
역삼투막의 제조 및 최근 동향



구자영박사

((주) 새한)

RO MEMBRANES : History,Fabrication and Application

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SAEHAN INDUSTRIES INC

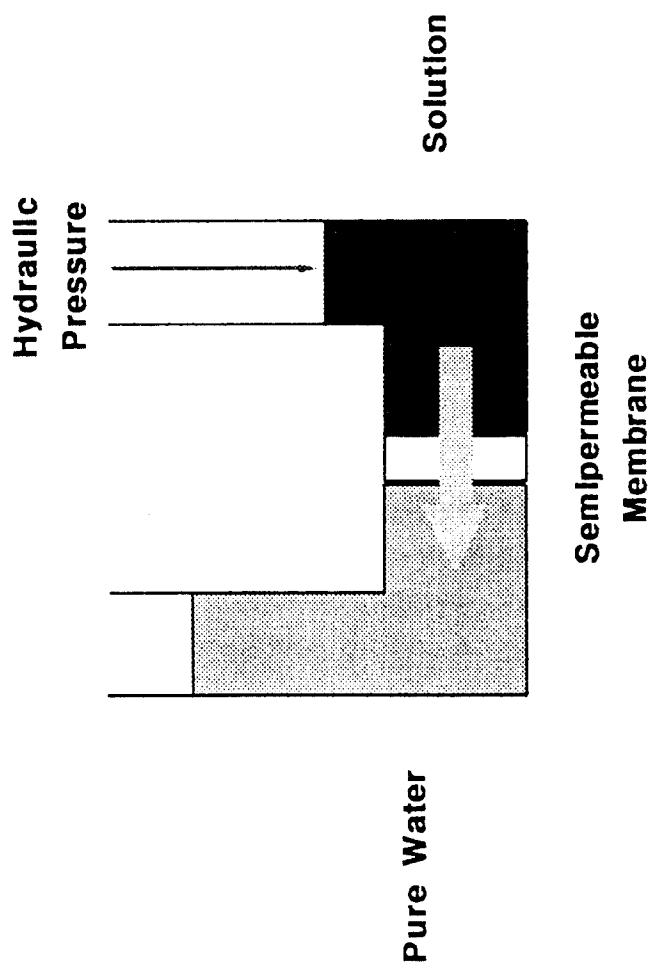


MEMBRANE SELECTIVITY

Range	Electron Microscopy	Optical Microscopy	Visible to Naked Eye			
	Ionic Range	Molecular Range	Macro Molecular Range	Micro Particle Range	Macro Particle Range	
Micrometer	10^{-3}	10^{-2}	10^{-1}	1	10	100
Angstrom	10	10^2	10^4	10^4	10^5	10^6
Molecular Weight	100	1000	100000			
Particle Type	Sugars	Carbon Black	Paint Pigment	Bacteria	Human Hair	Sand
	Pyrogen		Oil Emulsions	Virus		
	Soluble Salts		Colloids	Proteins / Enzymes		
	Metal Ions					
Membrane Type	Reverse Osmosis	Nanofiltration	Microfiltration	Ultrafiltration	Particle Filtration	

역삼투 현상

REVERSE OSMOTIC FLOW

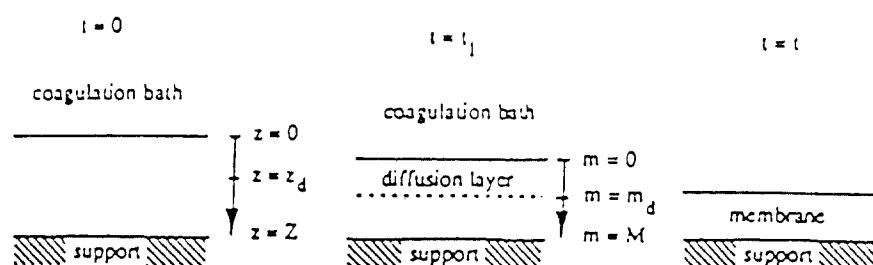
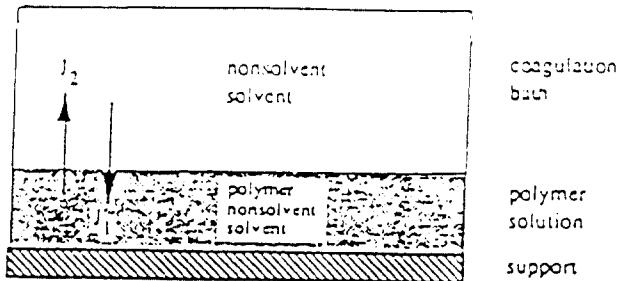


주식회사 미한

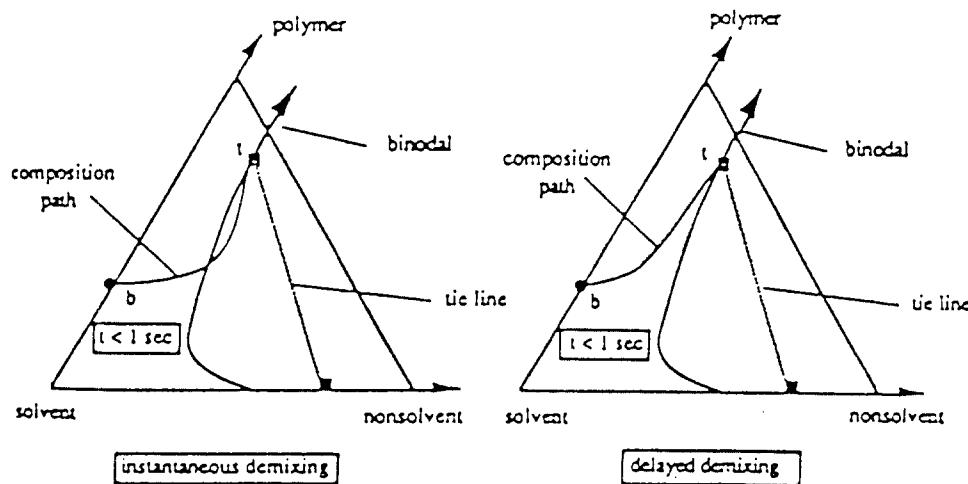
History of RO membrane

Year	Events	
1959	① Reid & Breton : Demonstration of desalination capability of cellulose acetate film	
1963	② Loeb & Sourirajan : Development of asymmetric cellulose acetate reverse osmosis membrane	UCLA
1965	③ Riley,Lonsdale : Elucidation of asymmetric CA membrane structure and proposal of solution-diffusion transport model.	
1966	④ Francis : Cellulose acetate thin film composite membrane concept	North Star
1972	⑤ John Cadotte : Interfacially synthesized thin film composite membrane NS-100 (PEI + TDI)	North Star R&D Institute
1978	⑥ John Cadotte : Fully aromatic polyamide thin film composite membrane	Filmtec
1982	⑦ Filmtec (J. Cadotte) Marketed "FT-30"	R : 98% FLUX : 25 GFD
1985	Dow purchase Filmtec	
1992	⑧ Dow Lost right of US patent 4,277,344 in lawsuit by Hydranautics and Fluid-systems	
1994	⑨ SAEHAN: Developed TFC type RO membrane.	R : 99% FLUX : 35 GFD
1995	⑩ Hydranautics : Marketed High flux membrane "ES-10" ESDA	R : 99% FLUX : 45 GFD
1997	⑪ SAEHAN: Developed High flux membrane "CSM-BL"	R : 99% FLUX : 50 GFD

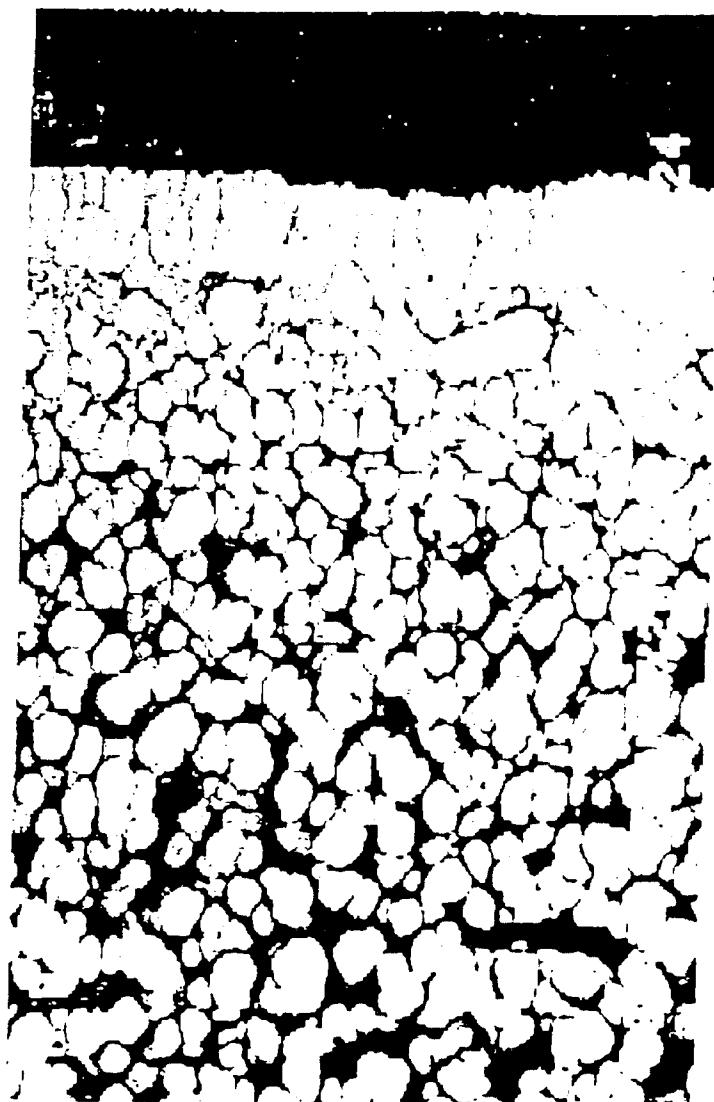
Phase Inversion Process



Schematic representation of the diffusional processes occurring after immersion in a quench medium
 [from M.H.V. Mulder, "Basic Principles of Membrane Technology", Kluwer Academic Publishers (1991), p.86,91]



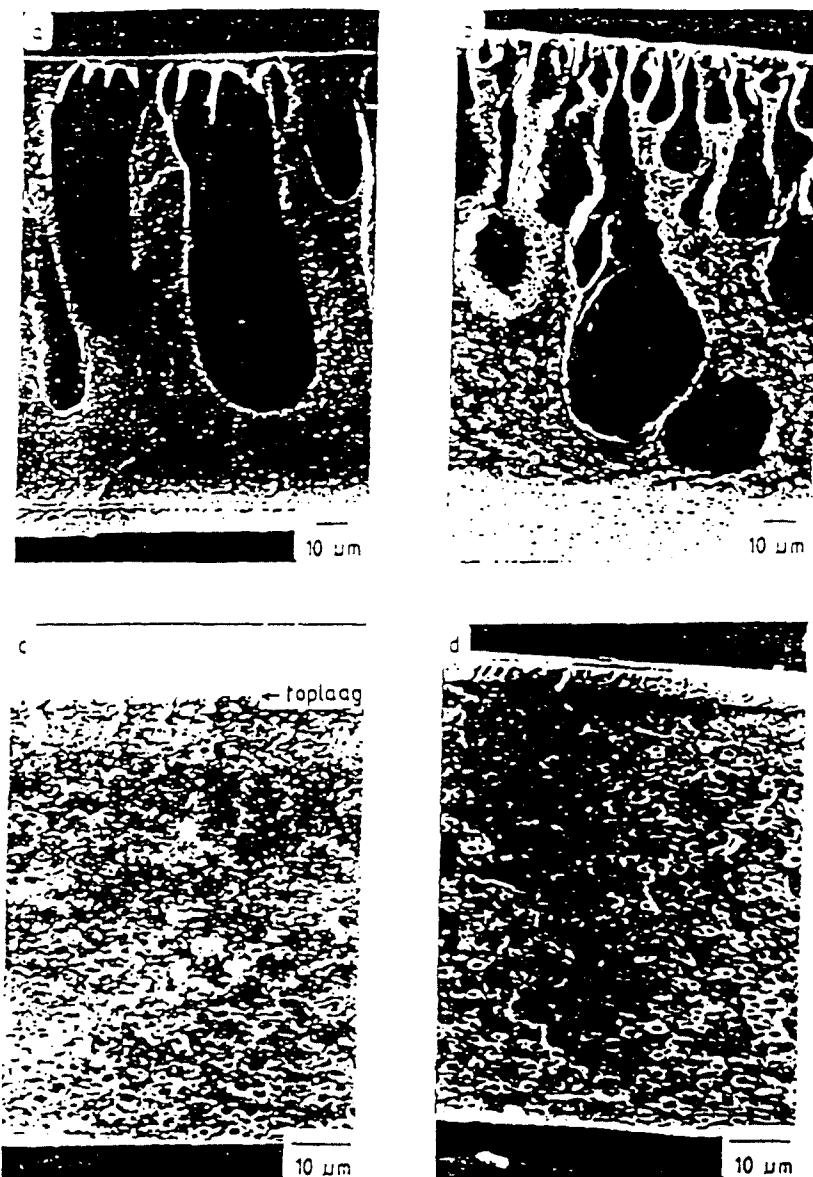
Schematic representation of the compositional change of a cast film at the quench bath-film interface immediately after immersion
 [from M.H.V. Mulder, "Basic Principles of Membrane Technology", Kluwer Academic Publishers (1991), p.93]



← Ultrathin Barrier Layer
(0.05 - 0.5 μm)

← Microporous Layer
(40 - 100 μm)

RO 단면
III



Cross-sections of cellulose acetate membranes prepared from 15 vol% CA casting solutions in different solvents immersed in pure water.
 a) DMF (instantaneous L-L demixing); b) dioxane (instantaneous L-L demixing);
 c) acetone (delayed L-L demixing); d) THF (delayed L-L demixing)
 [from B. Reuvers, Ph.D. Thesis, University of Twente, The Netherlands (1987)]

Drawbacks of CA Asymmetric membranes

- 1.Low Flux($2 \sim 5$ gfd) and Low Rejection(96 ~ 98%)
- 2.Narrow operating pH Range : pH 4.5 ~ 7.5
- 3.Weak to Biological attack
- 4.Prone to Compaction at High pressure(> 400psi)
- 5.Prone to Compaction at High temperature(> 35°C)
- 6.Prone to create defects during phase inversion
- 7.Once Fouled, No easy means of cleaning
- 8.Becomes expensive when expensive polymers are used

One advantage of CA membranes

- 1.Chlorine tolerant up to 1ppm Cl for continuous operation
2. low cost.

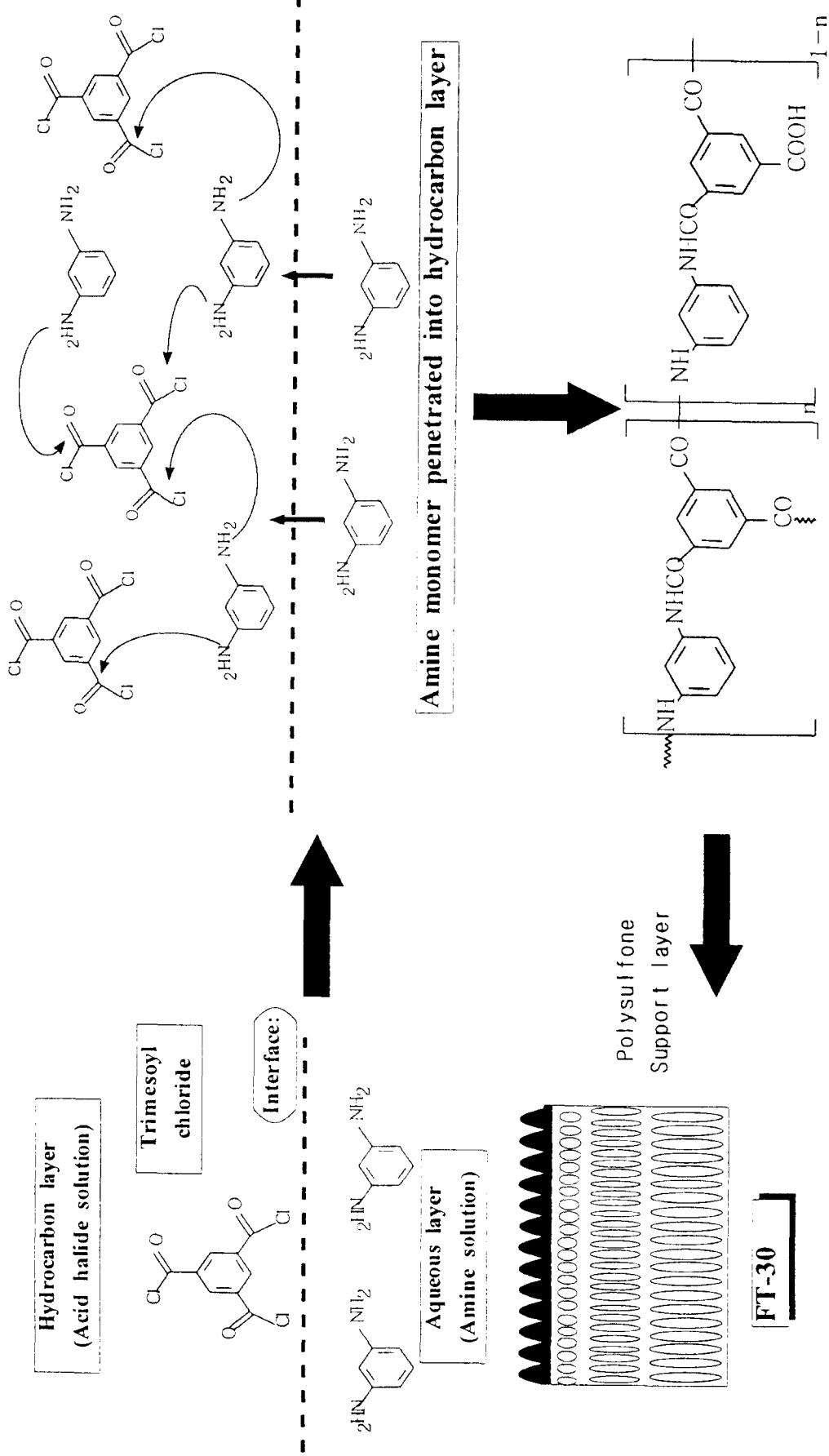
Other Asymmetric Membranes

- ◎ Asymmetric membrane from aromatic polyamide (Nomex, ~~B-9~~ ~~B-10~~ DuPont) solved the problems of narrow pH range and microbial attack, but was not chlorine tolerant.
- ◎ Cellulose Triacetate membrane showed better pH stability and higher salt rejection than CA.
- ◎ Polybenzimidazole and Polybenzimidazolone.
- ◎ Solved pH stability, microbial attack and chlorine damage problems, but the polymers were expensive and salt rejection was not as good as CA membrane.

Composite membrane

1. lamination
2. interfacial poly.
3. dip-coating of polymer solute
4. dip-coating of monomer + reaction
5. plasma

Schematic diagram of Interfacial polymerization(FT-30)



% REJECTION COMPARISONS

Substance	Cellulosic(%)	Thin-film(%)
Monovalent ions	95 ~ 97	95 ~ 99+
Divalent ions	>99	>99
Dissolved gases	None	None
Dissolved silica	85	90 ~ 99
Colloidal silica	100	100
Nitrates	85	95
Particles & Bacteria	100	100
Large Organics	100	100
Overall	96	98+

**Structure and Property Relationship of TFC Membranes
from various Diamines**

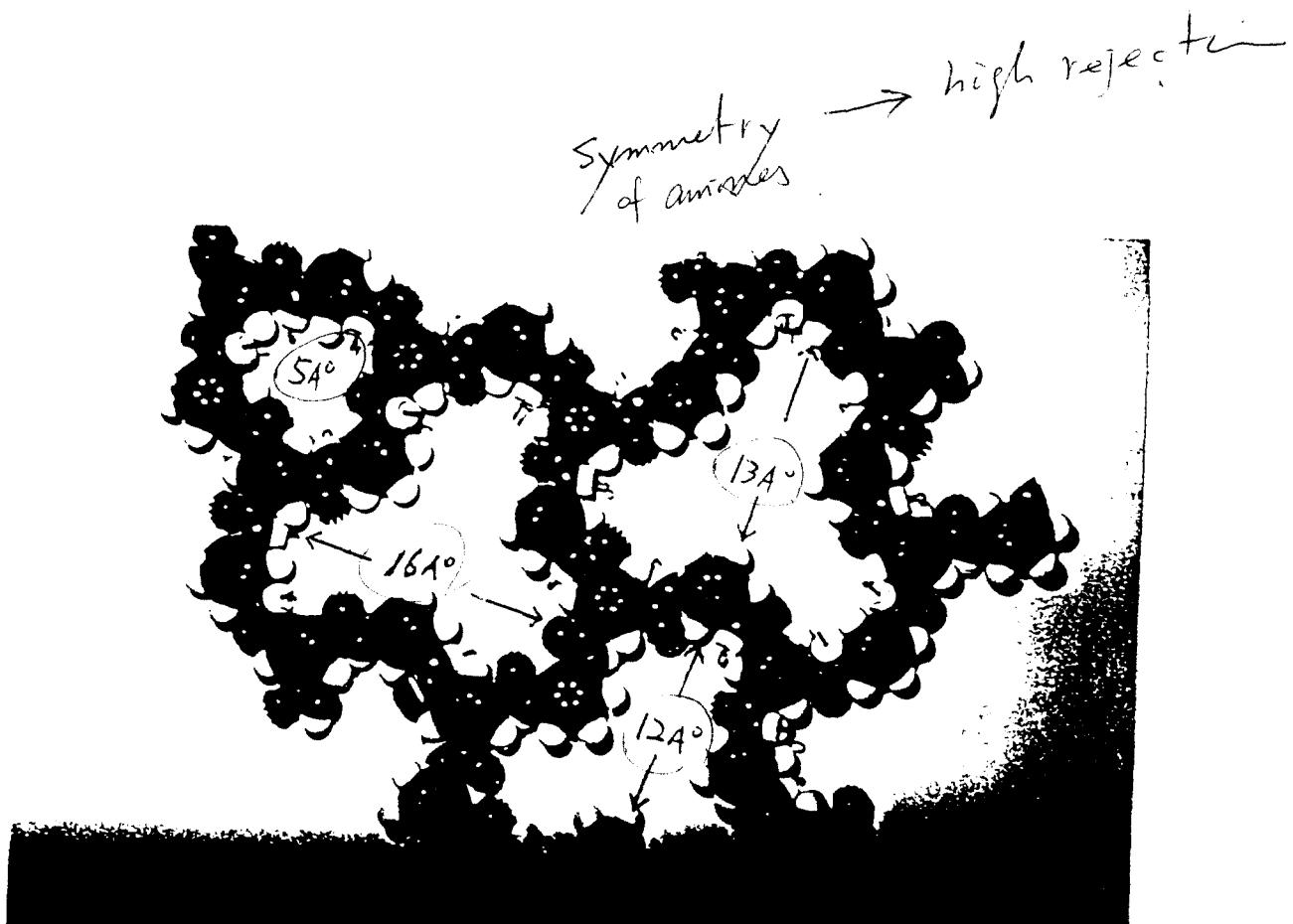
Diamines	Flux(gfd)	Rejection(%)
1,2-Ethylenediamine	1~6	95~97
1,3-Cyclohexane bis(methylamine)	11~14	85~94
1,4-Cyclohexanediamine	15~36	71~81
1,3-Phenylenediamine (FT-30)	25~30	98~99

(TEST Condition 225psi 0.2% NaCl solution)

◎Pore size and Flux
↓ pore size ↓

1,2-Ethylenediamine < 1,3-Cyclohexanebis(methylamine) < 1,3-Phenylenediamine < 1,4-Cyclohexanediamine

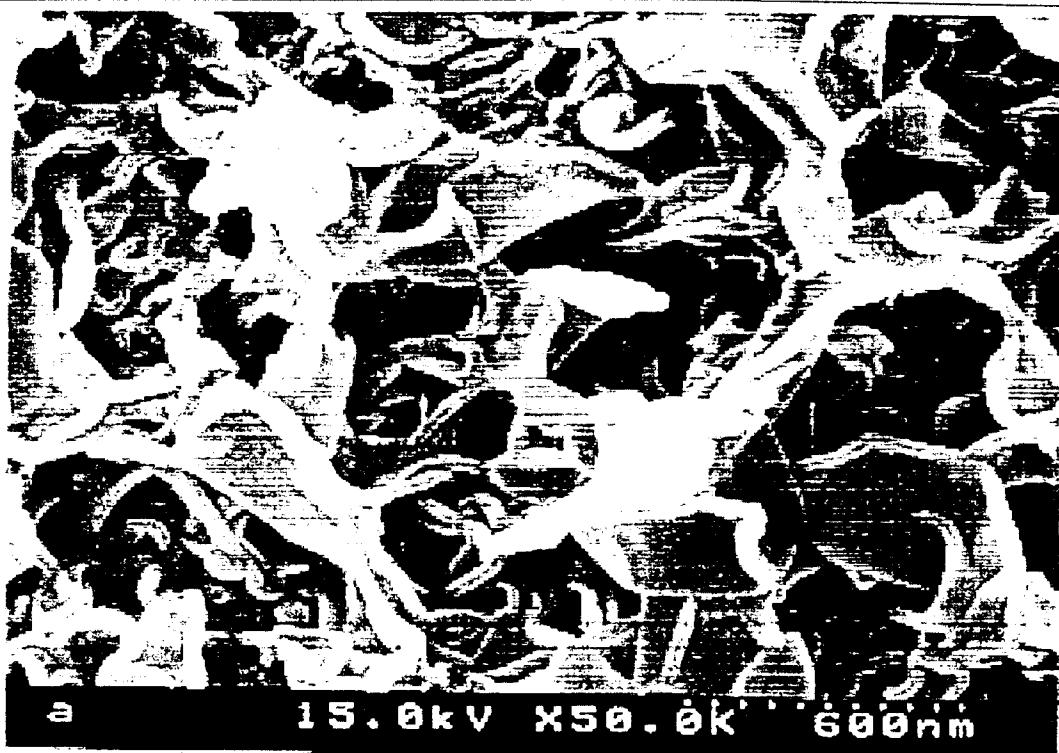
* effects of acid aldehydes on film properties



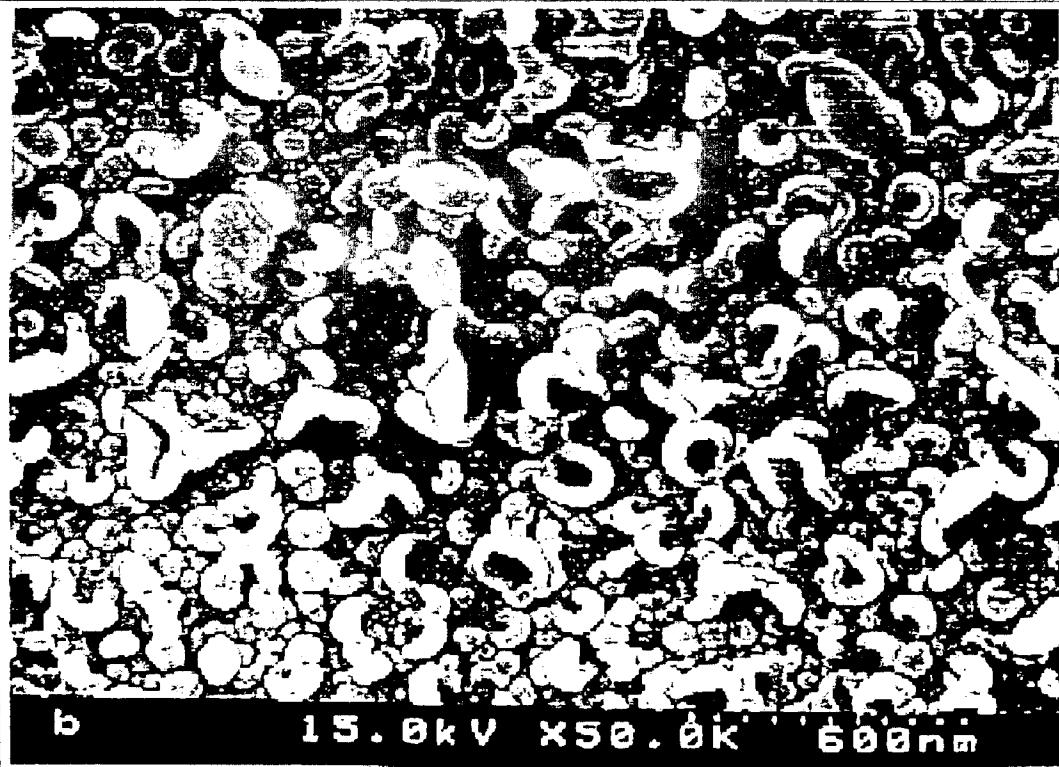
CPK Model of FT - 30 (JMS. Ippi, M. Hirase)

Field Emission SEM

High
Flux
Membrane

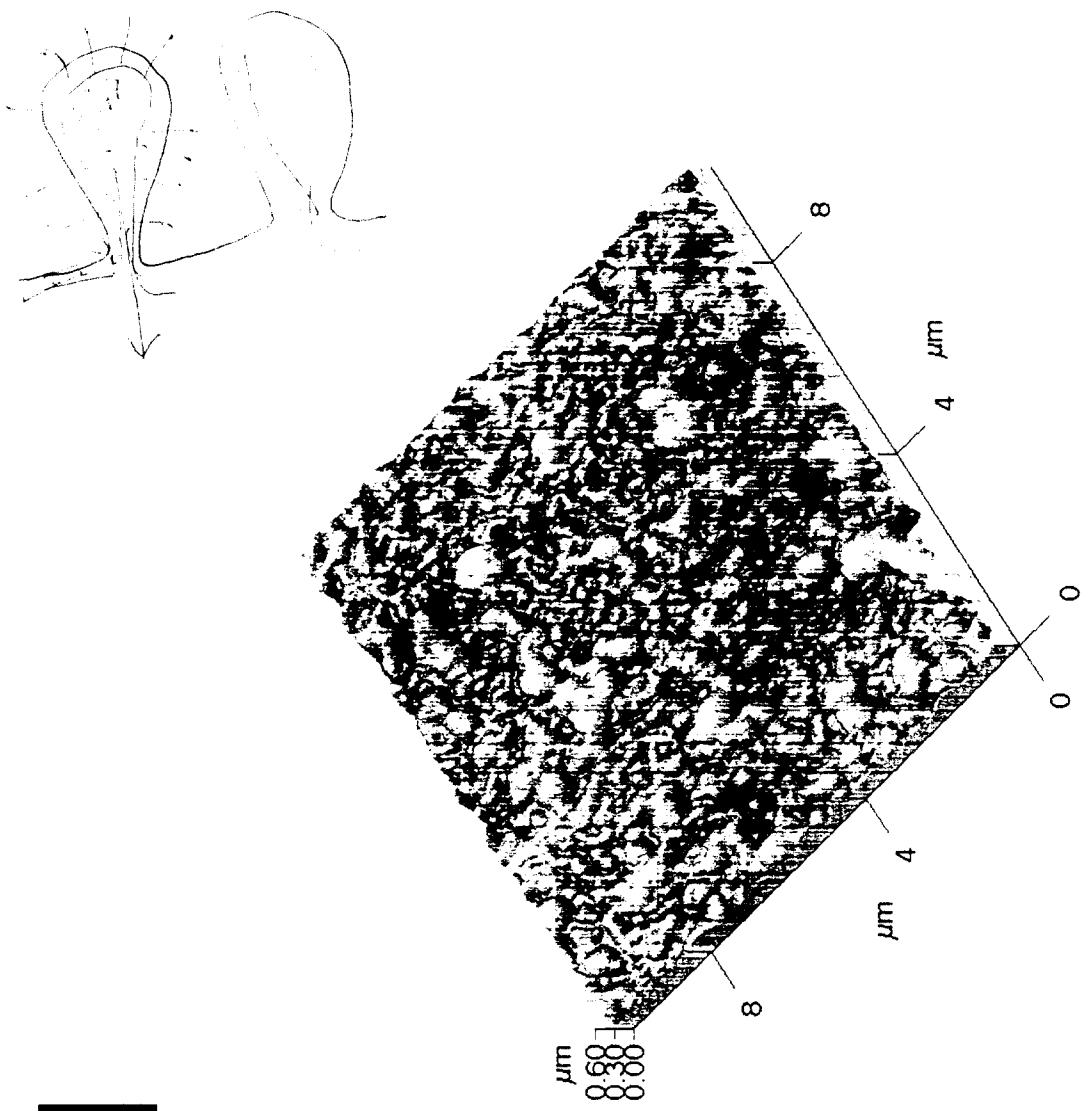


Regular
Flux
Membrane



AFM

High Flux Membrane



RO Membrane Materials and Manufacturers

- Cellulose Acetate

Desal, Koch Membrane System, Fluid system,
Hydranautics/Nitto-Denko, PCI, Stork and Toray

- Cellulose Triacetate

Toyobo

- Aromatic Polyamide

B-9, B-10, B-15(DuPont)

- Crosslinked Aromatic Polyamide

FT-30(FilmTec/Dow), TFCL(Fluid-systems)
UTC(Toray), CPA and ES-10(Hydranautics/Nitto-Denko)

- Polypiperazineamide

NF-40(Filmtec/Dow), SU-210(Toray)

Separerm, Desal

- Polyfuran

PEC-1000 (Toray)

- Sulfonated Polysulfone

- Polyvinylalcohol

NTR(Nitto-Denko)

- Aryl-Alkyl polyamide/polyurea

RC-100 and PA-300 (Fluid System)

- Polybenzimidazole

Osmomics/Cellulose

- Polybenzimidazolone

Teijin

RO Membrane Transport Model

◎ Solution-Diffusion Model

$$J_w = A(\Delta P - \Delta \pi)$$

A = Water permeability constant

ΔP = Operation pressure

$\Delta \pi$ = Osmotic pressure

$$J_s = B(C_m - C_p)$$

B = Solute permeability constant

C_m = Solute concentration on membrane

C_p = Solute concentration in permeate

$$\text{Salt Rejection}(R) = [1 + B/A(1/(\Delta P - \Delta \pi))]^{-1}$$

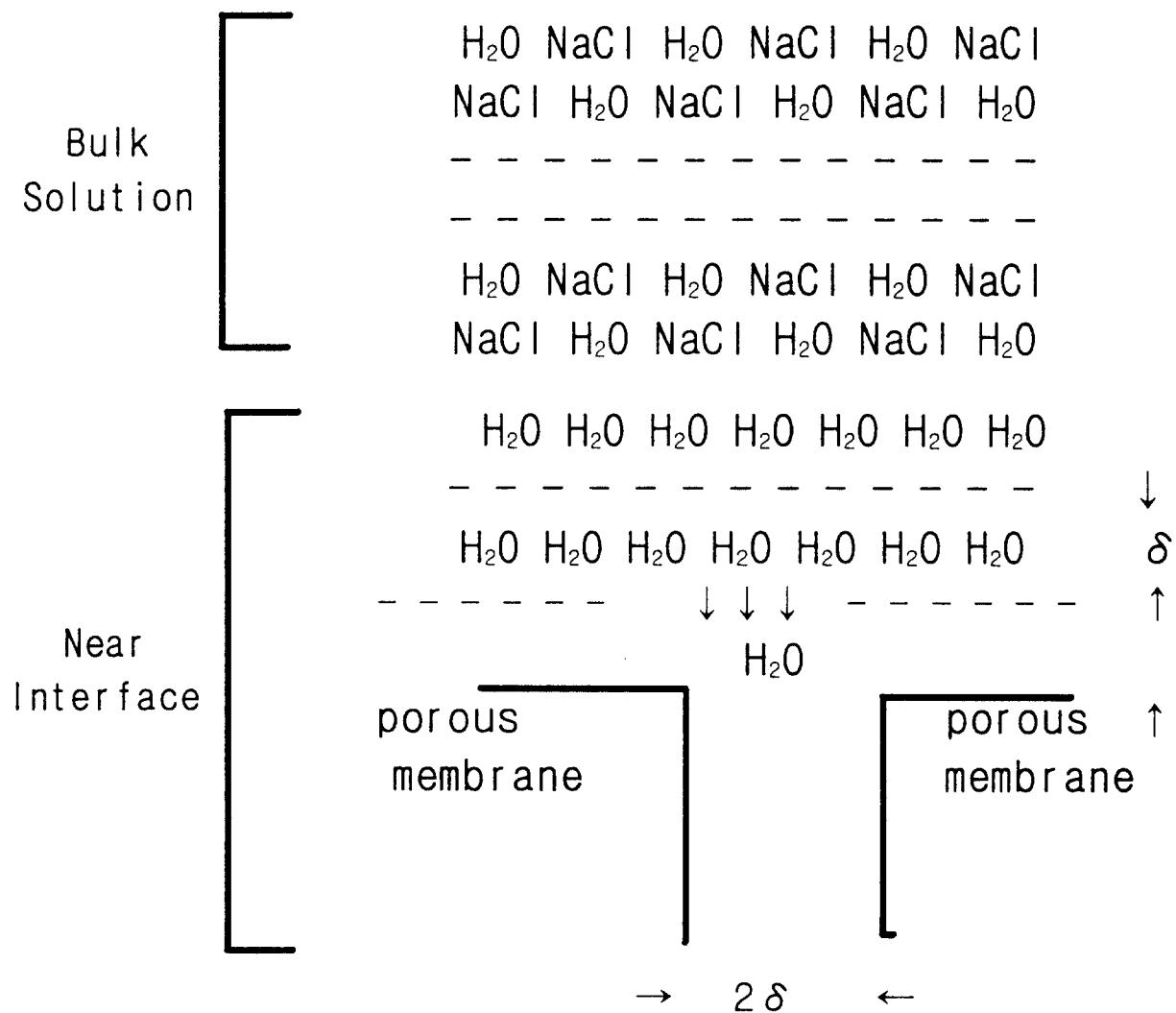
◎ Solution-Diffusion-Imperfection Model

$$J_w = A(\Delta P - \Delta \pi) + C\Delta P$$

$$J_s = B(C_m - C_p) + C\Delta P C_m$$

$$R = [1 + B/A(1/(\Delta P - \Delta \pi)) + C/A(\Delta P/(\Delta P - \Delta \pi))]^{-1}$$

◎ Preferential Sorption- Capillary Model



$$J_w = A(\Delta P - \Delta \pi)$$

$$J_s = C_t K_s D_{sm} (C_b - C_p) / L$$

$$C_t K_s D_{sm} / L \doteq B$$

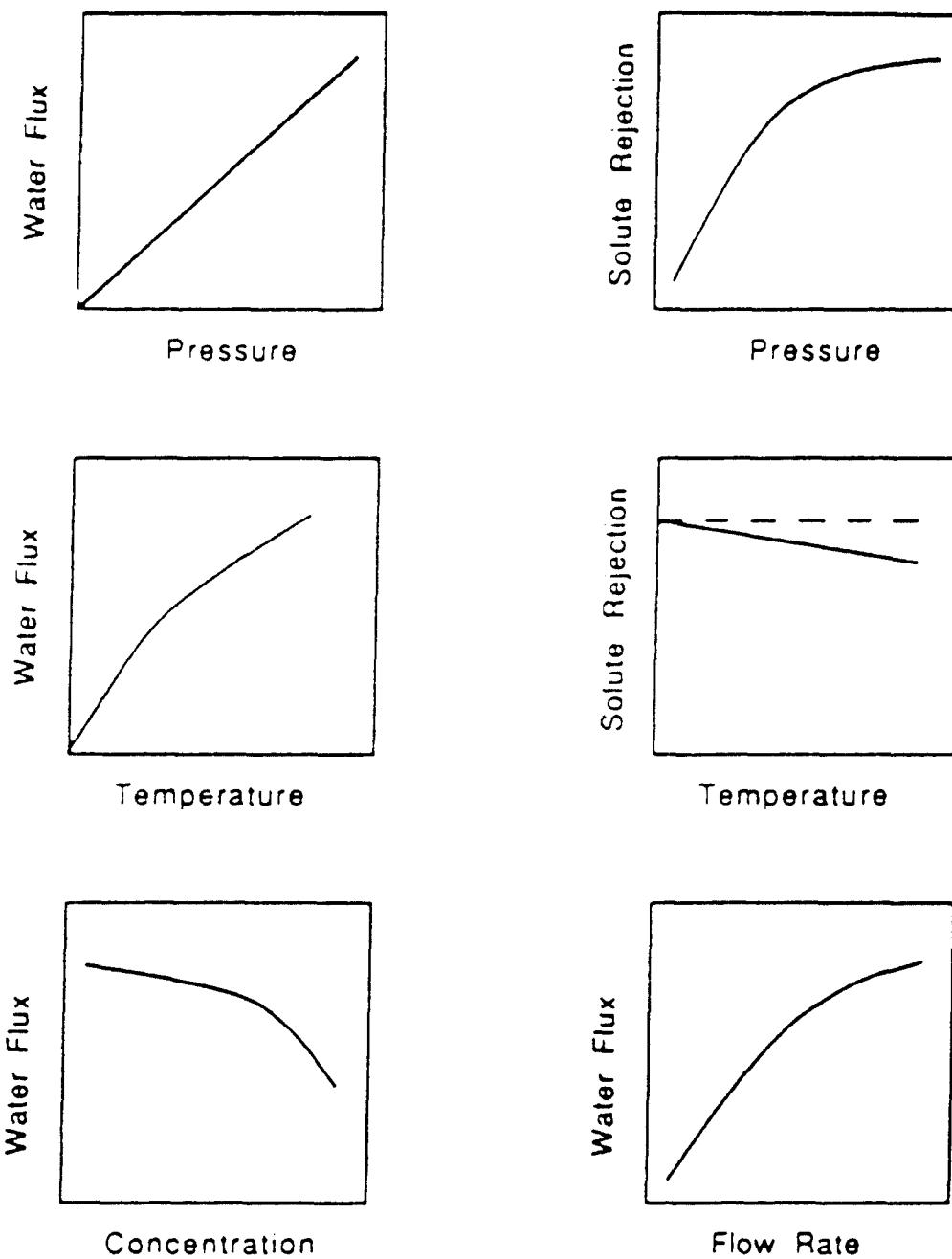
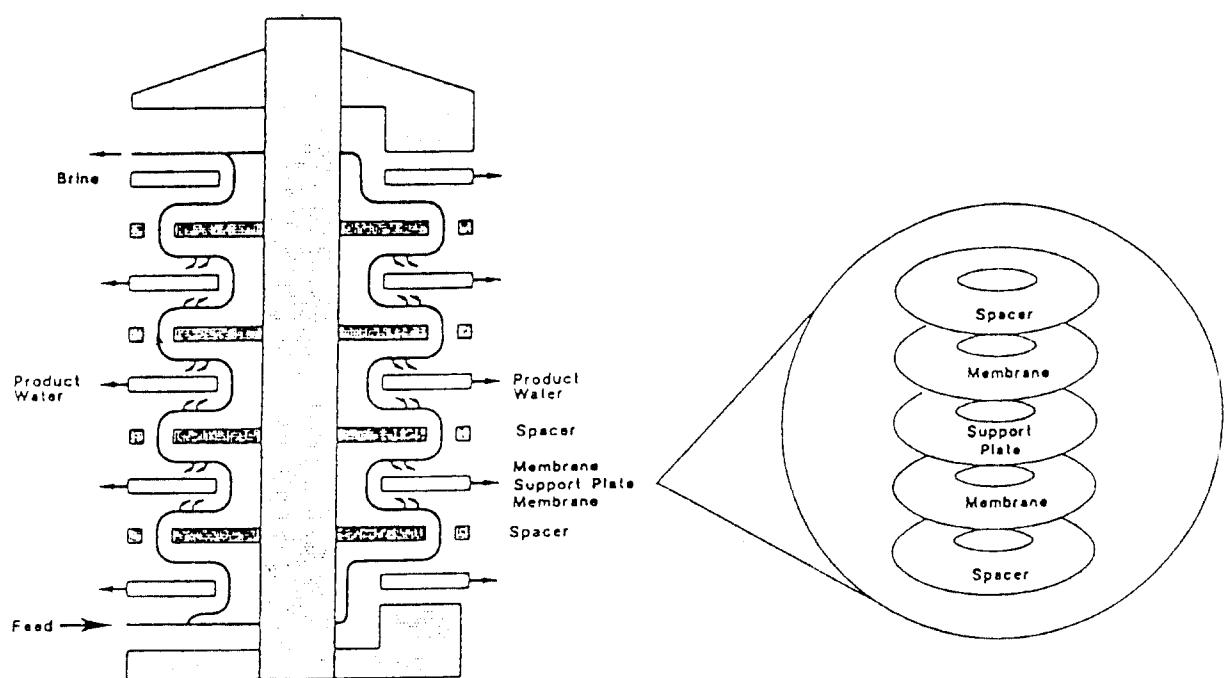


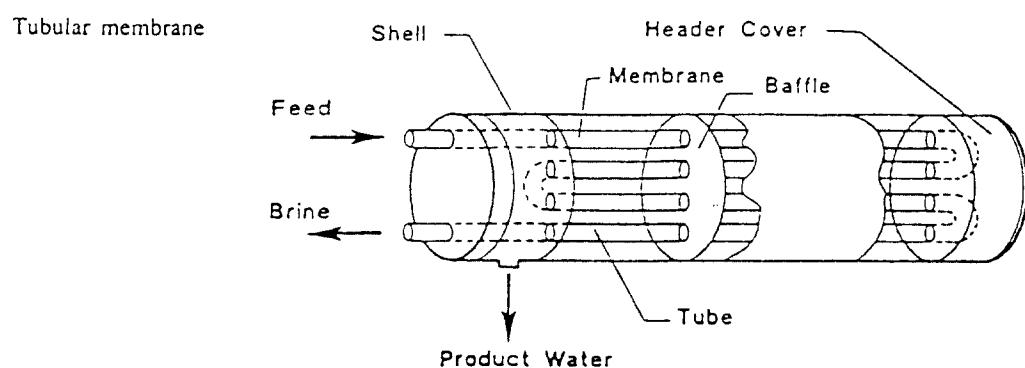
FIGURE Curves showing effect of variables on RO membranes (DOE 1990).

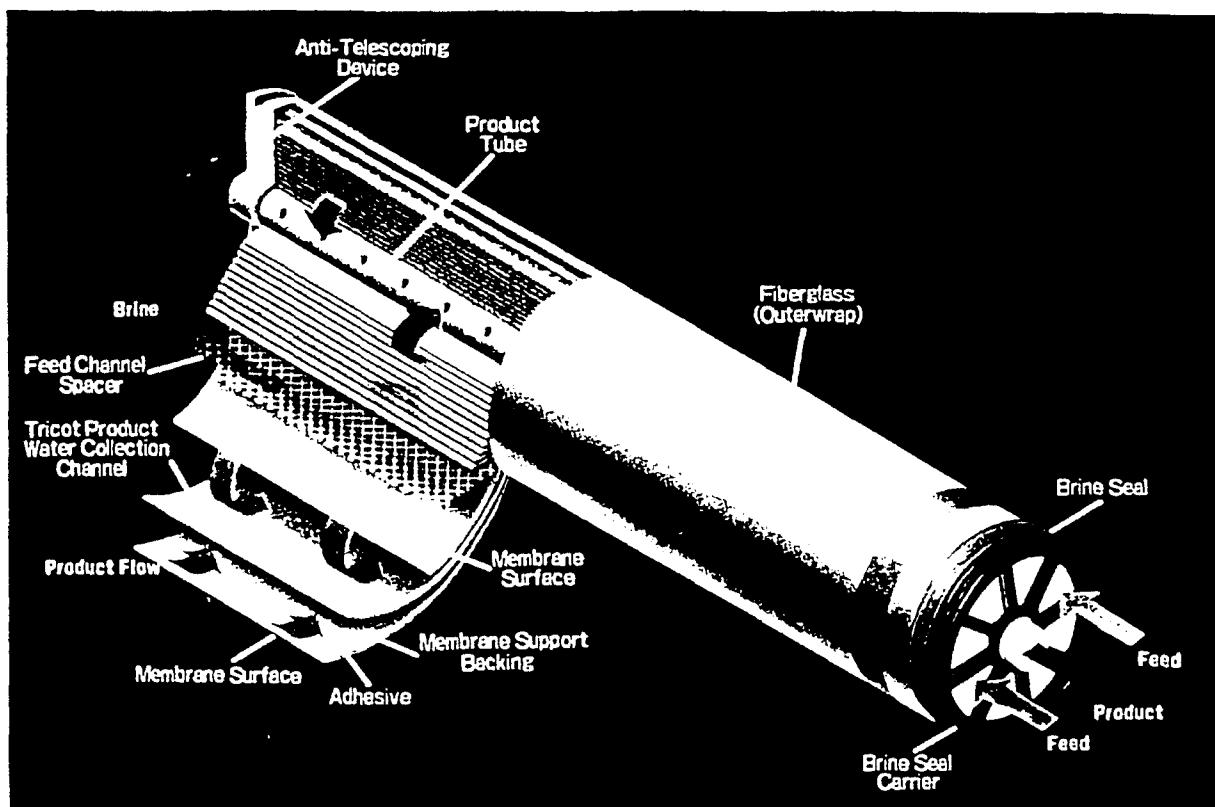
RO Module Configuration

ITEM	Tubular	Plate & Frame	Hollow Fiber	Spiral Wound
Cost	High	High	Low	Low
Cleaning	Easy	Easy	Difficult	Relatively Easy
Space	Large	Medium	Small	Small
Fouling	Low	Low	High	Medium
Energy	High	High	Medium	Low
Flux	Low	Low	High	Medium

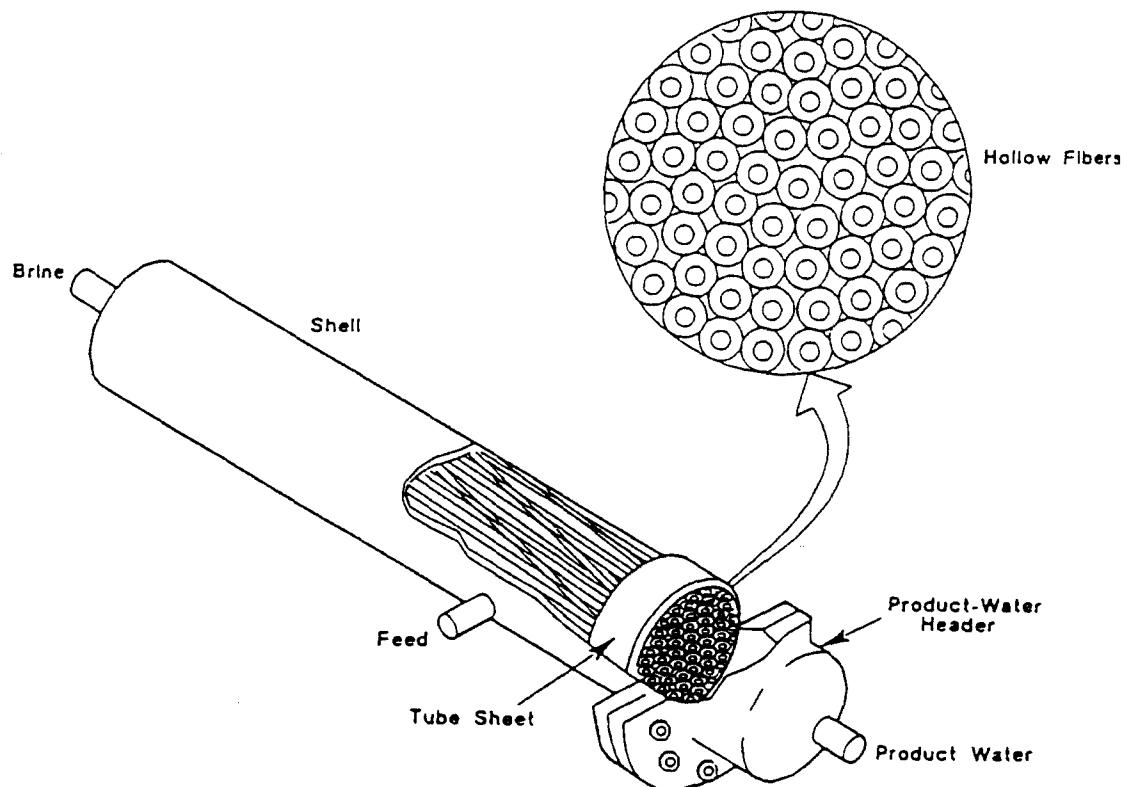


Schematic of a plate-and-frame module.



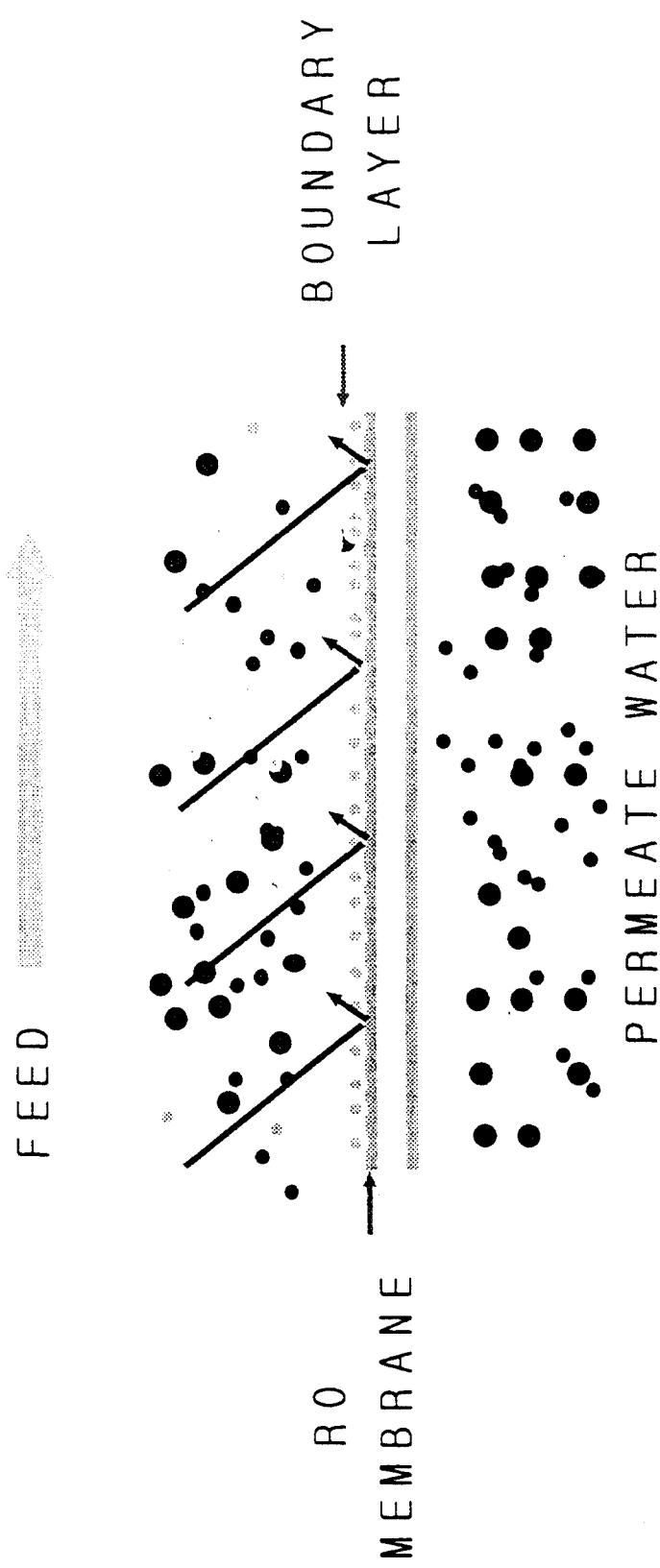


SPRAL-WOUND TYPE MODULE

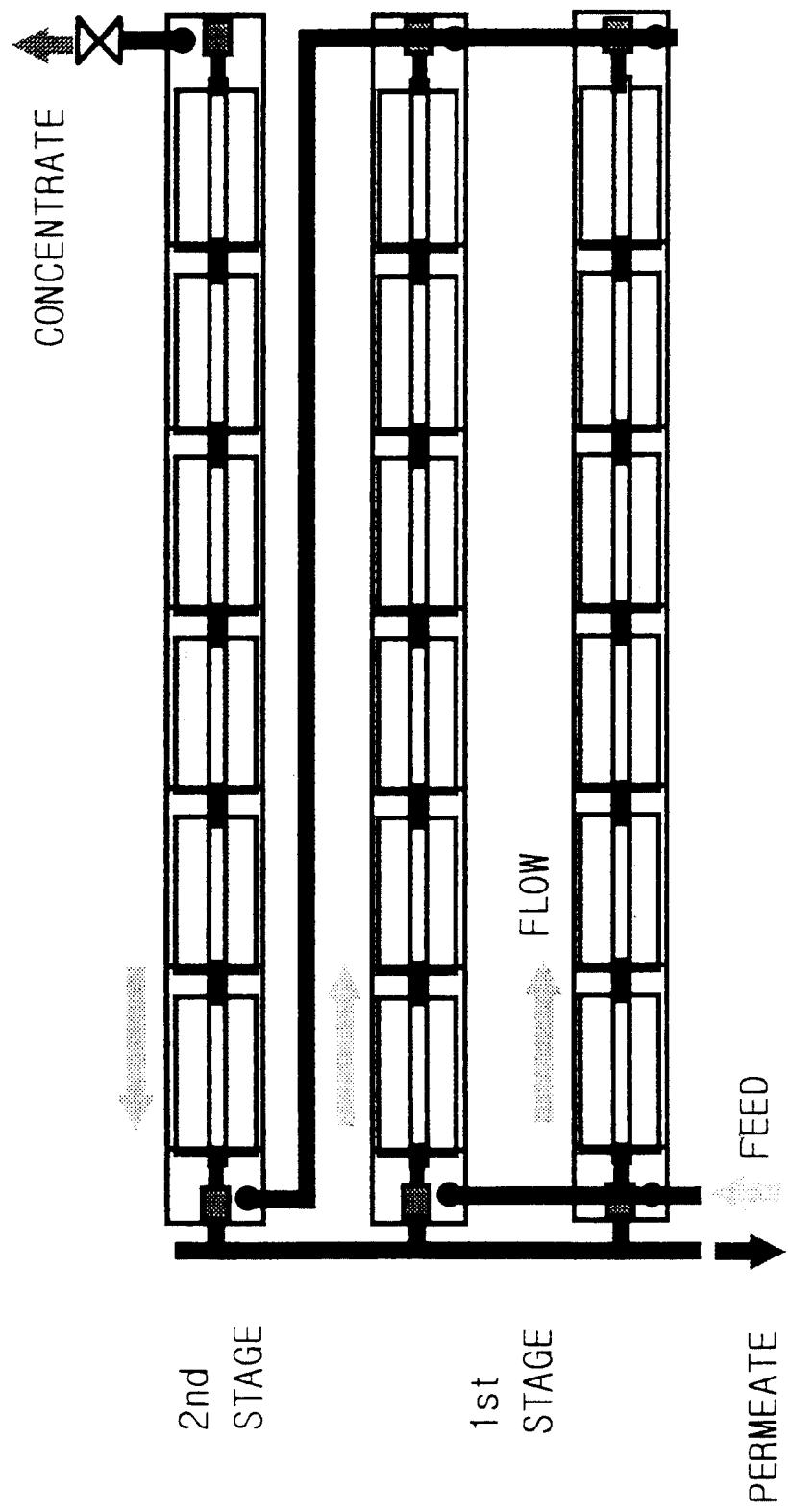


Cutaway view of hollow-fiber membrane module.

BOUNDARY LAYER

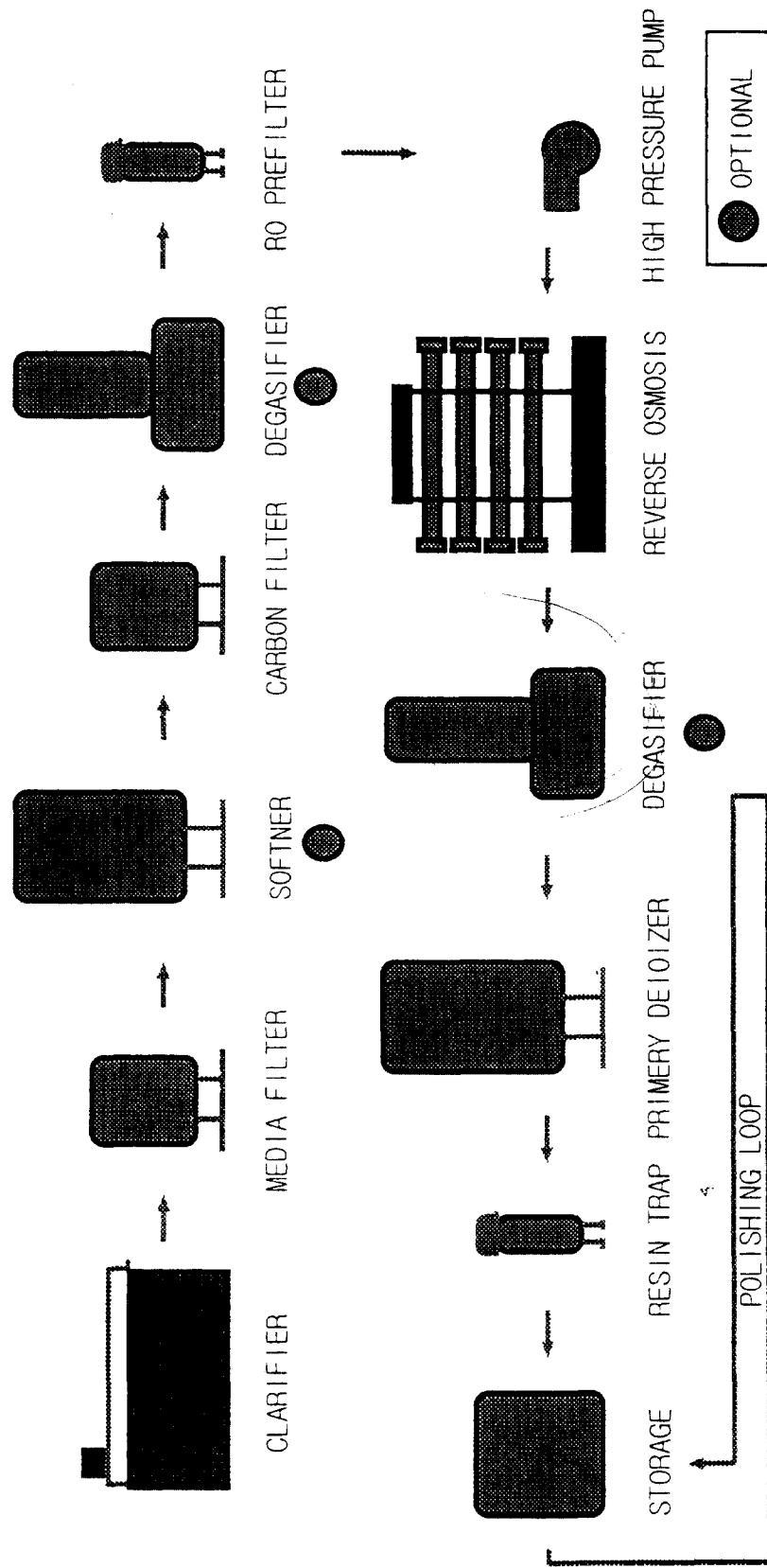


2:1 ARRAY SPIRAL WOUND ELEMENTS



주식회사사화

RO PRETREATMENT EQUIPMENT



주식회사 씨한

TYPICAL WATER ANALYSIS CONCERNS

Major Cations	Major Anions	Other Metals	Other Tests
Calcium (Ca)	Carbonate (CO_3)	Barium (Ba)	SDI
Magnesium (Mg)	Bicarbonate (HCO_3)	Sodium (Sr)	Turbidity
Potassium (K)	Chloride (Cl)	Iron (Fe)	TOC
Sodium (Na)	Nitrate (NO_3)	Aluminum (Al)	Fluoride (F)
	Sulfate (SO_4)	Copper (Cu)	Silica (SiO_2)
		Zinc (Zn)	Carbon Dioxide
			pH
			TDS

CONTROL OF FOULING

- CLARIFICATION (CARRY-OVER CAN CAUSE PROBLEMS)
- SAND & MULTIMEDIA FILTRATION
- RO PREFILTERS
- ADDITION OF BIOCIDES
- ADDITION OF DISPERSANTS
- MICROFILTRATION AND ULTRAFILTRATION

Future Trend in RO Industry

1.High Rejection : 99.5%

2.High Flux : 40~50gfd (225psi)
20~25gfd (150psi)

3.Fouling Resistant Membrane

4.Chlorine Resistant Membrane

5.Temperature Resistant Membrane

6.Organic Resistant Membrane