

## 감쇠시스템을 위한 개선된 Sturm 수열 성질 Modified Sturm Sequence Property for Damped Systems

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### ABSTRACT

Most of the eigenvalue analysis methods for the undamped or proportionally damped systems use the well-known Sturm sequence property to check the missed eigenvalues when only a set of the lowest modes is to be used for large structures. However, in the case of the non-proportionally damped systems such as the soil-structure interaction system, the structural control system and the composite structures, no counterpart of the Sturm sequence property for undamped systems has been developed yet. Hence, when some important modes are missed for those systems, it may leads to poor results in dynamic analysis. In this paper, a technique for calculating the number of eigenvalues inside the open disk of arbitrary radius for the eigenproblem with the damping matrix is proposed by applying Chen's algorithm and Gleyse's theorem. To verify the applicability of the proposed method, two numerical examples are considered.

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### 1. INTRODUCTION

To obtain the dynamic response of a large civil structure, it is economic and efficient to superpose the results of a few lowest modes. Therefore, there has been proposed many eigensolution techniques which can find only a set of the lowest modes. The Lanczos and subspace method are belong to this type of technique. In these techniques, however, some important modes can be missed in the calculation process, which may lead to poor results in dynamic analysis. Hence, a checking technique for missed eigenvalues is required in finding the missed one. For the case of undamped system or proportionally damped system, it can be easily found by using the Sturm sequence property<sup>(1-4)</sup>.

However, in the case of the non-proportionally damped systems such as the soil-structure interaction system, the structural control system and composite structures, no counterpart of the Sturm sequence property for undamped systems has been developed yet<sup>(5)</sup>. Hence, when some important modes are missed for those systems, it may leads to poor results in dynamic analysis.

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A number of researchers<sup>(6,7)</sup> have been performed to solve the eigenproblem with the damping matrix, whereas there have been few studies on a technique to calculate the number of eigenvalues in this case in the literature. Jung et al.<sup>(8)</sup> proposed a technique of checking missed eigenvalues for eigenproblem with damping matrix using argument principle. This method requires a selection of checking points and the  $LDL^T$  factorization of the characteristic polynomial at those points. The accuracy of the method increases with the number of checking points, so it need more factorization processes to get more exact results.

In this paper, Gleyse's theorem<sup>(9)</sup>, which can count the number of zeros of a characteristic polynomial inside an open unit disk, is used to calculate the number of eigenvalues for eigenproblem with the damping matrix. The characteristic polynomial of an eigenvalue problem is determined by using Chen's algorithm<sup>(10)</sup> which is considered as both stable and effective. The determinants(minors) of the leading principal submatrices of order  $i$  in the Schur-Cohn matrix can be easily calculated by the  $LDL^T$  factorization process and the final result obtained is very similar to the Sturm sequence property for undamped systems.

This paper is organized as follows. The modified Sturm sequence property is presented and discussed in Chapter 2. In Chapter 3, a numerical example is analyzed to verify the effectiveness of the proposed method. Finally, the concluding remarks are expressed in Chapter 4.

## 2. MODIFIED STURM SEQUENCE PROPERTY FOR DAMPED SYSTEMS

### 2.1. The equations of motion of damped systems

In the analysis of dynamic response of structural system, the equation of motion of damped systems can be written as:

$$M\ddot{u}(t) + C\dot{u}(t) + Ku(t) = 0, \quad (1)$$

where  $M, K$  and  $C$  are the  $(n \times n)$  mass, stiffness and nonclassical damping matrices, respectively, and  $\ddot{u}(t)$ ,  $\dot{u}(t)$  and  $u(t)$  are the  $(n \times 1)$  acceleration, velocity and displacement vectors, respectively. To find the solution of the free vibration of the system, we consider the following quadratic eigenproblem:

$$\lambda^2 M \phi + \lambda C \phi + K \phi = 0, \quad (2)$$

in which  $\lambda$  and  $\phi$  are the eigenvalue and eigenvector of the system. There are  $2n$  eigenvalues for the system with  $n$  degrees of freedom and these occur either in real pairs or in complex conjugate pairs, depending upon whether they correspond to overdamped or undamped modes.

The common practice is to reformulate the quadratic system of equation to a linear one by doubling the order of the system<sup>(6,7)</sup> such as:

$$\begin{bmatrix} -K & 0 \\ 0 & M \end{bmatrix} \begin{Bmatrix} \phi \\ \lambda \phi \end{Bmatrix} = \lambda \begin{bmatrix} C & M \\ M & 0 \end{bmatrix} \begin{Bmatrix} \phi \\ \lambda \phi \end{Bmatrix} \quad (3)$$

In general,  $M$  and  $C$  nonsingular, that is,  $\det(M) \neq 0$  and  $\det(C) \neq 0$ , so the above equation can be changed

to the form of a standard eigenproblem:

$$A\psi = \lambda\psi, \quad (4)$$

where

$$A = \begin{bmatrix} 0 & I \\ -M^{-1}K & -M^{-1}C \end{bmatrix}, \psi = \begin{Bmatrix} \phi \\ \lambda\phi \end{Bmatrix}. \quad (5)$$

Observing the above Equation (5), when the mass matrix  $M$  is lumped or banded, the change to the standard eigenproblem can be accomplished without much increase in computing time. The characteristic polynomial of Equation (4) can be represented as:

$$P(\lambda) = \det(A - \lambda I) = a_{2n}\lambda^{2n} + a_{2n-1}\lambda^{2n-1} + \dots + a_1\lambda + a_0 = \sum_{i=0}^{2n} a_i\lambda^i = 0, \quad (6)$$

where  $\lambda$  is a complex value and  $a_i (i=0, 1, \dots, 2n)$  are the real coefficients.

## 2.2. The coefficient of the characteristic polynomial

Chen<sup>(10)</sup> suggested a stable algorithm to obtain the coefficients of the characteristic polynomial of a real square matrix. According to his algorithm some given matrix  $A$ :

$$A = \begin{bmatrix} a_{11} & a_{12} & \dots & a_{1,2n-1} & a_{1,2n} \\ a_{21} & a_{22} & \dots & a_{2,2n-1} & a_{2,2n} \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ a_{2n-1,1} & a_{2n-1,2} & \dots & a_{2n-1,2n-1} & a_{2n-1,2n} \\ a_{2n,1} & a_{2n,2} & \dots & a_{2n,2n-1} & a_{2n,2n} \end{bmatrix}, \quad (7)$$

can be transformed to  $\bar{A}$ :

$$\bar{A} = \begin{bmatrix} -a_{2n-1} & -a_{2n-2} & \dots & -a_1 & -a_0 \\ 1 & 0 & \dots & 0 & 0 \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \dots & 0 & 0 \\ 0 & 0 & \dots & 1 & 0 \end{bmatrix}, \quad (8)$$

by applying a sequence of Gauss-elimination like similarity transformations. When some numerical instability occurs during the transformations, modified algorithm by Chen<sup>(10)</sup> can be used. Since  $\bar{A}$  was obtained by applying similar transformations to  $A$ , the eigenvalues and eigenvectors of both  $\bar{A}$  and  $A$  are same. The characteristic polynomial of  $A$ ,  $P(\lambda) = \det(A - \lambda I)$  can be obtained by observing the transformed matrix  $\bar{A}$ , and the characteristic polynomial is:

$$P(\lambda) = \det(A - \lambda I) = \det(\bar{A} - \lambda I) = \lambda^{2n} + a_{2n-1}\lambda^{2n-1} + \dots + a_1\lambda + a_0 = 0, (a_{2n} = 1). \quad (9)$$

## 2.3. The number of eigenvalues in an open unit disk.

Glyse<sup>(9)</sup> suggested a method of checking the number of eigenvalues of a real polynomial inside an open

unit disk by a determinant representation.

Let  $P(\lambda) = \sum_{h=0}^{2n} a_h \lambda^h = 0$  ( $a_h$  is a real number) then the number of eigenvalues inside the open unit disk can be determined as:

$$N_\lambda = 2n - S[1, d_1, d_2, \dots, d_{2n}] \quad (10)$$

where  $N_\lambda$  is the number of eigenvalues in an open unit disk,  $2n$  is the degree of the polynomial,  $S[k_0, k_1, k_2, \dots, k_{2n}]$  is the number of sign changes in the sequence  $k_i (i=0, 1, \dots, 2n)$  and  $d_i (i=1, 2, \dots, 2n)$  is the determinants (minors) of the leading principal submatrices of order  $i$  in the Schur-Cohn matrix  $T$ :

$$T = \begin{bmatrix} \cdot & \cdot & & \\ & t_{ij} & & \\ & & \cdot & \\ & & & \cdot \end{bmatrix}, t_{ij} = \sum_{h=0}^{\min(i,j)} (a_{2n-i+h} a_{2n-j+h} - a_{i-h} a_{j-h}) \quad (11)$$

The process of calculating the number of eigenvalues using the above theorem requires the calculation of the characteristic polynomial of a given matrix, the construction of the Schur-Cohn matrix  $T$  and the calculation of the determinants (minors) of the leading principal submatrices of order  $i$  in the Schur-Cohn matrix  $T$ . The coefficients of the characteristic polynomial of a given matrix can be determined by applying previous Chens algorithm, and by using these coefficients, each elements of the Schur-Cohn matrix can be obtained using Equation (11). The determinants (minors) of the leading principal submatrices of order  $i$  in the Schur-Cohn matrix  $T$  can be easily determined by applying  $LDL^T$  factorization of  $T$ , which is described in the following section.

#### 2.4. Modified Sturm sequence property.

Glyse's theorem<sup>(9)</sup> considers only about the number of eigenvalues in an open unit disk. To apply his theorem for an open disks of arbitrary radius  $\rho$ , substitute  $\lambda = \rho \bar{\lambda}$  ( $\rho$  is an real number) to Equation (6), then:

$$\begin{aligned} P(\bar{\lambda}) &= a_{2n} \rho^{2n} \bar{\lambda}^{2n} + a_{2n-1} \rho^{2n-1} \bar{\lambda}^{2n-1} + \dots + a_1 \rho \bar{\lambda} + a_0 \\ &= \bar{a}_{2n} \bar{\lambda}^{2n} + \bar{a}_{2n-1} \bar{\lambda}^{2n-1} + \dots + \bar{a}_1 \bar{\lambda} + \bar{a} = \sum_{i=0}^{2n} \bar{a}_i \bar{\lambda}^i = 0, \end{aligned} \quad (12)$$

where  $\bar{a}_i = a_i \rho^i (i=0, 1, \dots, 2n)$  are modified coefficients.

Using the modified coefficients  $\bar{a}_i (i=0, 1, \dots, 2n)$  in Equation (12), His theorem can be extended to calculate the number of eigenvalues in the open disks of arbitrary radius  $\rho$ . The calculation of  $d_i (i=1, 2, \dots, 2n)$  can be easily performed by the  $LDL^T$  factorization of the Schur-Cohn matrix  $T$ . If  $T = LDL^T$ , then:

$$T_i = L_i D_i L_i^T \quad (13)$$

where  $T_i$  is the leading principal submatrices of order  $i$  in the  $T$ ,  $L_i$  is the leading principal submatrices of order  $i$  in the  $L$  and  $D_i$  is the leading principal submatrices of order  $i$  in the  $D$ . Therefore each  $d_i (i=1, 2, \dots, 2n)$  can be easily obtained as:

$$\begin{aligned} d_i &= \det(T_i) = \det(L_i D_i L_i^T) = \det(D_i) \\ &= d_{11} \times d_{22} \times \dots \times d_{ii} = \prod_{h=1}^i d_{hh} \end{aligned} \quad (14)$$

Considering Equation (10), we only need to know the signs of each  $d_i$  because the unknown value of  $S[1, d_1, d_2, \dots, d_{2n}]$  depends only on sign changes of each  $d_i (i=1, 2, \dots, 2n)$  and from Equation (14) the signs of each  $d_i$  can be determined from the number of negative elements of each diagonal elements of  $D_i$ , which is very similar to Sturm sequence property for undamped systems.

### 3. A NUMERICAL EXAMPLE

To show the effectiveness of the proposed method, two numerical examples are analyzed. First, a simple spring-mass-damper system that has the exact analytical eigenvalues is considered to verify that the proposed method can exactly calculate the number of eigenvalues in the open disk of arbitrary radius for the eigenproblem with the damping matrix.

#### 3.1. Simple Spring-Mass-Damper System<sup>(11)</sup>

The finite element discretization of the system results in a diagonal mass matrix, a tridiagonal damping and stiffness matrices of the following forms:

$$M = mI \quad (15)$$

$$C = \alpha M + \beta K \quad (16)$$

$$K = k \begin{bmatrix} 2 & -1 & & & \\ -1 & 2 & -1 & & \\ & -1 & \ddots & \ddots & \\ & & \ddots & 2 & -1 \\ & & & -1 & 1 \end{bmatrix} \quad (17)$$

where  $\alpha$  and  $\beta$  are the damping coefficients of the Rayleigh damping. The analytical solutions can be resulted through following relationships:

$$\lambda_{2i-1, 2i} = -\xi_i \omega_i + j\omega_i + \sqrt{1 - \xi_i^2} \quad \text{for } i=1, \dots, n \quad (18)$$

$$\xi_i = \frac{1}{2} \left( -\frac{\alpha}{\omega_i} + \beta \omega_i \right) \quad (19)$$

$$\omega_i = 2\sqrt{\frac{m}{k}} \sin \frac{2i-1}{2n+1} \frac{\pi}{2} \quad (20)$$

where  $\omega_i$  and  $\xi_i$  are the undamped natural frequency and modal damping ratio, respectively.

A system with order 10 is used in analysis. The  $k$  and  $m$  are 1, and the coefficients,  $\alpha$  and  $\beta$ , of the Rayleigh damping are 0.05 and 0.5, respectively. All the eigenvalues and their radius from the origin in the complex plane are as in Table I. In this example the checking process performed for open disks of three different radius. First two cases are for checking in between eigenvalues. Their location is selected considering the relative distances between two adjacent eigenvalues except for a conjugate eigenvalues, and two eigenvalues with smaller distances from the next are selected. The third is for checking the number of all the eigenvalues of the system. The radius of the open disk is should be only a bit larger than the selected eigenvalue to ensure that the next eigenvalue is not within the open disk. The Sturm sequence check proposed by Bathe<sup>(1)</sup> has used 1.01 times the magnitude of the largest known eigenvalue for the eigenproblem without the damping matrix. However, according to Jung et al.<sup>(8)</sup>, the value used by Bathe is too large to ensure that the next largest eigenvalue is not within the open disk, and recommended times the magnitude of the largest known eigenvalue. In this example, therefore, the radius  $\rho$  of the open disk is chosen by 1.005 times the magnitude of the largest eigenvalue ( $\rho = 1.005|\lambda|$ ). For each cases the calculated coefficient of the characteristic polynomial  $\overline{a}_i$ , diagonal element  $d_{ii}$ , and sign of  $d_i$  are as in Table I. Using the sign of  $d_i$  Table I, the number of eigenvalues for each cases are calculated as followings:

Case 1:  $\rho = 1.005|\lambda_{16}| = 1.8109$

$$N_\lambda = 2n - S[1, d_1, d_2, \dots, d_{2n}]$$

$$N_\lambda = 20 - 4 = 16$$

Case 2:  $\rho = 1.005|\lambda_{18}| = 1.9207$

$$N_\lambda = 2n - S[1, d_1, d_2, \dots, d_{2n}]$$

$$N_\lambda = 20 - 2 = 18$$

Case 4:  $\rho = 1.005|\lambda_{20}| = 1.9875$

$$N_\lambda = 2n - S[1, d_1, d_2, \dots, d_{2n}]$$

$$N_\lambda = 20 - 0 = 20$$

Referring to Table II, the number of eigenvalues which is inside open disks of radius  $\rho=1.005|\lambda_{16}|=1.8109$ ,  $\rho=1.005|\lambda_{18}|=1.9207$  and  $\rho=1.005|\lambda_{20}|=1.9875$  are 16, 18 and 20 which are exactly agree with the calculated values. As seen from this result, therefore, we verify that the proposed method can exactly check the number of eigenvalues inside some open disk of arbitrary radius.

Table I. The calculated eigenvalues, characteristic coefficient  $\bar{a}_i$  and sign of  $d_i$

i	Eigenvalues( $\lambda$ )		Radius ( $\rho= \lambda $ )	$\rho=1.005 \lambda_{16} =1.8109$		$\rho=1.005 \lambda_{18} =1.9207$		$\rho=1.005 \lambda_{20} =1.9875$	
	Real	Imaginary		$\bar{a}_i$	$sign(d_i)$	$\bar{a}_i$	$sign(d_i)$	$\bar{a}_i$	$sign(d_i)$
0	-	-	-	3.079e-04	+	2.055e-04	+	1.618e+00	+
1	-0.0306	-0.1463	0.1495	4.322e-03	+	3.059e-03	+	2.492e+00	+
2	-0.0306	0.1463	0.1495	8.065e-02	+	6.055e-02	+	5.104e+00	+
3	-0.0745	-0.4388	0.4450	6.252e-01	+	4.979e-01	+	4.343e+00	+
4	-0.0745	0.4388	0.4450	4.147e+00	+	3.503e+00	+	3.161e+00	+
5	-0.1585	-0.7133	0.7307	1.947e+00 *	+	1.745e+01	+	1.629e+01	+
6	-0.1585	0.7133	0.7307	7.601e+01	+	7.222e+01	+	6.979e+01	+
7	-0.2750	-0.9614	1.0000	2.373e+02	+	2.391e+02	+	2.391e+02	+
8	-0.2750	0.9614	1.0000	6.251e+02	+	6.681e+02	+	6.913e+02	+
9	-0.4137	-1.1763	1.2470	1.374e+03	+	1.558e+03	+	1.668e+03	+
10	-0.4137	1.1763	1.2470	2.581e+03	+	3.104e+03	+	3.439e+03	+
11	-0.5624	-1.3540	1.4661	4.111e+03	+	5.242e+03	+	6.011e+03	+
12	-0.5624	1.3540	1.4661	5.610e+03	+	7.588e+03	+	9.002e+03	+
13	-0.7077	-1.4932	1.6525	6.495e+03	-	9.318e+03	+	1.144e+04	+
14	-0.7077	1.4932	1.6525	6.395e+03	+	9.731e+03	+	1.236e+04	+
15	-0.8368	-1.5959	1.8019	5.261e+03	+	8.491e+03	+	1.116e+04	+
16	-0.8368	1.5959	1.8019	3.592e+03	+	6.149e+03	+	8.365e+03	+
17	-0.9381	-1.6651	1.9111	1.960e+03	-	3.558e+03	-	5.008e+03	+
18	-0.9381	1.6651	1.9111	8.325e+02	+	1.603e+03	+	2.335e+03	+
19	-1.0028	-1.7046	1.9777	2.446e+02	+	4.996e+02	+	7.529e+02	+
20	-1.0028	1.7046	1.9777	4.429e+01	+	9.595e+01	+	1.496e+02	+

\*  $sign(d_i)$  represents the sign of  $d_i$ , so  $sign(d_i)$  is '+' when  $d_i > 0$  and  $sign(d_i)$  is '-' when  $d_i < 0$ .  
 $d_0$  is defined as equal to 1.

#### 4. CONCLUSIONS

A technique of calculating the number of eigenvalues inside an open disk of arbitrary radius was given. The technique is based on Chens algorithm and Gleyse's theorem and can be used to check the missed eigenvalues for the eigenproblem with damping matrix. By analyzing the numerical examples, it is verified that the proposed method can exactly check the number of eigenvalues for distinct or multiple eigenvalues for damped systems.

The technique by Jung et al. should find the variation of arguments of complex numbers along a

predefined path. Therefore, a large number of checking points should be used to obtain accurate result. However, the proposed method can exactly find the number of eigenvalues by performing the factorization process only once. In result, much effort in finding the number of eigenvalue of larger structures with damping matrix can be eliminated by the proposed method.

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