left[\sum_{i=1}^n x_i d_i^{\frac{1}{3}} \right]^3 \\
 E_o &= \sum_{i=1}^n \sum_{j=1}^n x_i x_j E_{oi}^{\frac{1}{2}} E_{oj}^{\frac{1}{2}} (1 - k_{ij})^4
 \end{aligned}$$

Table 1. Interaction parameter, k_{ij}

이성분계	k_{ij}	이성분계	k_{ij}
Methane - Ethane	0.01	Methane - n-Heptane	0.06
Methane - Propane	0.023	Methane - n-Octane	0.07
Methane - n-Butane	0.031	Methane - n-Nonane	0.081
Methane - n-Pentane	0.041	Methane - n-Decane	0.092
Methane - n-Hexane	0.05	-	-

Table 2. Generalized Constant A_j and B_j for MBWR EOS

매개변수의 첨자	매개변수 값	
	A_j	B_j
1	0.4443690	0.115449
2	1.284380	-0.920731
3	0.356306	1.708710
4	0.544979	-0.270896
5	0.528629	0.349261
6	0.484011	0.754130
7	0.0705233	-0.044448
8	0.504087	1.322450
9	0.0307452	0.179433
10	0.0732828	0.463192
11	0.006450	-0.022143

Sample(input data): Methane-Propane Binary System

```

1
.1E-6   .2E-6   .3E-6   .1E-5  1.000001  2.
2 2 30
METHANE      1 16.042   -116.43   0.013    0.6274   673.40
-5.58114 0.564874 0.101132E-03 0.417399E-06 -1.525576E-101.958857E-14 -0.623373
PROPANE       2 44.0940   206.13   0.157    0.3121   616.30
-1.22301 0.179733 0.664580E-04 0.250998E-06 -1.247461E-101.893509E-14 0.178189
0.023
1
0.948     0.052
5
1
-100.      500.
2
-100.      500.
3
-100.      300.
4
-100.      500.
5
-100.      500.

```

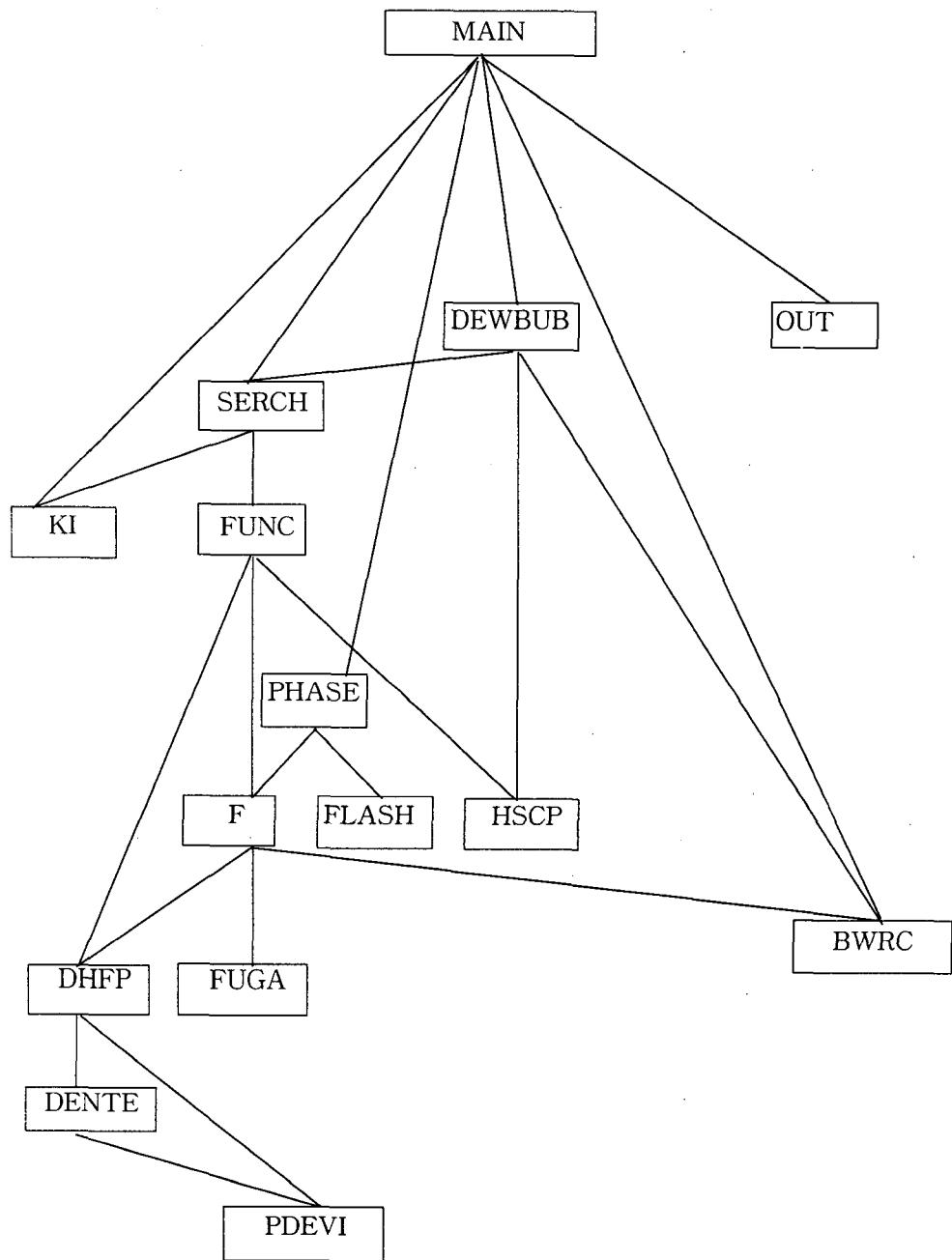


Fig1. Algorithm of MBWR EOS Program

3. 결과 : MBWR EOS를 이용한 flash 계산결과(METHANE-PROPANE)

1	NRUN					
1						
EPSD	EPSV	FUGERR	EPSS	STEP	DMAX	
.10E-06	.20E-06	.30E-06	.10E-05	1.0000010	2.0	
NC	NPHASE	ITNM	IPRNT			
2	2	90	0			
COMP	IDCOM	CMW	TC	ACF	CD	PC
METHANE	1	16.0420	-116.4300	.0130	.6274	673.4000
CI	-5.58114	.564874	.101132E-03	.417399E-06	-.152558E-09	.195886E-13
PROPANE	2	44.0940	206.1300	.1570	.3121	616.3000
CI	-1.22301	.179733	.664580E-04	.250998E-06	-.124746E-09	.189351E-13
CKIG	.0230					
***** FLUID THERMODYNAMIC BEHAVIOR PREDICTOR USING HAN-STARLING GENERALIZED CORRELATION *****						
INLET CONDITIONS						
FLASH CALCULATION(P AND T SPECIFIED, V,L,X AND Y VARIABLE,NTYPE = 1)						
TEMPERATURE= -100.000		F	PRESSURE= 500.000	PSIA		
COMPONENT		MOLE FRACTION		K VALUE		FUGACITY
<hr/>						
METHANE		FEED	VAPOR	LIQUID	VAPOR	LIQUID
.		.948000	.989250	.553183	1.78829	388.512
PROPANE		.052000	.010750	.446817	.240582E-01	1.59112
<hr/>						
PROPERTY		FEED	VAPOR	LIQUID		
<hr/>						
MW		17.5007	16.3435	28.5761		
VOLUME FRACTION		1.00000	.982893	.171068E-01		
<hr/>						
LBMOLE BASIS						
PHASE MOLE FRACTION		1.00000	.905404	.945964E-01		
VOLUME, CU-FT/LBMOLE		5.10832	5.54552	.923791		
DENSITY, LBMOLE/CLFT		.195759	.180326	1.08250		
ENTHALPY, BTU/LBMOLE		2572.66	3022.06	-1728.67		
ENTROPY, BTU/LBMOL-R		37.3846	37.6508	34.8364		
HEAT CAP.,BTU/LBMOL-R		22.2184	20.0957	42.5348		
<hr/>						
LBMASS BASIS						
PHASE MASS FRACTION		1.00000	.845538	.154462		
VOLUME, CU-FT/LB		.291892	.339310	.323274E-01		
DENSITY, LB/CU-FT		3.42592	2.94716	30.9335		
ENTHALPY, BTU/LB		147.003	184.908	-60.4935		
ENTROPY, BTU/LB-R		2.13617	2.30371	1.21908		
HEAT CAP.,BTU/LB-R		1.26957	1.22958	1.48847		