

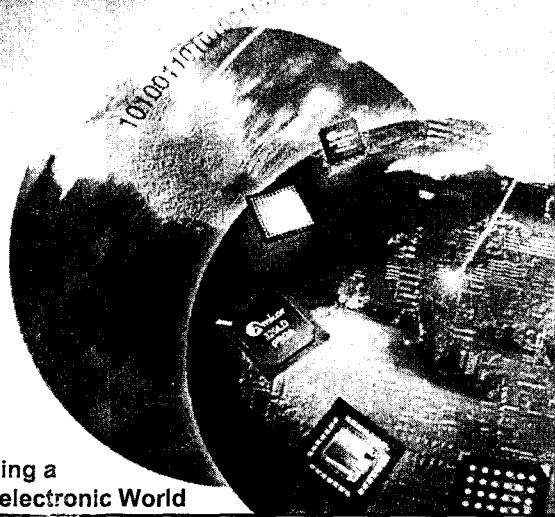
Prediction Methodology for Reliability of Semiconductor Package

AMKOR

R&D

Design & Application

Jin-Young Kim



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Microelectronic World

Package Types



2 Lyr PBGA



etCSP



4 Lyr PBGA



MCM PBGA



TEPBGA - 2



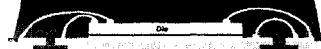
flexBGA



TSBGA



MLF



SBGA



ultraCSP

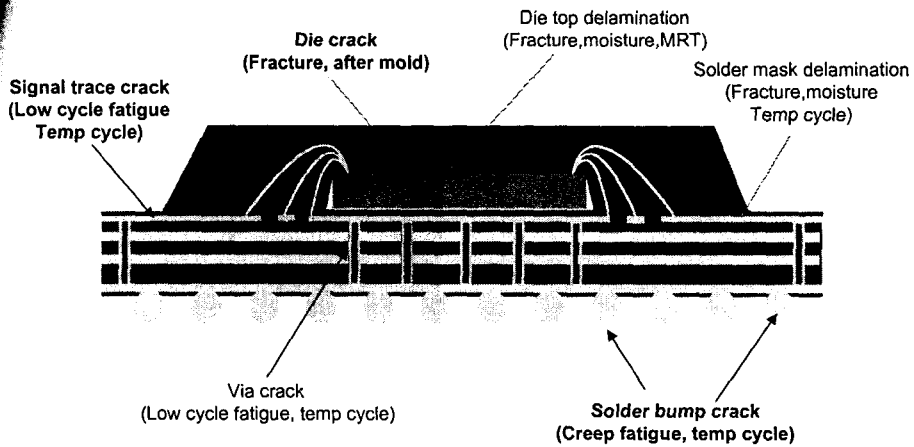


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Mechanical Failures in Package



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AGENDA

- ➔ 1. Die crack problem
2. Signal trace failure
3. Soder joint failure



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Mechanical Reliability of Semiconductor Packages

- Die crack problem -

Package type

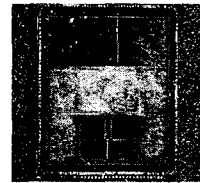
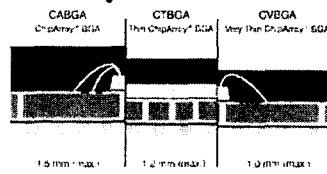
- CABGA, TABGA, μ BGA, flexBGA, etc.
- Thin packages
- Thin substrates (2-layer laminate, Tape)

Root cause

- Bending stress caused by molding pressure or external force
- Initial defect on a die surface
; micro crack induced by roughness of die

Prediction methodology

- Elastic FEM analysis with temperature dependent material properties.
- Failure criteria based on the maximum stress



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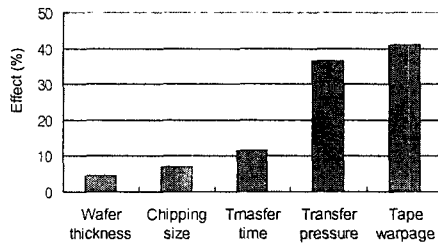
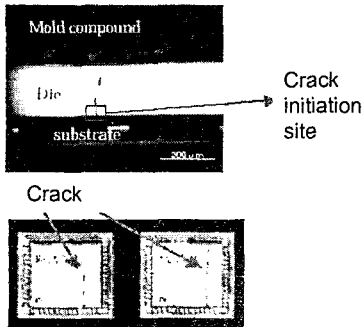
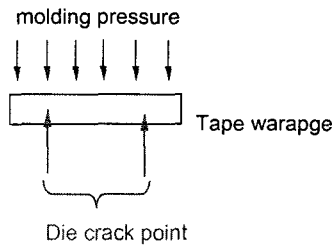
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Mechanical Reliability of Semiconductor Packages

- DOE ANALYSIS -

- Die crack propagates from the bottom surface of die
- Die cracks are the horizontal mode in most cases
- Tape/Substrate warpage and molding pressure are significant factors



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Mechanical Reliability of Semiconductor Packages

- Prediction methodology -

- Analysis of tape/substrate warpage using Finite element method
- Investigation of die flag, trace pattern, and Cu plugging effects
- Suggestion of optimal design to obtain the minimum warpage level
- Stress analysis & failure prediction with a optimized design

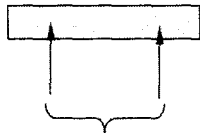
"Tape warpage"



molding pressure

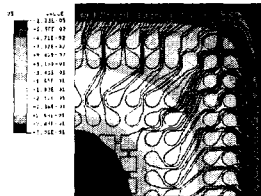


Tape warpage



Die cracks

Warpage Contour



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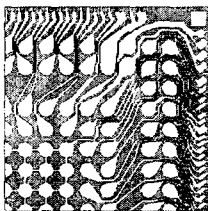
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Mechanical Reliability of Semiconductor Packages

- Optimal Design -

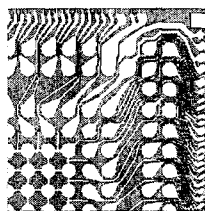
- ◆ Die flag design
 - Wider connection bar of die flag pattern
 - Larger Cu area of die flag pattern
- ◆ Dummy Cu pattern in signal trace area is not necessary
- ◆ Cu plug gives small improvement in tape warpage performance

proposal 1



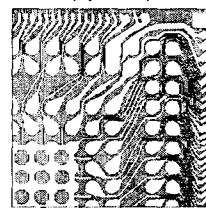
0.2715mm

proposal 2



0.2607mm

proposal 3
(optimal)



0.2073mm

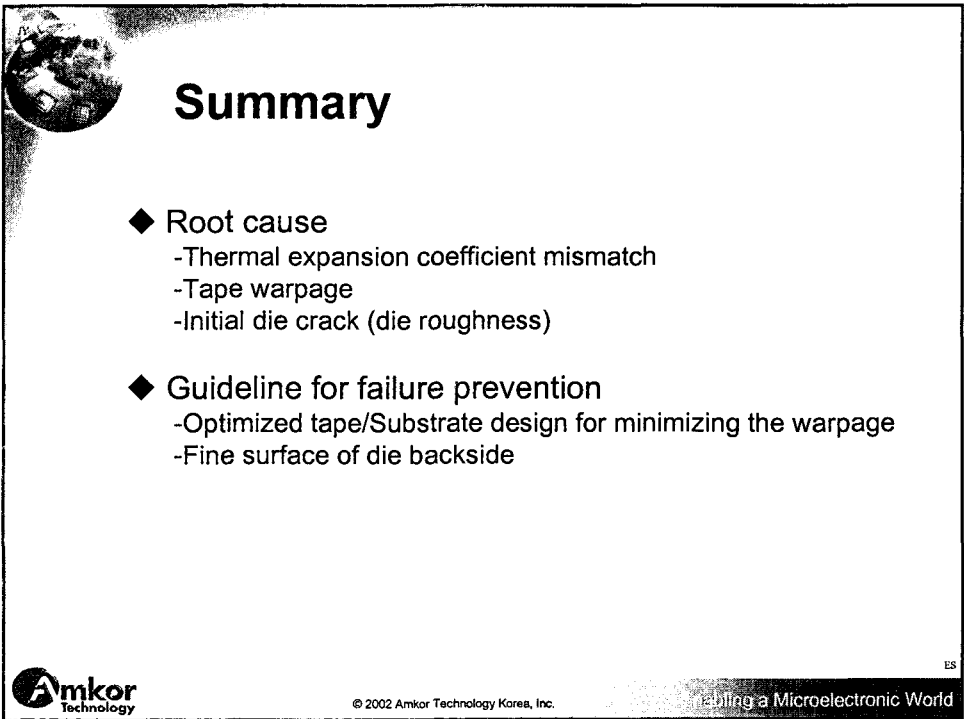
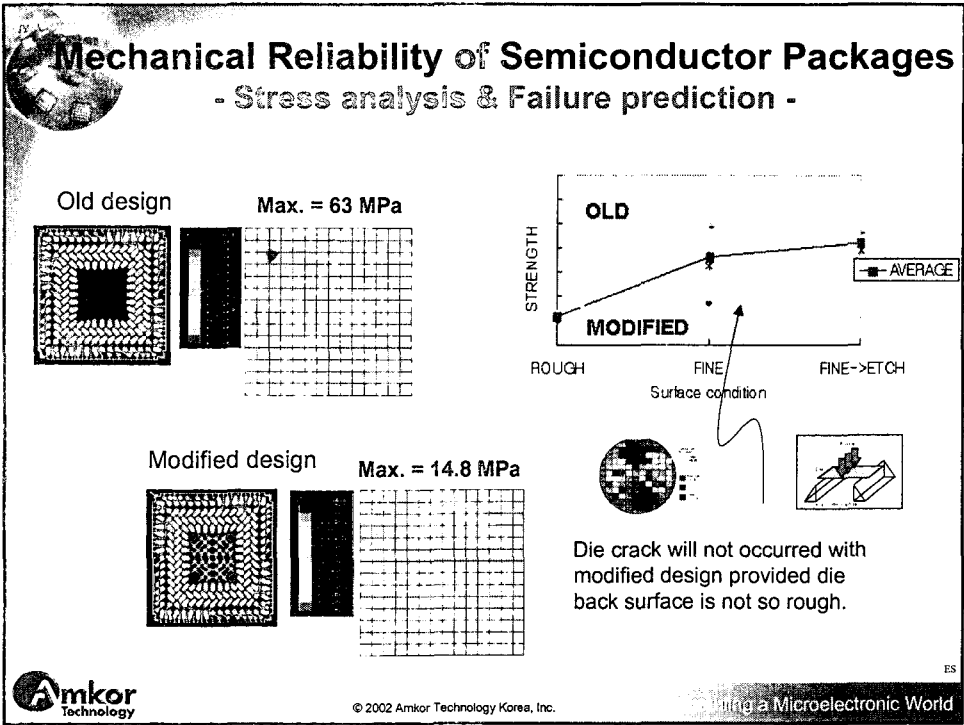
Adding dummy line
4% improve

Enhancement of Connection bar (x3 wider)
20.4% improve



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AGENDA

1. Die crack problem
- ➔ 2. Signal trace failure
3. Soder joint failure



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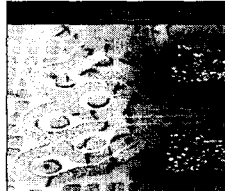
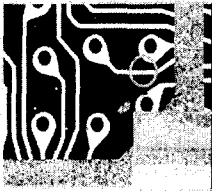
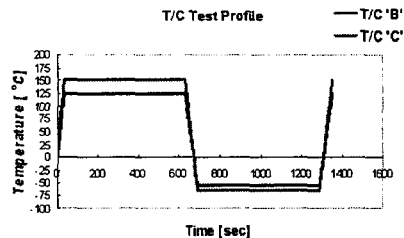
Mechanical Failures of Semiconductor Packages - Signal Trace Crack -

u Package type

- All kinds of laminate packages with fine pitch design

◆ Root cause

- Repetitive bending of a signal trace during temperature cycle
- Solder mask crack propagation



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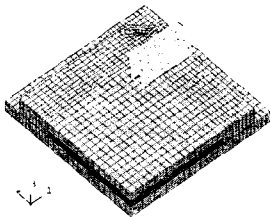
Mechanical Reliability of Semiconductor Packages

- Modeling Methodology -

- The pkg deformation during the T/C test is obtained using a Global model
- The plastic strain induced at the Cu trace under die is calculated using a Sub-model
- The fatigue life of Cu trace is predicted using low cycle fatigue equation

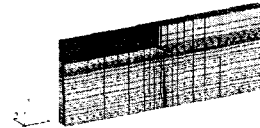
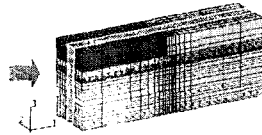
Global model

- To obtain the pkg's macro behavior
- 3-dimensional quarter model
- Effective property used for PCB substrate



Sub-model

- To obtain the plastic strain of Cu trace at the interested region
- Layer by layer real property used for PCB substrate
- Epoxy fillet feature considered
- Cu trace width modeling



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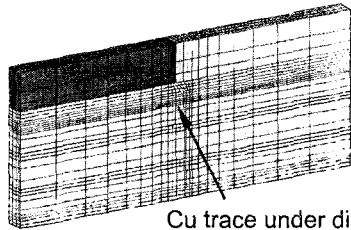
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Mechanical Reliability of Semiconductor Packages

- Deformation of Cu Trace During T/C Test -

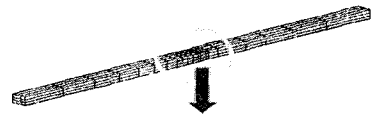
Side view of Cu trace in the Sub-model



Cu trace under die



T/C 'C' condition



Deformed Cu trace under die edge



Concentrated Plastic Strain

Deformation with x20 magnification factor



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Mechanical Reliability of Semiconductor Packages - Life Prediction -

Life Prediction Rule

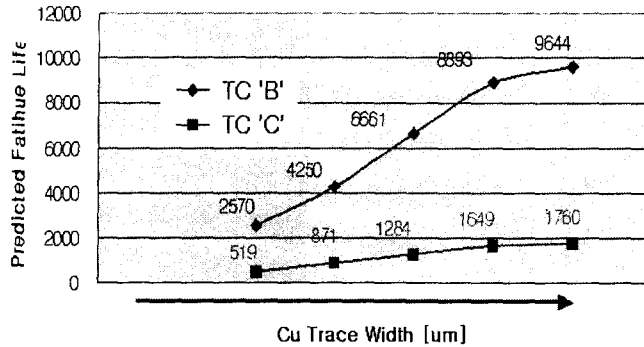
$$N_f^{-m} \times \epsilon_f^n = PSR$$

Where,

PSR = Plastic Strain Range

N_f = No of cycles-to-failure

ϵ_f = Fatigue ductility coefficient (ductility)



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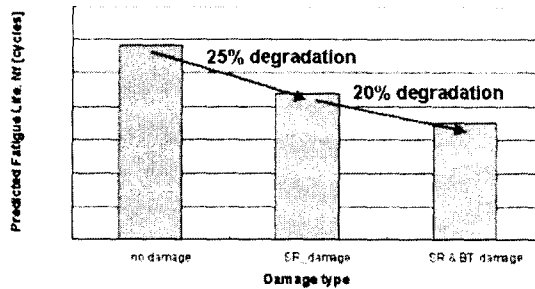
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Mechanical Reliability of Semiconductor Packages - SR damage effect-

Parameters : Initial damage around Cu trace



T/C 'C' condition
(-60 oC ~ 150 oC)



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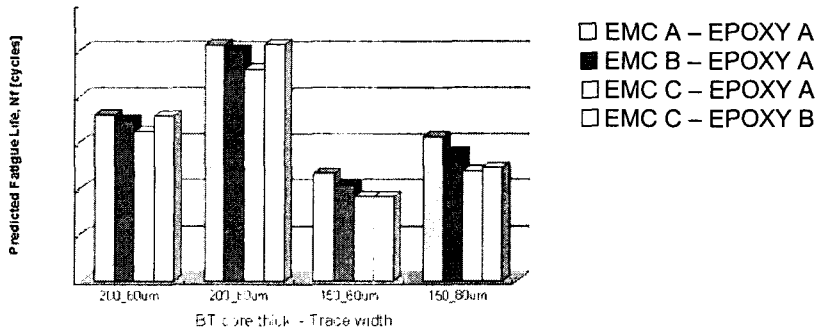
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Mechanical Reliability of Semiconductor Packages

- Material set, BT core thickness effect-

Parameters : Material set, BT core thick, Trace width



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Summary

- ◆ Root cause
 - Thermal expansion coefficient mismatch
 - Repetitive bending of a signal trace during TC cycle
 - Solder mask damage
- ◆ Guideline for failure prevention
 - Increase of trace width
 - Don't make signal trace passing the die edge
 - Proper material selection with thick substrate core



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AGENDA

1. Die crack problem
2. Signal trace failure
- ➔ 3. Soder joint failure



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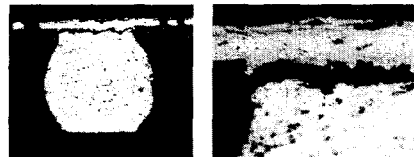
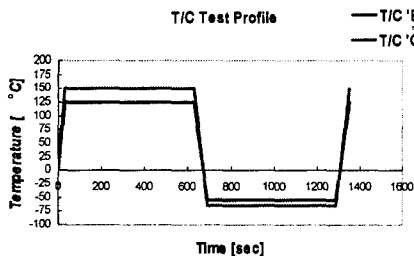
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Mechanical Failures of Semiconductor Packages - Creep-Fatigue Failure -

u Creep-fatigue failure

- $T > 0.3 T_m$ (melting temperature) : eutectic solder ($T_m=183\text{ }^\circ\text{C}$) : $\sim 50\text{ }^\circ\text{C}$
- material degradation : micro crack (Pb rich/Sn rich phase), coarsening
- Time dependent failure : ramp rate, hold time
- Accumulated creep strain is the main concern of failure
- Material structure is important ; eutectic/lead free solder



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Mechanical Failures of Semiconductor Packages

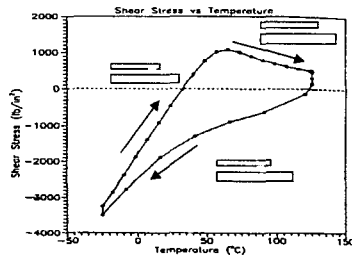
- Solder joint reliability -

◆ Failure Mechanism

- Displacement due to mismatch of the CTE
- Thermally induced displacement results in a high peel and shear stress near the bonded edges of joint
- Fatigue crack initiates at the bonded edges
- Crack propagates along the interface leading to failure of the bump

$$\text{CTE} = \alpha_2$$

$$\text{CTE} = \alpha_1$$



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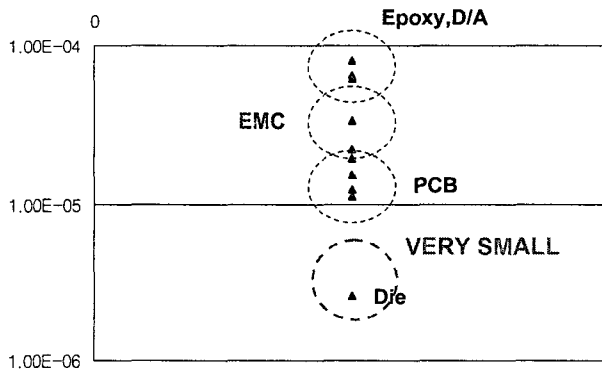
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Mechanical Failures of Semiconductor Packages

- CTE mismatch -

- ◆ CTE mismatch is the root cause of all kinds of the mechanical failure
- die crack/signal trace crack/solder joint crack



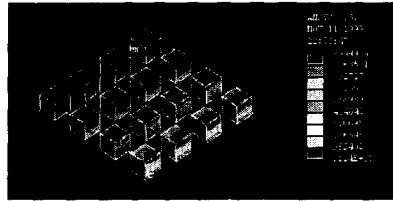
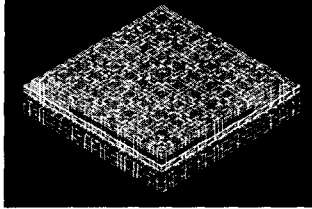
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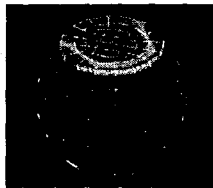
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Mechanical Reliability of Semiconductor Packages - Modeling Methodology -

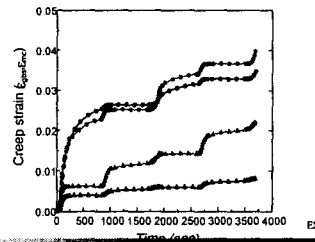
• Global Package Model



• Local Solder Joint Model



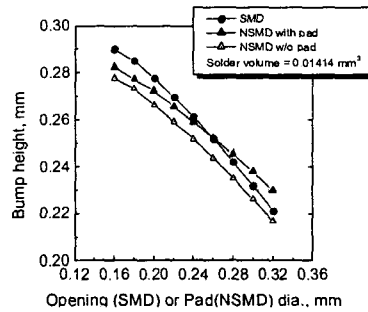
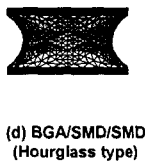
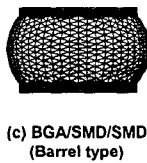
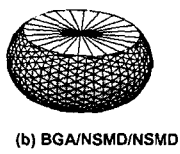
Accumulation of creep strain



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Mechanical Reliability of Semiconductor Packages - Solder shape prediction -

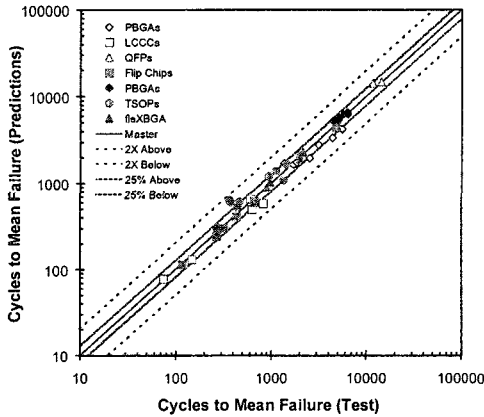


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Mechanical Reliability of Semiconductor Packages

- Life Prediction Model -



$$N_f = (\alpha \epsilon_{GBS} + \beta \epsilon_{MC})^{-1}$$

Where,

ϵ_{GBS} & ϵ_{MC} = Accumulated Creep Strains

N_f = Cycles to Mean Failure (N50)

First Failure is Estimated from Mean Life as

Prediction Accuracy : ± 25%

$$0.6N_f \leq \text{First Failure} \leq 0.7N_f$$



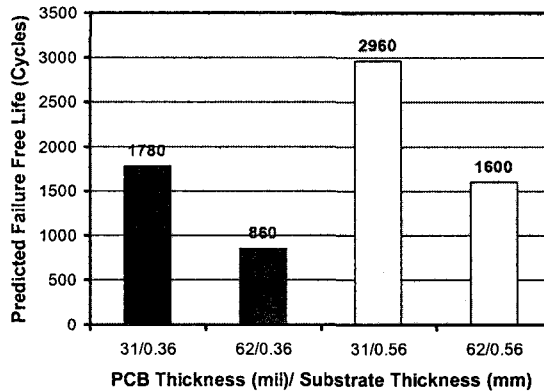
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Mechanical Reliability of Semiconductor Packages

- PBGA, PCB/Substrate thickness effect -

- 256 PBGA, 17 x 17 mm, 1.0 mm Pitch
 - Die Size = 11.5 mm
 - Solder Ball Size = 20 mils

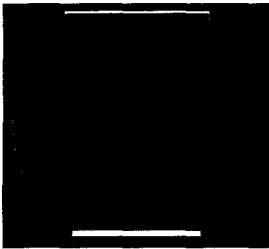
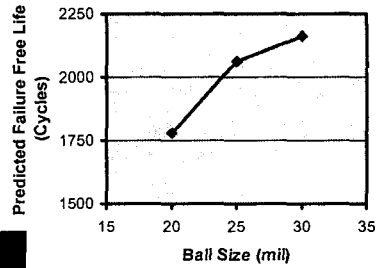


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Mechanical Reliability of Semiconductor Packages - PBGA, Solder ball size effect -

- 256 PBGA, 17 x 17 mm, 1.0 mm Pitch
 - Die Size = 11.5 mm
 - Substrate : 0.36 mm Thick, 2 Layer
 - PCB : 31 Mils Thick



30 Mils Ball
Diameter = 0.78 mm
Height = 0.70 mm



25 Mils Ball
Diameter = 0.66 mm
Height = 0.56 mm



20 Mils Ball
Diameter = 0.56 mm
Height = 0.375

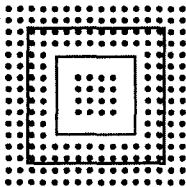


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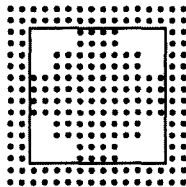
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Mechanical Reliability of Semiconductor Packages - PBGA, Ball array effect -

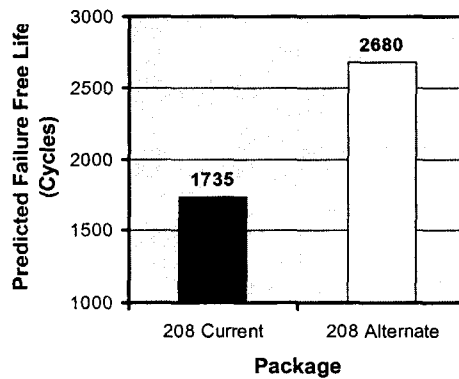
- Die : 11.5 mm
- PCB : 31 Mil Thick
- Substrate : 0.36 mm



For Die Size
<= 7 mm Sq.
Life > 2900 Cycles



For Die Size
> 7 mm Sq.



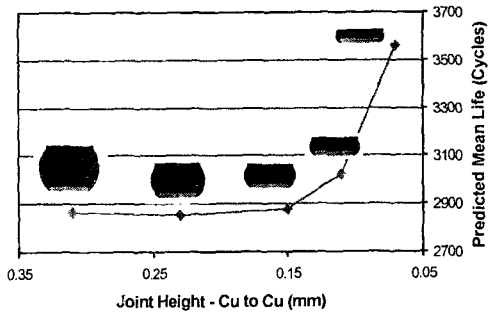
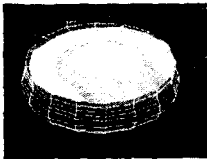
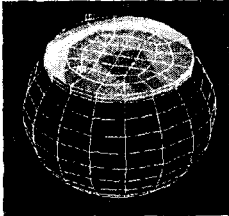
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Mechanical Reliability of Semiconductor Packages - LCA & BGA -

- Test Case: ChipArray BGA
 - 8mm-64 Lead, 0.8mm Pitch, 3.2mm Die
 - -40 <=> 125°C, 2 cycles/hour, 0.8mm Board



Depending on Assembly Stiffness (Thickness, Modulus, Sizes)
Tensile Load May Dominate Over Shear Load



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Mechanical Reliability of Semiconductor Packages - SMD & NSMD -

- SMD on Package Side
- NSMD on Package Side



- 3560 Cycles



- 12,650 Cycles

- > 3X Improvement in Life with NSMD Pad on Package Side
Solder Fillet on the Sides of Cu Pad Improves Reliability



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Summary

◆ Root cause

- Thermal expansion coefficient mismatch
- Creep deformation of solder joint (shear/normal)
- Material degradation

◆ Guideline for failure prevention

- Increase of solder ball size
- Proper selection of the PCB/Substrate thickness
- Optimal design of the ball array
- Solder mask opening type : NSMD
- In some case, LGA type is better



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Package characterization in Amkor

Electrical analysis

- R,L,C extraction
- Signal integrity
- RF design

Mechanical analysis

- Die cracking
- Warpage
- Interconnection failure
- Moisture induced failure
- Moldflow analysis

Thermal analysis

- Thermal parameter
- Natural/Force convection
- Optimal design of thermal management

Material DB

Methodology DB
Analysis procedure

Automation of
FE Analysis

Experimental analysis

- 2nd Reliability test
- Thermal test
- Material Test



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